
**Technology Resource Document for the
Assembled Chemical Weapons Assessment
Environmental Impact Statement
Volume 3: Assembled Systems for
Weapons Destruction at Pine Bluff Arsenal**

**Environmental Assessment Division
Argonne National Laboratory**



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Volume 3

Technology Resource Document for the Assembled Chemical Weapons Assessment Environmental Impact Statement Volume 3: Assembled Systems for Weapons Destruction at Pine Bluff Arsenal

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NOTATION

The following is a list of the acronyms, initialisms, and abbreviations (including units of measure) used in this document. Some acronyms used in tables and figures only are defined the respective tables and figures.

ACW	assembled chemical weapons
ACWA	Assembled Chemical Weapons Assessment
AIRS	agent impurities removal system
ANAD	Anniston Army Depot
APG	Aberdeen Proving Ground
ASG	U.S. Army Surgeon General
ATP	Alternative Technology Program (development of chemical agent neutralization process)
BGAD	Blue Grass Army Depot
BIF	boiler or industrial furnace
BRA	brine reduction area (Baseline post-treatment drum drier equipment)
BRT	batch rotary treater
BSRM	burster size reduction machine
CAA	Clean Air Act
CAMDS	Chemical Agent Munitions Disposal System
CatOx	catalytic oxidation
CBDCOM	U.S. Army Chemical and Biological Defense Command
CFR	Code of Federal Regulations
COE	U.S. Army Corps of Engineers
COINS™	Continuously Indexing Neutralization System™
Composition B	a high explosive composed of 60% RDX, 39.5% TNT, and 0.5% calcium silicate (referred to as Comp B)
CRS	condensate recovery system
CST	continuous steam treater
CSTR	continuously stirred tank reactor
CTF	Chemical Transfer Facility
CWA	Clean Water Act
CWC	Chemical Weapons Convention
DCD	Deseret Chemical Depot
DFS	deactivation furnace system (baseline furnace consisting of a rotary retort and a heated discharge conveyor [HDC])
DOD	U.S. Department of Defense
DOT	U.S. Department of Transportation
DPE	demilitarization protective ensemble (highest level of chemical agent personal protective equipment)
DPG	Dugway Proving Ground

DRE	destruction removal efficiency
DSHS	dunnage shredder/hydropulper system
ECBC	Edgewood Chemical Biological Center
ECR	explosion-containment room
ECV	explosion-containment vestibule
EDS	engineering design study
EIRS	energetics impurities removal system
EIS	environmental impact statement
EPA	U.S. Environmental Protection Agency
EPRI	Electric Power Research Institute
ERH	energetics rotary hydrolyzer
FDA	U.S. Food and Drug Administration
FIRE	Factor Information Retrieval
FTE	full-time equivalent
GPCR	Gas-Phase Chemical Reduction™
HDC	heated discharge conveyor (baseline electric radiation tunnel furnace)
HEPA	high-efficiency particulate air (type of filtration system)
HMA	hot mix asphalt
HPLC	high-pressure liquid chromatography
ICB	Immobilized Cell Bioreactor™
JACADS	Johnston Atoll Chemical Agent Disposal System
LEL	lower explosive limit
LIC	liquid incinerator
LLNL	Lawrence Livermore National Laboratory
M23	land mine, 13-in.-diameter and 5-in.-high munition filled with VX
M28	propellant grain (M55 rocket)
M2A1	cartridge, 4.2 in., chemical agent (HD or HT)
M417	M55 rocket fuze
M426	projectile, 8 in., chemical agent (GB or VX)
M55	rocket, 115 mm, chemical agent (GB or VX)
M56	warhead, 115-mm rocket, chemical agent (GB or VX)
M60	cartridge, 105 mm, chemical agent (H or HD)
M60	rocket, 115 mm, inert
M61	rocket, practice 115 mm, simulant (EG)
MDB	Munitions Demilitarization Building
MPF	metal parts furnace (baseline tunnel furnace for drained munitions bodies)

MPT	metal parts treater
MRSM	modified rocket shear machine
NCD	Newport Chemical Depot
NEPA	National Environmental Policy Act
NRC	National Research Council
PBA	Pine Bluff Arsenal
PCD	Pueblo Chemical Depot
PM ₁₀	particulate matter with a diameter less than or equal to 10 micrometers
PMACWA	U.S. Department of Defense, Program Manager for Assembled Chemical Weapons Assessment
PMB	Personnel and Maintenance Building
PMCD	U.S. Army, Program Manager for Chemical Demilitarization
PMD	projectile/mortar disassembly (baseline reverse assembly equipment)
POTW	publicly owned treatment works
PRH	projectile rotary hydrolyzer
PUB	Process Utilities Building
RCRA	Resource Conservation and Recovery Act
RDM	rocket demilitarization machine
RDS	rocket drain station (baseline reverse assembly equipment on RSM)
RFP	request for proposal
ROD	record of decision
RSM	rocket shear machine (baseline reverse assembly equipment)
RSS	rocket shear station
SCWO	supercritical water oxidation
SDS	spent decontamination system (baseline) or spent decontamination solution (secondary waste from surface decontamination operations)
TAP	toxic air pollutant
TC	ton container
TCLP	toxicity characteristic leaching procedure
TOCDF	Tooele Chemical Agent Disposal Facility
TOX	toxic cubicle (baseline bulk agent buffer tank)
TRBP	thermal reduction batch processor
TRD	technical resource document
TSCA	Toxic Substances Control Act
TW	transpiring wall
UMDA	Umatilla Depot Activity
1X, 3X, 5X	U.S. Army system for material safety hazard classification (X, XXX, and XXXXX, respectively)

CHEMICAL FORMULAS

AgCl	silver chloride
AgNO ₃	silver nitrate
Al(OH) ₃	aluminum hydroxide
CaN ₂ O ₆	calcium nitrate
CEES	chloroethyl ethyl sulfide
CH ₄	methane
CO	carbon monoxide
CO ₂	carbon dioxide
DDT	dichlorodiphenyltrichloroethane
DMMP	dimethyl methylphosphonate
FeSO ₄	ferrous sulfate
GB	sarin (nerve agent), O-isopropyl methylphosphonofluoride
H	undistilled sulfur mustard, bis(2-chloroethyl)sulfide
H ₂	hydrogen
HC	hydrocarbons
HCl	hydrogen chloride
HCN	hydrogen cyanide
HD	distilled sulfur mustard, bis(2-chloroethyl)sulfide
HF	hydrogen fluoride
HNO ₃	nitric acid
H ₂ O	water
H ₂ O ₂	hydrogen peroxide
H ₃ PO ₄	phosphoric acid
H ₂ S	hydrogen sulfide
HT	blister agent, mustard agent (H) with T
KOH	potassium hydroxide
LN ₂	liquid nitrogen
LOX	liquid oxygen
MPA	methylphosphonic acid
N or N ₂	nitrogen
NaCl	sodium chloride
Na ₂ CO ₃	sodium carbonate
NaF	sodium fluoride
NaOCl	sodium hypochlorite (supertropical bleach, household bleach)
NaOH	sodium hydroxide
NH ₄ OH	ammonium hydroxide
NO	nitrogen oxide
NO ₂	nitrogen dioxide
N ₂ O	nitrous oxide
NO _x	nitrogen oxides
O or O ₂	oxygen
PCB	polychlorinated biphenyl
PCP	pentachlorophenol
PH ₃	phosphine

RDX	cyclotrimethylenetrinitramine (a high explosive)
SO ₂	sulfur dioxide
SO _x	sulfur oxides
SVOC	semivolatile organic compound
TNT	2,4,6-trinitrotoluene (a high explosive)
TOC	total organic carbon
VOC	volatile organic compound
VX	methylphosphonothioic acid (nerve agent)

UNITS OF MEASURE

acfm	actual cubic foot (feet) per minute
atm	atmosphere(s)
°C	degree(s) Celsius
cm	centimeter(s)
d	day(s)
°F	degree(s) Fahrenheit
ft	foot (feet)
ft ²	square foot (feet)
ft ³	cubic foot (feet)
gal	gallon(s)
g	gram(s)
GWh	gigawatt hour(s)
h	hour(s)
ha	hectare(s)
in.	inch(es)
kg	kilogram(s)
km	kilometer(s)
kW	kilowatt(s)
L	liter(s)
lb	pound(s)
M	molar
m	meter(s)
m ³	cubic meter(s)
mg	milligram(s)
mi	mile(s)
min	minute(s)
mm	millimeter(s)
MMBtu	million British thermal units
MW	megawatt(s)
MWh	megawatt hour(s)
MPa	megapascal(s)
ppm	part(s) per million
psia	pound(s) per square inch, absolute
s	second(s)

rpm	revolutions per minute
scf	standard cubic foot (feet)
t	metric ton(s)
ton	short ton(s)
wt%	weight percent
yd ³	cubic yard(s)
yr	year(s)

**TECHNOLOGY RESOURCE DOCUMENT
FOR THE
ASSEMBLED CHEMICAL WEAPONS ASSESSMENT
ENVIRONMENTAL IMPACT STATEMENT**

**VOLUME 3:
ASSEMBLED SYSTEMS FOR WEAPONS DESTRUCTION
AT PINE BLUFF ARSENAL**

by

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3.1 INTRODUCTION

3.1.1 DOCUMENT PURPOSE

This volume of the Technical Resource Document (TRD) for the Environmental Impact Statement (EIS) for the *Design, Construction and Operation of One or More Pilot Test Facilities for Assembled Chemical Weapons Destruction Technologies at One or More Sites* (PMACWA 2001g) pertains to the destruction of assembled chemical weapons (ACW) stored in the U.S. Army's unitary chemical stockpile at Pine Bluff Arsenal (PBA), located outside Pine Bluff, Arkansas. This volume presents technical and process information on each of the destruction technologies applicable to treatment of the specific ACW stored at PBA. The destruction technologies described are those that have been demonstrated as part of the Assembled Chemical Weapons Assessment (ACWA) selection process (see Volume 1).

It should be noted that some options for establishing ACWA pilot-scale facilities at specific installations are highly unlikely. However, no judgment regarding the feasibility or practicality of establishing a pilot-scale facility at a specific installation is expressed in this TRD.

3.1.2 ASSEMBLED CHEMICAL WEAPONS ASSESSMENT PROGRAM AT PINE BLUFF ARSENAL

The U.S. Department of Defense (DOD) Program Manager for Assembled Chemical Weapons Assessment (PMACWA) defines ACW as munitions containing both chemical agents

and energetic materials (e.g., propellants, explosives) that are stored in the U.S. unitary¹ chemical weapons stockpile. Such devices include rockets, projectiles and mortars, and land mines.² Unitary agents include chemical blister agents (i.e., the mustard agents H, HD, and HT) and chemical nerve agents (i.e., GB [sarin] and VX) (U.S. Army Chemical and Biological Defense Command [CBDCOM] 1997). These agents are not listed as hazardous wastes in Arkansas, although the destruction facility would be permitted under federal and state hazardous waste laws. Volume 1 of this TRD provides background information on the agent and energetic components of ACW.

Each of the stockpile installations stores a different combination of individual types or configurations of ACW. Different or modified component treatment technologies are often required for the diverse ACW types or configurations maintained at the various stockpile locations. Thus, a technology or unit that can be applied to one type or configuration of ACW may not be applicable to another. This volume of the TRD provides specific information for destruction of ACW stored at PBA.

The original ACW unitary stockpile contained approximately 31,500 tons (28,576 t) of unitary agents (Pacoraro 1999, as cited in National Research Council [NRC] 1999) stored in a variety of ACW and bulk containers (e.g., ton containers [TCs]). In addition to PBA, stockpile locations in the continental United States include Aberdeen Proving Ground (APG), Maryland; Anniston Army Depot (ANAD), Alabama; Newport Chemical Depot (NCD), Indiana; Blue Grass Army Depot (BGAD), Kentucky; Pueblo Chemical Depot (PCD), Colorado; Desert Chemical Depot (DCD), Utah; and Umatilla Depot Activity (UMDA), Oregon.³ ACW were also stored at the Johnston Atoll Chemical Agent Disposal System (JACADS) facility; however, ACW destruction at JACADS has been completed. The ACW at Tooele Chemical Agent Disposal Facility (TOCDF) at DCD are currently being destroyed through the baseline incineration process; this process, as defined by the U.S. Army Program Manager for Chemical Demilitarization (PMCD 1988), has undergone a number of improvements since its initial implementation. Baseline incinerator systems are currently being constructed at other stockpile locations, specifically, at PBA, ANAD, and UMDA. Only bulk agent containers are stored at APG and NCD; nonincineration-based destruction facilities are planned for these installations.

Figure 3.1 shows all the unitary stockpile locations. Table 3.1 provides an inventory (as of November 1999) of the various types of chemical munitions stored at these installations, including PBA.

¹ The term “unitary” refers to the use of a single hazardous compound (i.e., chemical agent) in the munitions. In contrast, “binary” chemical weapons use two relatively non-hazardous compounds that are mixed together to form a hazardous or lethal compound after the weapon is fired or released.

² Mortars are often defined as a type of cartridge or projectile.

³ These installations, except for BGAD, store both ACW and chemical agents in bulk (e.g., TCs). Chemical agents stored in bulk are not considered ACW and are not addressed under the ACWA program.

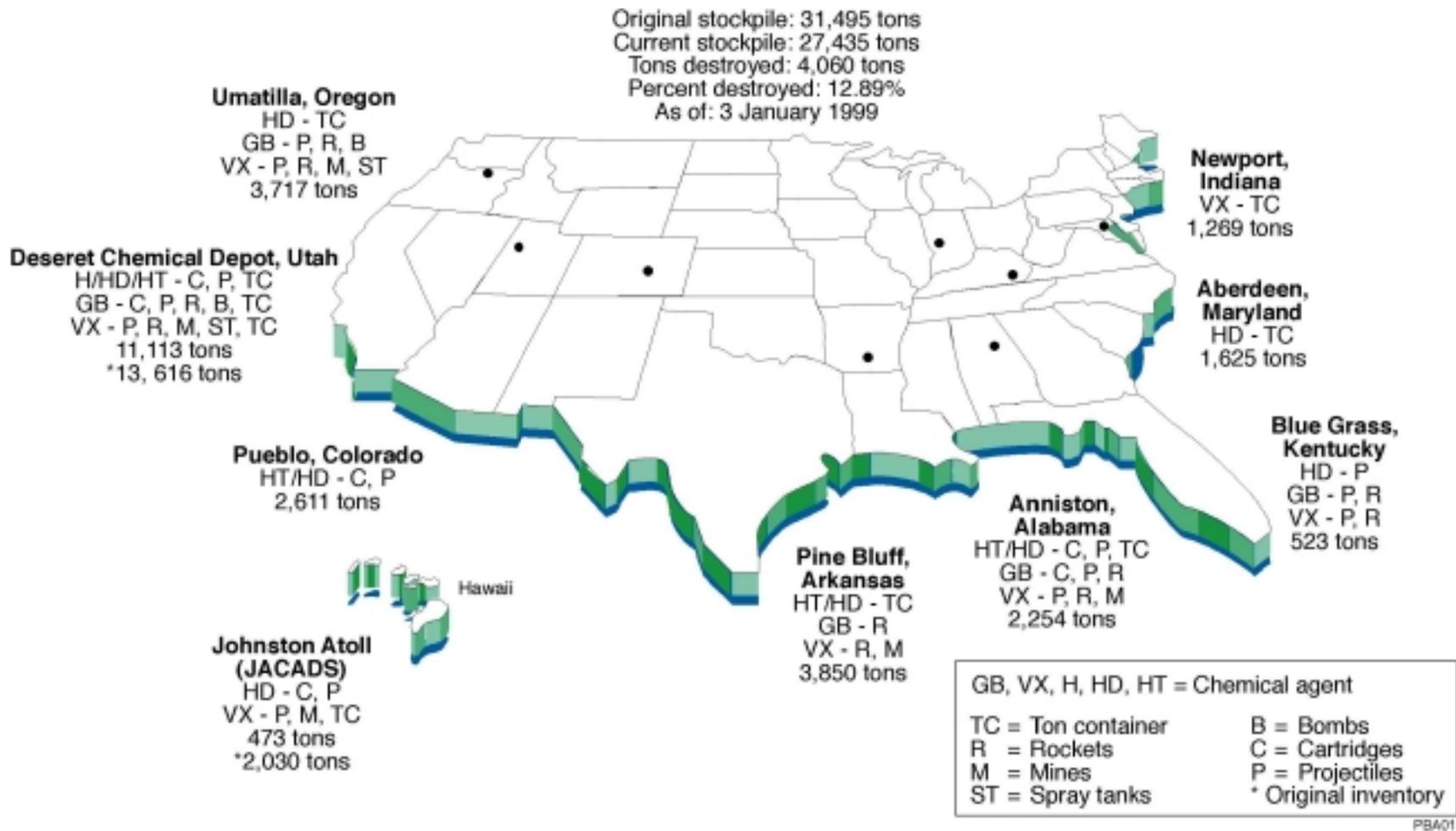


FIGURE 3.1. Types of Agent, Quantities of Agent, Types of Munitions, and Percentage of Total Agent Stockpiled at Each Storage Site (Source: Pacoraro 1999, as cited in NRC 1999) (Note: The information presented in this figure represents the stockpile as of January 3, 1999. Since that time, destruction of the inventory at JACADS has been completed, and much of the inventory at Deseret Chemical Depot has been destroyed.)

TABLE 3.1 Chemical Munitions Inventory by Stockpile Location^{a,b}

Agent	Item	<u>Anniston Army Depot</u>		<u>Deseret Chemical Depot</u>	
		No. of Munitions	Agent (lb)	No. of Munitions	Agent (lb)
H	155-mm projectiles	c		54,663	639,540
HT	4.2-in. cartridges	183,552	1,064,600	62,590	363,020
HD	4.2-in. cartridges	75,360	452,160	976	5,860
HD	105-mm cartridges	23,064	68,500		
HD	155-mm projectiles	17,643	206,420		
GB	105-mm cartridges	74,014	120,640	119,400	194,620
GB	105-mm projectiles	26	40	679,303	1,107,260
GB	155-mm projectiles	9,600	62,400	89,141	579,420
GB	8-in. projectiles	16,026	232,380		
GB	M55 rockets	42,738	457,300	28,945	309,720
GB	M56 rocket warheads	24	260	1,056	11,300
VX	155-mm projectiles	139,581	837,480	53,216	319,300
VX	8-in. projectiles			1	20
VX	M55 rockets	35,636	356,360	3,966	39,660
VX	M56 rocket warheads	26	260	3,560	35,600
VX	Mines	44,131	463,380	22,690	238,240
L	Ton containers			10	25,920
HD	Ton containers	108	185,080	6,398	11,383,420
HT	Ton container				
GA	Ton containers			2	2,820
TGA ^d	Ton containers			2	1,280
TGB ^d	Ton containers			7	6,960
GB	WETEYE bombs			888	308,140
GB	500-lb bombs				
GB	750-lb bombs			4,463	981,860
GB	Ton containers			5,709	8,598,200
VX	Spray tanks			862	1,168,880
VX	Ton containers			640	910,960

TABLE 3.1 (Cont.)

Agent	Item	Blue Grass Army Depot		Pine Bluff Arsenal	
		No. of Munitions	Agent (lb)	No. of Munitions	Agent (lb)
H	155-mm projectiles				
HT	4.2-in. cartridges				
HD	4.2-in. cartridges				
HD	105-mm cartridges				
HD	155-mm projectiles	15,492	181,260		
GB	105-mm cartridges				
GB	105-mm projectiles				
GB	155-mm projectiles				
GB	8-in. projectiles	3,977	57,660		
GB	M55 rockets	51,716	553,360	90,231	965,480
GB	M56 rocket warheads	24	260	178	1,900
VX	155-mm projectiles	12,816	76,900		
VX	8-in. projectiles				
VX	M55 rockets	17,733	177,340	19,582	195,820
VX	M56 rocket warheads	6	60	26	260
VX	Mines			9,378	98,460
L	Ton containers				
HD	Ton containers			107	188,400
HT	Ton container			3,591	6,249,100
GA	Ton containers				
TGA	Ton containers				
TGB	Ton containers				
GB	WETEYE bombs				
GB	500-lb bombs				
GB	750-lb bombs				
GB	Ton containers				
VX	Spray tanks				
VX	Ton containers				

TABLE 3.1 (Cont.)

Agent	Item	Pueblo Chemical Depot		Umatilla Arsenal	
		No. of Munitions	Agent (lb)	No. of Munitions	Agent (lb)
H	155-mm projectiles				
HT	4.2-in. cartridges	20,384	118,220		
HD	4.2-in. cartridges	76,722	460,340		
HD	105-mm cartridges	383,418	1,138,760		
HD	155-mm projectiles	299,554	3,504,780		
GB	105-mm cartridges				
GB	105-mm projectiles				
GB	155-mm projectiles			47,406	308,140
GB	8-in. projectiles			14,246	206,560
GB	M55 rockets			91,375	977,720
GB	M56 rocket warheads			67	720
VX	155-mm projectiles			32,313	193,880
VX	8-in. projectiles			3,752	54,400
VX	M55 rockets			14,513	145,140
VX	M56 rocket warheads			6	60
VX	Mines			11,685	122,700
L	Ton containers				
HD	Ton containers			2,635	4,679,040
HT	Ton container				
GA	Ton containers				
TGA	Ton containers				
TGB	Ton containers				
GB	WETEYE bombs				
GB	500-lb bombs			27	2,960
GB	750-lb bombs			2,418	531,960
GB	Ton containers				
VX	Spray tanks			156	211,540
VX	Ton containers				

- ^a Information on items appearing below the dashed line (including ton containers, bombs, and spray tanks) is provided for information purposes only. Although considered part of the unitary stockpile, these items are not ACW.
- ^b The chemical munitions inventory at JACADS is not included in this table because destruction of this inventory has been completed.
- ^c A blank indicates that the item is not included in the inventory at that location.
- ^d The “T” before GA and GB stands for “thickened.”

The unitary stockpile at PBA differs from other installations in that it is the only stockpile site used to store ACW containing only nerve agent (GB and VX).⁴ In addition, the incinerator that is being constructed at PBA does not rule out establishment of an ACWA pilot facility at the installation. Overall, the quantity of chemical agent stored at PBA accounts for 12.3 wt% of the total U.S. stockpile. PBA's inventory is the second largest among the U.S. Army's eight continental U.S. storage sites.

The unitary stockpile at PBA consists of rockets and rocket warheads containing GB and VX agent and land mines containing VX agent. No projectiles or mortars are stored at PBA. Specific ACW stored at PBA include M55 rockets filled with either GB or VX agent, and M56 rocket warheads filled with either GB or VX agent. M23 land mines containing VX agent are also stored at PBA. The energetics in these ACW are limited to those present in rockets and land mines.

Table 3.2 identifies the types of rockets and land mines stored at PBA and their agent and energetic components. Volume 1 of this TRD contains more detailed descriptions of the ACW types and their components.

3.1.3 ORGANIZATION OF TECHNICAL RESOURCE DOCUMENT

This document provides primary support for an EIS that evaluates alternative weapons destruction technologies for pilot-scale testing at ANAD, PBA, PCD, and BGAD, in compliance with the National Environmental Policy Act (NEPA) (PMACWA 2000b). This TRD consists of five volumes (see Figure 3.2). Volume 1 provides general information on the ACWA program; a description of the ACW, including chemical and energetic components; an overview of the ACWA technology selection process; and a summary of each of the ACWA system treatment technologies. Volume 1 also includes five supporting appendices. Volume 2 pertains to ANAD; Volumes 4 and 5 pertain to PCD

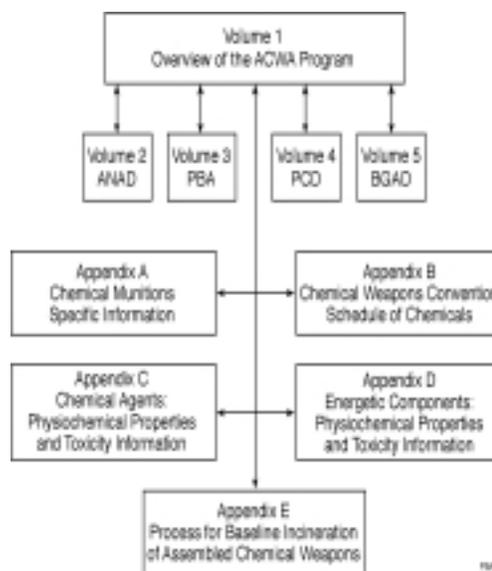


FIGURE 3.2 Organization of Technical Resource Document

⁴ PBA also stores bulk containers of mustard agent, which, as indicated previously, are not considered ACW. However, the ACWA technology systems discussed herein are capable of destroying the bulk mustard agent stored at PBA.

TABLE 3.2 Assembled Chemical Weapons Inventory at PBA

Munition	Number in Storage ^a	Length ^b	Weight ^b	Agent Amount ^b	Burster Type	Burster Amount ^b	Propellant Type	Propellant Amount ^b	Fuze Type	Fuze Amount ^b
115-mm M55 Rocket GB filled	90,231	1.98 m	25.9 kg	4.9 kg	Comp B or Tetrytol	1.5 kg	M28 ^c	8.7 kg	M417 (RDX)	11.9 g
115-mm M55 Rocket VX filled	19,582	1.98 m	25.9 kg	4.5 kg	Comp B or Tetrytol	1.5 kg	M28 ^c	8.7 kg	M417 (RDX)	11.9 g
115-mm M56 Rocket warhead GB Filled	178	NA ^d	NA	4.9 kg	Comp B or Tetrytol	1.5 kg	None	None	M417 (RDX)	11.9 g
115-mm M56 Rocket warhead VX filled	26	NA	NA	4.5 kg	Comp B or Tetrytol	1.5 kg	None	None	M417 (RDX)	11.9 g
33-cm M23 Land Mine VX filled	9,378	13 cm (height)	10.3 kg (without fuze)	4.77 kg	Comp B4 ^e	1.8 kg	None	None	M603 ^f	0.5 9

^a Number in storage represents data as of July 11, 1997.

^b Conversions: 1 in. = 2.54 cm; 1 lb = 0.454 kg.

^c M28 propellant consists of 60% nitrocellulose, 23.8% nitroglycerine, and 9.9% triacetin.

^d NA = data not available.

^e M23 mines also contain a tubular mine activator made of Composition B4, a cylindrical booster made of Composition A5, and a small tetryl booster pellet.

^f The M603 fuze consists of an upper charge (47 mg potassium chlorate, 15 mg antimony sulfide, 22 mg lead thiocyanate, and 5 mg lead azide), an intermediate charge (250 mg lead azide), and a lower charge (120 mg RDX)

Source: Compilation of information presented in Appendix A of Volume 1 of this TRD and Appendix A of NRC (1999).

and BGAD, respectively; and this volume, Volume 3, addresses PBA. Section 3.2 of this volume identifies and describes each of the technologies that could be used to treat the ACW stored at PBA for each of the six process categories (munitions access, agent treatment, energetics treatment, dunnage treatment, metal parts treatment, and effluent management and pollution controls). Following a brief introduction, the history of the technology system is reviewed. Then, a general process overview is provided, the results of demonstration testing and engineering design studies are discussed, and a detailed process description is presented.⁵ For all the

⁵ The descriptions are based on the equipment used by the technology providers during the PMACWA demonstrations (General Atomics 1999, Parsons/Allied Signal 1999, Foster Wheeler/Eco Logic/Kvaerner 2000, AEA/CH2MHILL 2000). The equipment that may eventually be used in a pilot-scale facility may vary, depending on the system that is actually employed and system refinements. However, conceptually, the equipment used in a pilot-scale facility would be similar to that evaluated during the demonstration test phase of the ACWA program.

described systems, technologies common to other systems are also identified, as are possible technology combinations that can be employed to create different, but viable, systems.

Section 3.3 of this volume provides supplemental information for pilot testing assembled systems. Included are facility descriptions, system inputs and resource requirements, routine emissions and wastes, and activities and schedules. This section also addresses both construction and operation of the facility.

Section 3.4 of this volume contains a list of references that were used in preparing this volume. The technology provider reports included in this list (General Atomics 1999; Parsons/Allied Signal 1999; Foster Wheeler/Eco Logic/Kvaerner 2000; AEA/CHM2HILL 2000) contain more detailed information on the ACWA technologies.

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3.2 ASSEMBLED SYSTEMS FOR WEAPONS DESTRUCTION AT PINE BLUFF ARSENAL

Four ACWA technology systems are presently under consideration for pilot-scale testing at PBA.⁶ These systems and their corresponding processes are as follows:

- Primary destruction: agent and energetics neutralization; secondary destruction: supercritical water oxidation (SCWO) (demonstrated by General Atomics⁷). This system is referred to herein as neutralization/SCWO.
- Primary destruction: agent and energetics neutralization; secondary destruction: biological treatment (demonstrated by Parsons/Honeywell⁸). This system is referred to herein as neutralization/biotreatment.
- Primary destruction: agent and energetics neutralization and Gas-Phase Chemical Reduction (GPCR)TM; secondary destruction: transpiring-wall supercritical water oxidation (TW-SCWO) (demonstrated by Foster Wheeler/Eco Logic/Kvaerner). This system is referred to as neutralization/GPCR/TW-SCWO.
- Primary destruction: electrochemical oxidation via the SILVER IITM process (demonstrated by AEA/CH2MHILL). The technology provider indicates that no secondary treatment is needed. This system is referred to as electrochemical oxidation.

The neutralization/SCWO system is a viable technology system for treating ACW containing mustard agent or nerve agent. The neutralization/biotreatment system is viable only for ACW containing mustard agent. Both of these technology systems were demonstrated during Demonstration I (Demo I) of the ACWA demonstration test program. The latter two technologies, neutralization/GPCR/TW-SCWO and electrochemical oxidation, were demonstrated during Demonstration II (Demo II) of the ACWA demonstration test program. These technology systems are amenable to treating ACW stored at PBA containing nerve agent.

⁶ The technology system descriptions presented in this TRD were derived from data and information developed by technology providers during the PMACWA demonstration test phase for the ACWA program (PMACWA 1999a; 2001b,c). The use of technology provider names and nomenclature from demonstration documentation (General Atomics 1999, Parsons/Allied Signal 1999, Foster Wheeler/Eco Logic/Kvaerner 2000, AEA/CH2MHILL 2000) does not imply endorsement of a specific technology provider.

⁷ General Atomics refers to its ACWA system as the General Atomics Total Solution (GATS).

⁸ Honeywell purchased Allied Signal in early 2000; General Electric purchased Honeywell in 2000. Parsons/Honeywell refers to its ACWA system as the Water Hydrolysis of Explosives and Agent Technology (WHEAT) process.

As indicated in Volume 1, incineration is not a candidate technology in the EIS that this TRD supports. A baseline incineration facility is being constructed at PBA, however. The presence of an incinerator does not preclude pilot testing of an ACWA system at PBA. Although incineration is not a candidate ACWA technology, the four ACWA technologies listed above employ one or more components of the baseline incineration process (e.g., reverse assembly, pollution abatement system). Elements of the baseline incineration process are therefore included in the overview of baseline and ACWA system technologies provided in Volume I of this TRD (see Section 1.4). In addition, the baseline incineration process is described in more detail in Appendix E of Volume 1.

Table 3.3 provides an overview of the baseline incineration process and the ACWA technology systems being considered for PBA. A more detailed description of each of the ACWA technology systems follows.⁹ This document is based on a conceptual “full-scale” facility, as defined in the PMACWA Request for Proposal (RFP) for the ACWA Program (CBDCOM 1997). Exact specifications of units and processes, including operating temperatures and pressures, may vary.

3.2.1 NEUTRALIZATION/SCWO

The neutralization/SCWO technology system consists of neutralization of agents and energetics and secondary treatment of neutralization residuals using SCWO. This technology system, proposed by General Atomics,¹⁰ is applicable to all ACW stored at ANAD, including ACW containing nerve or mustard agent. It uses a solid-wall SCWO process. Operation of a transpiring-wall (TW)-SCWO unit is discussed in Section 2.2.3. The following subsections provide a more detailed discussion of the technologies and processes involved in this system. The technology provider’s technology demonstration report (General Atomics 1999) may be viewed for additional detail.

3.2.1.1 Process Overview

The neutralization/SCWO process, as applied to rockets and land mines stored at PBA, is summarized in Figure 3.3. As Figure 3.3 illustrates, ACW at PBA would be disassembled by using a modified baseline reverse assembly process, with some differences for rockets versus land mines. For rockets and land mines, the agent would first be accessed by using a punch and drain process. Rockets would then be sheared to access the fuze, burster, and propellant. For land

⁹ Monitoring of emissions is part of any environmental waste management scenario. Monitoring of ACW treatment processes will be prescribed in environmental permits issued under the federal Resource Conservation and Recovery Act (RCRA). Monitoring methodologies are not specifically described in this TRD.

¹⁰ Neutralization is a common element of three of the four technology systems discussed in this volume of the TRD.

TABLE 3.3 Technology Overview for Baseline Incineration and ACWA Technology Systems for PBA^a

Technology	Munitions Access	Agent Treatment	Energetics Treatment	Metal Parts Treatment	Dunnage Treatment
Baseline Incineration	Baseline reverse assembly	Liquid incinerator (LIC) (a stationary LIC)	Deactivation furnace system (DFS) (a rotary kiln incinerator), with heated discharge conveyor (HDC)	Metal parts furnace (MPF) (a roller hearth incinerator)	Size reduction and stationary bed incinerator
Neutralization/ SCWO	Parts of baseline reverse assembly, cryofracture	Hydrolysis ^b followed by SCWO	Caustic hydrolysis followed by SCWO	Caustic hydrolysis followed by thermal treatment with steam	Size reduction/ pulping followed by SCWO
Neutralization/ Biotreatment ^c	Modified baseline reverse assembly (fluid-abrasive cutting and fluid-mining)	Hydrolysis ^b followed by biotreatment	Caustic hydrolysis followed by biotreatment	Thermal treatment with steam	Size reduction/ thermal treatment with steam
Neutralization/ GPCR/TW-SCWO	Modified baseline reverse assembly (uses baseline process with modified equipment)	Hydrolysis ^b followed by TW-SCWO	Caustic hydrolysis followed by TW-SCWO	Caustic hydrolysis and spray washing followed by GPCR using hydrogen and steam	GPCR using hydrogen and steam
Electrochemical oxidation	Modified baseline reverse assembly (fluid-abrasive cutting and fluid-mining)	Electrochemical oxidation using SILVER II process	Electrochemical oxidation using SILVER II process	Detonation chamber and thermal treatment with steam	Size reduction followed by thermal treatment with steam

^a Combinations of these technologies may also be considered.

^b Nerve agents are treated using caustic hydrolysis; mustard agents are treated using water hydrolysis followed by a caustic wash.

^c Biotreatment is viable for mustard agent only.

Source: Adapted from PMACWA (1999a; 2001b,c).

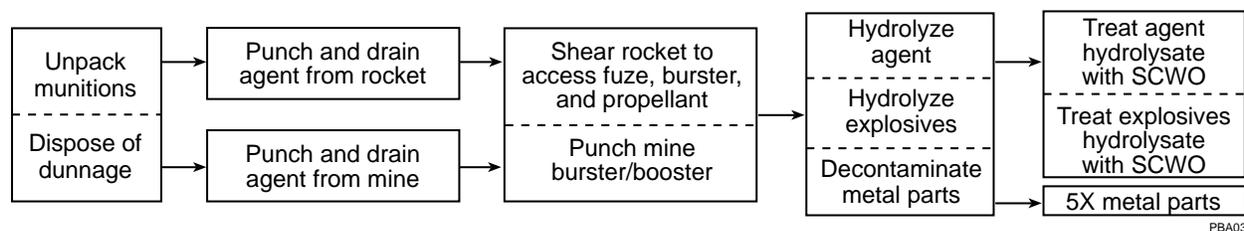


FIGURE 3.3 Overview of the Neutralization/SCWO Process (General Atomics System) for the Treatment of ACW at PBA (Source: Adapted from NRC 1999)

mines, fuzes and activators are stored separately from the land mines (but in the same container). The central burster would be pushed out of the mine after the agent is drained. The burster would then be processed with the fuze and activator. The drained nerve agents (GB and VX) would then be neutralized/hydrolyzed with sodium hydroxide (NaOH) solutions in systems operated at 194°F (90°C) and atmospheric pressure;¹¹ energetics would also be neutralized/ hydrolyzed with a NaOH solution, in systems also operated at 194°F (90°C) and atmospheric pressure. Dunnage would be shredded, micronized, hydropulped, and neutralized/hydrolyzed. Resulting hydrolysates would then be treated in separate SCWO units. Dunnage hydrolysate would be added to energetics hydrolysate and treated in the same SCWO unit. Thermal treatment would be used to treat metal parts to a 5X condition.¹²

3.2.1.2 History of Destructive Process

Neutralization and SCWO are the primary destructive processes employed in this technology. The history of these processes is summarized below.

3.2.1.2.1 Neutralization of Agents and Energetics

Agent neutralization and energetics neutralization by hydrolysis are discussed in detail in a 1999 NRC report (Appendixes D and E, respectively) (NRC 1999). The literature is extensive on neutralization of HD (NRC 1999). Technically, neutralization is a chemical reaction between an acid and a base to form a salt and water (NRC 1999). In this application, neutralization refers to a hydrolysis reaction in which a target compound reacts with water, an acid, or a base to break chemical bonds in the target compound (NRC 1999). Chemical demilitarization literature,

¹¹ The unit is not operated under pressure.

¹² The definition of 5X is provided in Volume 1 of this TRD (see Section 1-2.2.4). While materials treated to a 5X condition may be released for unrestricted use (e.g., recycling), materials that have been treated to a 3X condition must remain under government control. For example, hazardous waste disposal facilities may receive 3X waste.

therefore, often uses neutralization and hydrolysis as interchangeable terms for the same process (NRC 1999).

For energetics, this technology involves neutralization using solutions of NaOH. The NRC reports that there is less experience with base neutralization of energetic materials relative to experience with chemical agents (NRC 1999). However, neutralization of energetics has been substituted for open burning/open detonation, a treatment that has historically been applied to these materials (NRC 1999). The open literature contains many references to caustic hydrolysis of energetics, dating back to the mid-1800s (NRC 1999). The Navy recently published a review of alkaline hydrolysis of energetic materials pertinent to ACW (Newman 1999, as cited in NRC 1999).

Base hydrolysis decomposes energetic materials to organic and inorganic salts, organic degradation products, and various gases (NRC 1999). The base used — typically NaOH, potassium hydroxide (KOH), ammonium hydroxide (NH₄OH), or sodium carbonate (Na₂CO₃) — usually attacks all the functional groups of the energetic material (NRC 1999). While previous work with base hydrolysis involved studying reactions under ambient conditions, recent work has been conducted at elevated temperatures and pressures, which increases the solubility of the energetics in solution, increases the reaction rate, and reduces clogging of the reactor vessel (NRC 1999). The reactions, however, are exothermic and must be carefully controlled and monitored to prevent an explosion (NRC 1999).

The NRC indicates that caustic neutralization of energetics is not a mature technology; nevertheless, it concludes that “the current level of understanding is, perhaps, sufficient to indicate that engineering practices can probably restrict the domain of possible reaction products” (NRC 1999). Products from the neutralization reaction may include nitrates, nitrites, ammonia, nitrogen, hydrogen, organic acids, and formaldehyde, as well as various salts (NRC 1999).

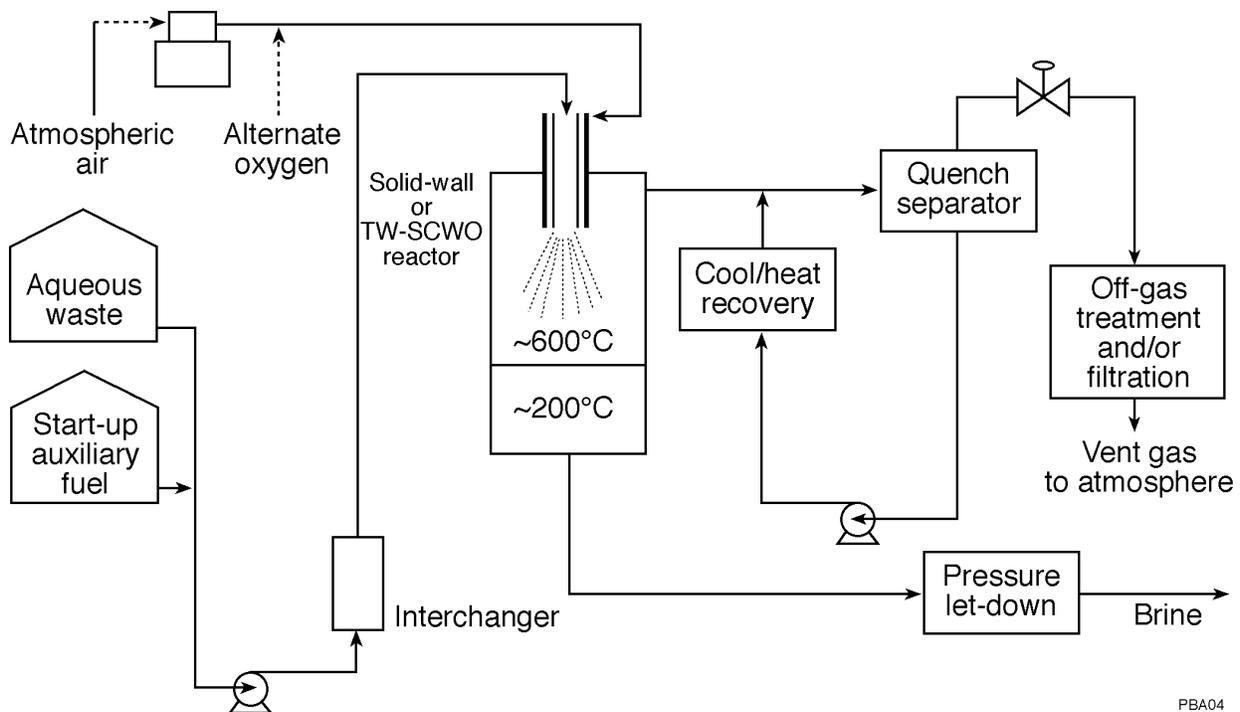
3.2.1.2.2 Supercritical Water Oxidation

The NRC reviews the SCWO process in Appendix F of its 1999 report. Much of the material in this appendix is based on a review of the SCWO technology for application to VX hydrolysates that the NRC performed in 1998 (NRC 1998). That work was conducted primarily in response to the proposed use of the SCWO technology for treating the VX hydrolysates resulting from neutralization of the U.S. Army’s bulk stockpile of VX at NCD, Newport, Indiana. Hydrolysis followed by application of SCWO is nearing the pilot-scale testing phase at NCD (PMCD 1998b, NRC 1999). The U.S. Army prepared an EIS of the hydrolysis/SCWO process proposed for treatment of bulk VX at NCD (PMCD 1998b), and concluded that the proposed facility would meet stringent permitting requirements of the Clean Water Act (CWA), the Resource Conservation and Recovery Act (RCRA), and the Clean Air Act (CAA). The U.S. Army further concluded that the site and environs of the facility would be affected by construction and pilot testing of the proposed facility, but that appreciable adverse human health

and environmental impacts would be unexpected, and those that may occur would be well within regulatory limits (PMCD 1998b).

When SCWO is used, the temperature and water pressure are raised to above supercritical conditions (705°F [374°C] and 3,204 psia [22 MPa]). Under these conditions, salts precipitate out of solution, and organic compounds are oxidized to carbon dioxide (CO₂) and water (H₂O), (NRC 1999). Figure 3.4 is a simplified process flow diagram for a typical solid-wall SCWO process.

SCWO is not widely used within the United States. The NRC reports that SCWO has been used on a pilot scale to treat other types of wastes, but that it is used commercially at only one location within the United States (NRC 1998, as cited in NRC 1999). Although SCWO has been under development for over 20 years, both in the United States and overseas, only recently have problems with the reactor vessel been sufficiently overcome to permit consideration of full-scale operations.



PBA04

FIGURE 3.4 Typical Flow Diagram for SCWO (Source: Adapted from NRC 1999)

3.2.1.3 Demonstration Testing¹³

The neutralization/SCWO technology was demonstrated during Demo I of the PMACWA demonstration test program. Demo I testing was conducted in spring 1999. This section provides a summary of demonstration testing for neutralization/SCWO. Demo I testing results are provided in PMACWA (1999a).

Baseline reverse assembly, carbon filtration, brine reduction area (BRA) operation, and other technologies employed in neutralization/SCWO were not evaluated during the demonstration testing. The following unit operations proposed for neutralization/SCWO were not selected for demonstration for the reasons given below.

Cryofracture System (bath, robotic transport, and press). This is a well-developed system that has been demonstrated at full scale at Dugway Proving Ground (DPG). For the ACWA program, the only required changes to the demonstrated equipment were scaling down the press and instituting conveyor transport of individual munitions through the liquid nitrogen (LN₂) bath. Demonstration of this unit was therefore not required.

Projectile Rotary Hydrolyzer (PRH). Drum dryers, the basis of the PRH, are well developed and have been demonstrated commercially. The PRH is essentially a batch process with a slow tumbling action (identical in principle to the energetics rotary hydrolyzer [ERH]). Therefore, demonstration of this unit was not considered critical.

Heated Discharge Conveyor (HDC). The proposed unit is essentially identical in design to the baseline HDC (used at TOCDF) but would operate in a nitrogen atmosphere. Heated bucket conveyors are well developed and have been demonstrated commercially. While demonstration of the HDC was originally planned, the discontinuation of testing of polychlorinated biphenyls (PCBs) made an HDC demonstration less essential at this stage in the program.¹⁴

Metal Parts Furnace (MPF). This batch furnace is similar to the baseline MPF structure except that induction heaters rather than gas-fired heaters are used. Operationally, the MPF differs from the baseline version because an inert atmosphere is used to process solid wastes. Demonstration of this unit was not required because the MPF has been proposed to treat only surface-washed metal hardware with a low organic loading.

¹³ This material was derived from PMACWA (1999a) and refers to demonstration testing conducted during Phase I of the ACWA demonstration process. Because demonstration testing was intended to apply to all ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

¹⁴ PCBs were originally identified as a constituent of concern for the M55 rockets because the rockets are stored in shipping/firing tubes made of an epoxy resin that can contain PCBs. PCBs were not evaluated during demonstration testing because regulatory approvals could not be obtained within the allotted timeframe. PCBs will be evaluated during pilot-scale operations.

The reasons for selecting the neutralization/SCWO demonstration unit, testing objectives, and significant deviations from the planned demonstration testing are answered in the following subsection.

3.2.1.3.1 Agent Hydrolysis

The U.S. Army demonstrated agent hydrolysis extensively as part of its Alternative Technology Program (ATP).¹⁵ The PMACWA ran agent hydrolysis units primarily to provide representative feedstock for SCWO and to characterize the intermediate product stream for residual agent, Schedule 2 compounds, and other substances required to verify the mass balance. The specific test objectives for these demonstration units included the following:

- Design, fabricate, and deliver GB and VX hydrolysate production systems with a production capacity of 100 gal (379 L) of hydrolysate per run;
- Use the hydrolysate recipes developed and tested by the Edgewood Chemical Biological Center (ECBC);
- Demonstrate that the agent concentration in the hydrolysate solution is less than the waste control limit by using the analytical methods developed and approved by the ECBC;
- Characterize solid, liquid, and gas process streams; and
- Provide agent hydrolysate in support of demonstration testing.

GB and VX hydrolysates were produced in a newly constructed 100-gal (379-L) stirred tank reactor system at the U.S. Army's Chemical Agent Munitions Disposal System (CAMDS) located at DCD in Utah. The design and manufacture of a hydrolysis system provided information on equipment and operational parameters that can be used for scale-up to a full-scale facility. Hydrolysate was shipped to DPG for use in the SCWO demonstration.

HD hydrolysate was produced at the Chemical Transfer Facility (CTF) at APG. The equipment used was not intended to be a model for scale-up to a full-scale facility, but was an

¹⁵ Water was tested in the ATP for HD, and caustic was tested for VX.

expedient design suitable for use in the contained environment of the CTF. HD hydrolysate was shipped to DPG for use in the SCWO demonstration.¹⁶

There were no significant deviations from the planned demonstration testing.

3.2.1.3.2 Energetics Hydrolysis

Other government agencies have previously evaluated energetics hydrolysis; however, further knowledge of the process was needed for evaluation, feedstock for SCWO was required, and characterization of the intermediate product streams for residual energetics and other substances was required to verify a mass balance. The specific test objectives of these demonstration units included the following:

- Produce energetics hydrolysate for use as feed material in subsequent demonstration testing;
- Characterize solid, liquid, and gas process streams; and
- Gather process operation information to support the ACWA program and future scale-up.

M28 propellant was hydrolyzed with 12% NaOH to produce hydrolysate in two production runs at the Radford Army Ammunition Plant in Radford, Virginia. Composition B and tetrytol were also hydrolyzed by using 12% NaOH in a single production run at the Pantex Plant in Amarillo, Texas. All of the hydrolysates were transported to DPG, Utah, and used as feedstock for the SCWO.

There were no significant deviations from the planned demonstration testing.

3.2.1.3.3 Dunnage Shredder/Hydropulper System

The DSHS was demonstrated to show that solid wastes (wooden dunnage, demilitarization protective ensemble [DPE])¹⁷ suits, and butyl rubber) could be adequately size-reduced and pulped to a pumpable mixture. Shredded material was used for SCWO pulped dunnage testing. The objectives of the demonstration testing included the following:

¹⁶ HT or T-mustard agent was not tested because the PMACWA determined that HT is similar enough to HD that demonstration results for HD can be applied to HT.

¹⁷ DPE suits are made of a plastic material containing chlorinated hydrocarbons.

- Validate the ability of the shredders and the hydropulper to adequately prepare the dunnage for downstream processing in the SCWO;
- Qualitatively evaluate the operability of the shredder/hydropulper unit operations with particular focus on materials handling; and
- Validate the ability of the shredders to process pallets and, separately, plastics (DPE suits), and butyl rubber.

Several commercial shredders were used to size-reduce the solid materials of interest. A low-speed shredder was used to break up the wooden pallets. The rough-shredded wood was size-reduced to small chunks in a hammer mill and then further reduced in a micronizer to the consistency of flour. Belt conveyors were used to transport the feeds between the units. A baghouse was used to collect dust generated by the shredding equipment. DPE suits (with metal parts removed) and butyl rubber (the material of boots and gloves) were rough-shredded in the low-speed shredder, cryocooled in a bath of LN₂, and reduced in size in a granulator. The size-reduced wood, plastic, and rubber, along with activated carbon (air filter material) and energetics hydrolysate, were combined to produce a pumpable slurry to feed to the SCWO. The demonstration shredding equipment is identical in size to that of the units proposed for the full-scale system.

Significant deviations from the planned demonstration testing included the following:

- Metal pieces were removed from DPE suits prior to shredding because removal by magnets after shredding was ineffective, resulting in damaged granulator blades.
- DPE suit plastic was successfully shredded to less than 0.12 in. (3 mm), a test objective, but this size proved to be too large to be fed to the demonstration SCWO unit without plugging the feed system. Alternatives for further size reduction were explored, but ultimately the plastic was sieved to 0.04 in. (1 mm) or less for use as feed for the SCWO dunnage validation runs.
- The hydropulper operation was not validated. Systemization and the single work-up run indicated that the unit provided no size-reduction benefit. The hydropulper may not be used in the final system design.

3.2.1.3.4 Energetics Rotary Hydrolyzer

The ERH was demonstrated to determine its effects on the physical and chemical properties of the munitions and liquid effluent. The objectives of the demonstration testing included the following:

- Demonstrate effective dissolution of aluminum and energetics in fuzes and bursters and propellant in rocket motors to allow downstream processing in the continuously stirred tank reactor (CSTR), SCWO, and HDC;
- Determine the extent of deactivation of the energetics in fuzes and bursters and the propellant in rocket motors;
- Validate the retention times for aluminum and energetics in fuzes and bursters and propellant in rocket motors; and
- Characterize the gas, liquid, and solid process streams from the ERH.

Fuzes, bursters, and rocket motor propellants were tested with the ERH, thereby demonstrating aluminum and energetics dissolution and energetics hydrolysis for a full-scale ERH. The ERH demonstration unit was a custom-designed cylindrical drum 4 ft (1.22 m) in diameter ($\frac{1}{2}$ of full scale) and 2 ft (0.61 m) wide filled with 8- to 12-M NaOH, which rotated at the very slow rate of 0.1 rpm. The drum was heated with condensing steam at 212 to 230°F (100 to 110°C) to melt out the energetics and to increase the hydrolysis reaction rate. In the ERH tests, munition pieces were placed into the caustic-filled drum, and the drum was rotated for periods up to 10 hours. Lifting flights in the drum were tilted at an angle to ensure that the energetics rolled off the flight as the flight rotated out of the NaOH solution, thus minimizing the time the energetics were out of solution. Aluminum metal dissolved to form aluminum salts and hydrogen, and the energetics dissolved and reacted with the NaOH to form an energetics hydrolysate.

There were no significant deviations from the planned demonstration testing.

3.2.1.3.5 SCWO – Agent Hydrolysate

SCWO was demonstrated to validate destruction of Schedule 2 and other organic compounds from agent hydrolysis products. Destruction of Schedule 2 compounds is a Chemical Weapons Convention (CWC) requirement, and thus demonstration of the SCWO technology was essential. Testing had previously been performed with VX/NaOH hydrolysate during the ATP

but had not been performed with HD or GB/NaOH hydrolysates. The objectives of the demonstration testing included the following:

- Validate the ability of the solid-wall SCWO to eliminate the Schedule 2 compounds present in the agent hydrolysate feeds;
- Validate the ability of the agent hydrolysis process and the SCWO to achieve a destruction removal efficiency (DRE) of 99.9999% for HD, GB, and VX;
- Demonstrate the long-term operability of the SCWO reactor with respect to salt plugging and corrosion; and
- Characterize the gas, liquid, and solid process streams from the SCWO.

For the SCWO agent hydrolysate tests, mixtures of agent hydrolysate, water, and/or auxiliary fuel (along with air) were fed to the SCWO reactor — a tubular continuous flow reactor operated at approximately 3,400 psia [23 MPa] and 705°F (374°C). In solid-wall SCWO, the injected feed mixture is rapidly heated to supercritical conditions and oxidized to CO₂, water, and inorganic salts. Quench water is injected at the bottom of the reactor to cool the effluent and to dissolve the salts that are insoluble above the critical point of water. The effluent is further cooled in water-cooled heat exchangers and passed through a liquid/gas separator and pressure letdown system. Gaseous effluents are scrubbed in carbon filters and released to the atmosphere. During the demonstration testing, liquid effluents containing soluble and insoluble salts and metal oxides were collected and analyzed. The demonstrated SCWO system operated with a hydrolysate feed rate of approximately 0.1 gal/min (0.38 L/min), which is 1/10 to 1/20 the throughput cited for the full-scale unit.

Significant deviations from the planned demonstration testing included the following:

- SCWO treatment of VX hydrolysate was not demonstrated because of schedule constraints, and
- The proposed platinum-lined reactor was not used because of difficulties in fabrication.

3.2.1.3.6 SCWO – Energetics/Dunnage Hydrolysate

SCWO was demonstrated to validate destruction of organic compounds from energetic hydrolysis products and to show the feasibility of destroying organics in shredded solids.

Characterization of gaseous, liquid, and solid effluents and verification of operating parameters were required.

The objectives of the demonstration testing included the following:

- Validate the ability of the ERH, CSTR, and SCWO to achieve a DRE of 99.999% for tetrytol, Composition B, and M28 propellant;
- Determine the impact of the aluminum from the ERH process on SCWO operation;
- Determine the extent to which the organics in the shredded dunnage are oxidized in the SCWO; and
- Characterize the gas, liquid, and solid process streams from the SCWO.

Energetics hydrolysate and shredded/slurried dunnage (wood, DPE material, butyl rubber, and fresh granulated carbon) were blended and processed through SCWO. In this test, organic products, water, and/or auxiliary fuel (along with air) were fed to a solid-wall SCWO reactor operated at approximately 3,400 psia (23 MPa) and 705°F (374°C). Because of the low heating value of the slurry, electric preheaters were used to heat the slurry prior to injection. In SCWO, the injected feed mixture is rapidly heated under supercritical conditions and oxidized to CO₂, water, and inorganic salts. Quench water is injected at the bottom of the reactor to cool the effluent and to dissolve the salts that are insoluble above the critical point of water. The effluent is further cooled in water-cooled heat exchangers and passed through a liquid/gas separator and pressure letdown system. Gaseous effluents are scrubbed and passed through carbon filters and released to the atmosphere. During demonstration testing, liquid effluents containing soluble and insoluble salts and metal oxides were collected and analyzed. The demonstrated SCWO system operated with a feed rate of up to 0.1 gal/min (0.38 L/min), which is 1/10 to 1/20 the throughput cited for the full-scale unit.

Significant deviations from the planned demonstration testing included the following:

- The proposed platinum-lined reactor was not used because of difficulties in fabrication.
- During some of the SCWO testing, energetics hydrolysates and slurried dunnage were treated in separate runs because of differing effects of feed pre-heating. During the last week of demonstration testing, however, three validation runs were conducted using a mixed feed of tetrytol hydrolysate and slurried dunnage.

- Aluminum hydroxide [Al(OH)₃] was either removed from, or not added to, energetics hydrolysates prior to solid wall SCWO treatment. Reactor plugging occurred while energetics hydrolysate feeds containing Al(OH)₃ were processed.

3.2.1.3.7 Summary of Demonstration Testing

In summary, cryofracture and baseline reverse assembly are well-developed technologies, and, therefore, were not demonstrated. During demonstration testing, the government validated that caustic hydrolysis is effective for destroying agents and energetics. The agent hydrolysis process produces Schedule 2 compounds; however, the solid wall SCWO effectively destroyed all Schedule 2 compounds. The SCWO process effectively treats agent hydrolysates (demonstrated for HD and GB only), energetic hydrolysates, and dunnage, thus producing an effluent of low concern and impact to human health and the environment. Three hydrolysis/SCWO critical unit operations were demonstrated. Salt-plugging and corrosion of the SCWO unit are problems that will require further examination. These problems were to be examined during the engineering design studies (see Section 3.2.1.4). The PMACWA reviews the quality of the data generated during demonstration testing in PMACWA (1999c).

On the basis of demonstration testing, a number of process revisions were proposed that are applicable to PBA and the munitions stored there. Most of these minor revisions relate to the munitions access processes or dunnage treatment. These changes include the following (General Atomics 1999):

- Mortar bursters could not be sheared in the burster size reduction machine (BSRM). However, the tetryl fill in the bursters was found to melt out in the ERH during the demonstration tests. Thus, it appeared that size reduction would not be necessary.
- A live-bottom hopper would be used to collect shredded wood discharged from the low-speed shredder. The hopper would have a screw feeder at the bottom to meter the wood into the hammer mill. This change would prevent overfeeding of the hammer mill and micronizer.
- A separate low-speed shredder and collection hopper would be used to shred and store DPE suits and butyl rubber material before they would be fed to the cryocooler and granulator. This change would allow wood and plastic/rubber materials to be processed independently.
- DPE metal parts would be manually removed in a glove box before the DPE material would be fed to the DSHS. The metal parts would be treated to a 5X condition in the induction-heated batch MPF.

- A colloid mill would be used to wet-grind spent activated carbon to ensure adequate size reduction. The carbon slurry would then be added to the slurried dunnage and hydrolyzed energetics for processing through the SCWO system.
- Hydrolyzed aluminum, as $\text{Al}(\text{OH})_3$, would be filtered from the energetics hydrolysate before being fed to the solid-wall SCWO system. This filtering would prevent hard aluminum salt deposits from plugging the SCWO reactor. The filtered $\text{Al}(\text{OH})_3$ would be dried and decontaminated to a 5X condition in the MPF.

3.2.1.4 Engineering Design Studies¹⁸

Although demonstration testing for the Demo I and Demo II technologies has been completed, Engineering Design Studies (EDSs) are being implemented. The PMACWA determined that these studies were necessary in preparation for full-scale pilot design and permitting. While EDSs have been completed for the Demo I technologies, they have not been completed for the Demo II technologies. This TRD presents information on what was planned for EDSs only.

EDS-I objectives were as follows:

- Provide information for the full-scale facility with respect to total life-cycle cost, schedule, and safety;
- Support the EIS and permit application preparation under RCRA; and
- Support preparation of a RFP for a full-scale pilot-plant facility.

PMACWA (2000a) gives an overview of the planned EDSs for neutralization/SCWO. Figures 3.5 and 3.6 provide overviews of the neutralization/SCWO process and show unit operations that were evaluated during EDSs for projectiles and mortars (Figure 3.5) and for M55 rockets (Figure 3.6).¹⁹

The following subsections summarize planned EDS-I activities.

¹⁸ This material describes EDSs for the technologies evaluated in the Demo I PMACWA program and was derived, in part, from PMACWA (1999a). EDSs for Demo I technologies are designated EDS-I. Because EDSs were intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

¹⁹ No EDSs were conducted specific to the process for land mines.

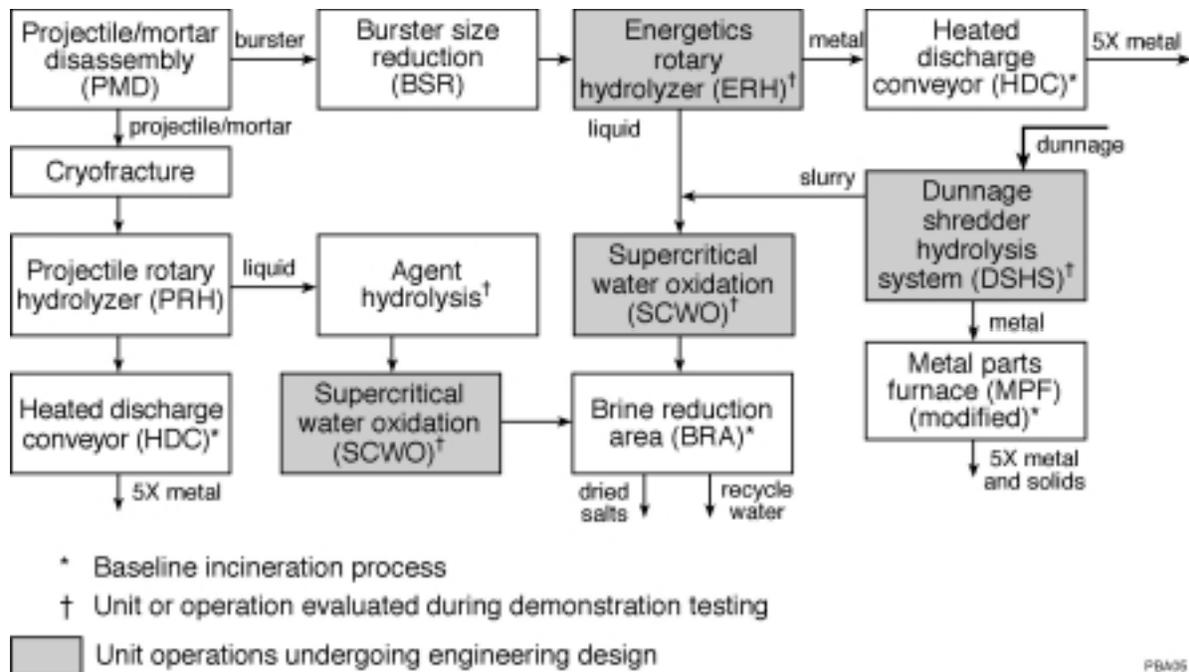


FIGURE 3.5 Flow Diagram of Neutralization/SCWO (General Atomics System) Showing Units or Operations Undergoing Engineering Design — Projectiles and Mortars (Source: Adapted from PMACWA 2000a)

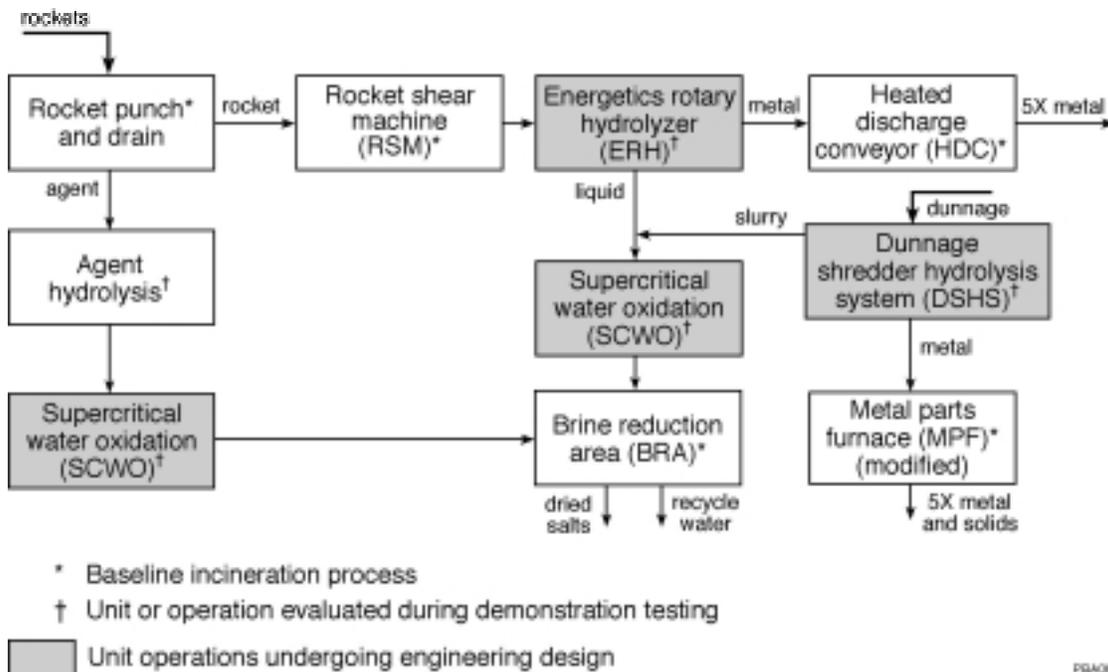


FIGURE 3.6 Flow Diagram of Neutralization/SCWO (General Atomics System) Showing Units or Operations Undergoing Engineering Design — M55 Rockets (Source: Adapted from PMACWA 2000a)

3.2.1.4.1 Energetics Hydrolysis²⁰

Planned EDS activities for energetics hydrolysis consisted of the following:

- Addressing PMACWA and NRC (NRC 2000) concerns regarding particle size, solubility, by-products that would be produced as a function of time, control strategies, mixtures of energetics and caustic concentrations; and
- Acquiring information for scale-up.

3.2.1.4.2 Agent Hydrolysis²¹

Planned EDS activities for agent hydrolysis consisted of the following:

- Determining the potential to use 15% by weight mustard agent hydrolysate for feed to the SCWO unit for increased throughput.

3.2.1.4.3 Energetics Rotary Hydrolyzer

Planned EDS activities for the ERH consisted of the following:

- Observing the effects of M28 propellant hydrolysis for rocket motor lengths measuring less than 12 in. (30 cm) (i.e., 4 plus 8 in. [10 plus 20 cm]) and multiple pieces of rocket motor lengths (4 in. [10 cm]) and comparing them with results during demonstration (12 in. [20 cm]);
- Observe containment of fugitive emissions; and
- Observing the effects of higher caustic concentration and bath temperature (19 M [50 wt%] NaOH, 277°F [136°C]; or highest allowable) on the rate of M28 propellant hydrolysis.

²⁰ This is the same testing program planned for neutralization/biotreatment and also is applicable to neutralization/GPCR/TW-SCWO.

²¹ This is the same testing program planned for neutralization/biotreatment and also is applicable to neutralization/GPCR/TW-SCWO.

3.2.1.4.4 Dunnage Shredder/Hydropulper System

Planned EDS activities for the DSHS consisted of the following:

- Demonstrating changes to the dunnage shredding equipment for the full-scale design and verifying improved efficiency and uninterrupted operation (e.g., avoiding unit overloads), while still meeting original particle size requirements; and
- Generating information required for design of duct emission control system.

3.2.1.4.5 Solid-Wall SCWO (HD and GB Hydrolysate Feed, Composition B/M28 Hydrolysate Feed, and Tetrytol Hydrolysate/Al[OH]₃/Dunnage Feed)

Planned EDS activities for solid-wall SCWO consisted of the following:

- Demonstrating long-term operability without plugging;
- Demonstrating an acceptable corrosion rate;
- Demonstrating that any feed additives for salt transport control do not interact with feed and/or equipment to generate salt plugs or accelerate corrosion;
- Determining a maintenance schedule and shutdown frequency on the basis of the results of long-term testing; and
- Generating data for use in validating the SCWO model development work sponsored by the U.S. Army Research Office.

As indicated previously, the results of the EDSs for neutralization/SCWO were not included in this TRD.

3.2.1.5 Detailed Process Description

This section presents a detailed process description for neutralization/SCWO, as applied to PBA and the ACW stored there, on the basis of the demonstration testing results. The equipment used in a pilot-scale facility may vary in nomenclature and design from that described here, depending on the system selected and system requirements.

Figure 3.7 illustrates the entire neutralization/SCWO process as applied to PBA and the ACW stored there. As the figure shows, the munitions would be accessed with a modified baseline reverse assembly. For rockets, agent would be accessed first by using a punch and drain process. The rocket would then be sheared to access the fuze, burster, and propellant. The land mines are contained in drums, with detached fuzes and activators. The drums would be manually unpacked, and fuzes and activators would be removed from the drums. Then, the agent would be accessed by a punch and drain system. The bursters would be removed and processed along with the fuzes and activators. Following munitions access for rockets and land mines, the process for treating specific agents and energetics would be largely independent of the type of munition.

Caustic hydrolysis using NaOH would be used to neutralize nerve agents and energetics. Munition hardware would be treated with caustic in rotary hydrolyzers (rotating vessels with a helical transport flight²²); the ERH²³ would be used for all rocket and land mine munition components. Drained agents would be neutralized in CSTRs.²⁴ ERH effluent liquids would be treated in similar CSTRs. Dunnage and other organic solid wastes from rockets and land mines would be shredded, pulverized, and pulped in a water/caustic solution (with solids removal) into a slurry hydrolysate. Thermal treatment would be used to decontaminate the solids that are not pulped. Solid effluents from the ERH would pass to modified (inert atmosphere) baseline HDCs for thermal decontamination to a 5X condition. Nonshreddable solid wastes (metals, glass, etc.) would undergo thermal decontamination to a 5X condition in an induction-heated, inert atmosphere MPF. Nonmetal solid waste, if classified as hazardous waste, would be managed as hazardous waste.²⁵ If defined as nonhazardous wastes, these solid wastes may be disposed in a nonhazardous waste landfill.

Agent hydrolysate (independent of agent type), energetics hydrolysate from the ERH, and dunnage slurry hydrolysate would undergo secondary treatment in solid-wall SCWO units. The energetics and the dunnage hydrolysate would be treated in a separate SCWO processing train.

²² A continuous, flat plate (or “flight”) attached to the inner wall of the vessel, forming a corkscrew or augerlike apparatus from one end to the other. Material is moved along the bottom of the vessel by the helical transport as the vessel rotates.

²³ The term ERH is specific to General Atomics. Conceptually, other processes that use a caustic washout design can be substituted for this process.

²⁴ CSTRs were developed pursuant to the U.S. Army’s ATP.

²⁵ Solids treated to remove residual agent may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in Title 40, Parts 260.21 – 260.24 of the *Code of Federal Regulations* (40 CFR 260.21 – 260.24).

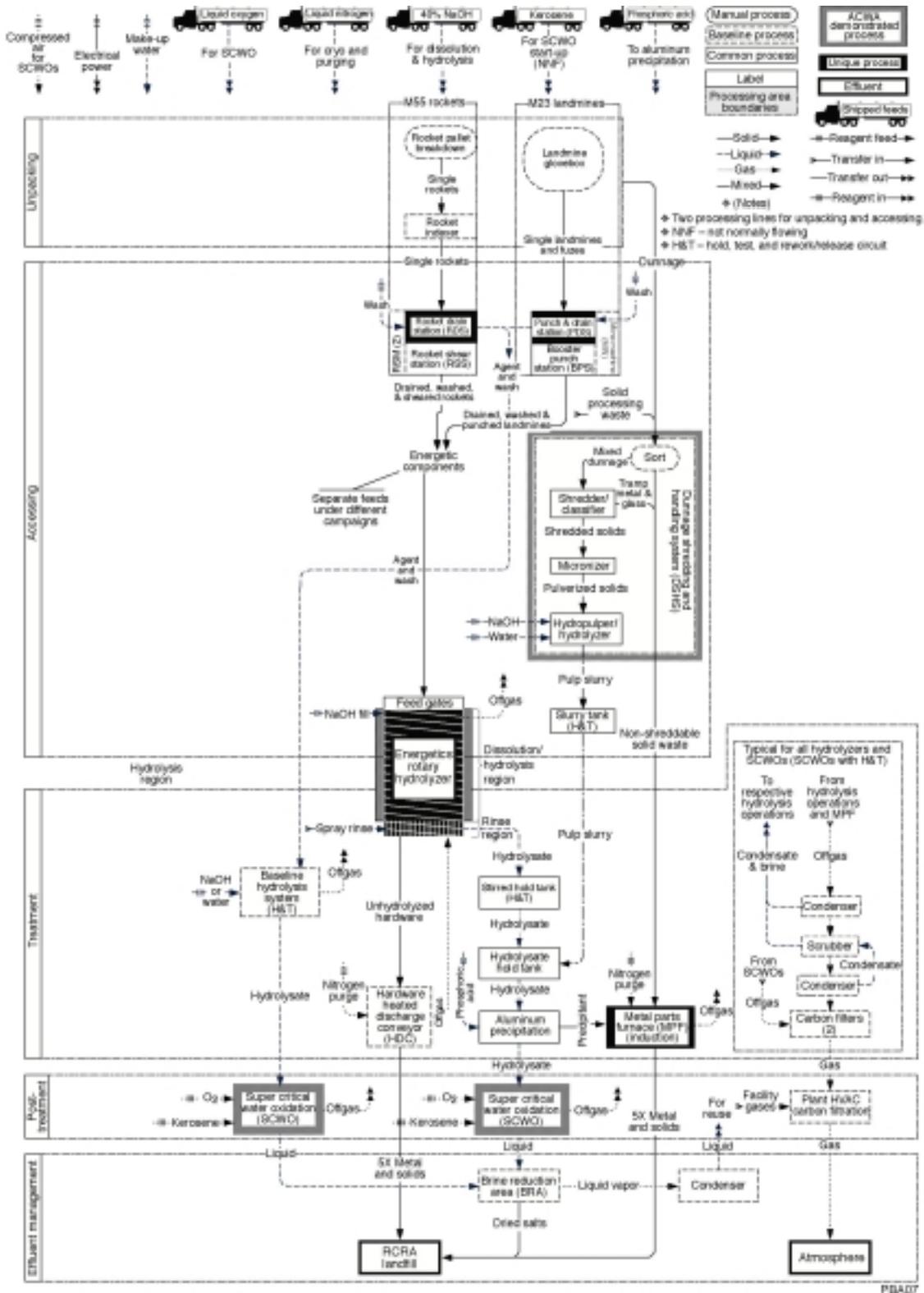


FIGURE 3.7 Flow Diagram of Entire Neutralization/Solid-Wall SCWO Process at PBA (Source: Adapted from PMACWA 1999a,b)

Brine from the SCWO units would be evaporated, the water would be condensed and recycled to the hydrolysis units, and the salts would be sent to a RCRA-permitted hazardous waste landfill.²⁶ The salts may need to be treated prior to placement in a landfill to meet RCRA land disposal requirements. Off-gases from the HDCs would vent to their respective rotary hydrolyzers. Off-gases from the hydrolyzers and the MPF would pass through condensers, scrubbers, and carbon filters before being released to the atmosphere. Liquid from condensers and scrubbers would return to the rotary hydrolyzers for reuse and eventual treatment by SCWO. SCWO off-gas would pass through carbon filters and be released to the atmosphere.

Short descriptions of each of the unit processes included in the neutralization/SCWO process as applied to rockets and land mines stored at PBA are provided below. Because of the differences in the munitions access process for rockets versus land mines, a separate description of the munitions access process is provided. However, the remaining process descriptions (for agent and energetics treatment, metal parts treatment, dunnage treatment, and effluent management and pollution controls) apply to both rockets and land mines. General Atomics (1999), which includes detailed process flow diagrams, may be reviewed for additional details.

3.2.1.5.1 Munitions Access – Rockets

The proposed design for the M55 rockets and the M56 rocket warheads incorporates the following units and processes that are used in the baseline reverse-assembly process (see Appendix E of TRD Volume 1 for details): reverse-assembly machines, material handling conveyors, robotic loaders and handlers, elements of the MPF thermal treatment system, auxiliary systems, and facilities and support systems. Some of these units are slightly modified from the baseline process, but the basic units and operations are retained.

The basic unit used for processing the rockets is referred to as the rocket shear machine (RSM). The RSM is a custom-designed, automated machine with both a punch-and-drain operation and a shear operation. Rockets are clamped in the punch-and-drain station, where the agent cavity is punched and the agent (GB or VX) is drained. The drained agent is pumped to a surge tank prior to hydrolysis. The rocket is then moved to the shear station, where energetics are accessed and reduced in size. One modification from the baseline process that has been instituted is to increase the size and number of the hole-punches to improve agent drainage and increase throughput. A flush system has also been added (using hot water) to wash out the agent cavity. Additional shear cuts will also be made to the rocket motor assembly to improve access to the propellant.

²⁶ These salts may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in 40 CFR 260.21 – 260.24. Typically, these salts contain heavy metals and exhibit the RCRA toxicity characteristic (40 CFR 261.24). In some states, the salts may be regulated as listed hazardous wastes because of their association with chemical agent. If the salts are listed as hazardous wastes, a RCRA delisting petition may be pursued to reclassify the waste as nonhazardous.

3.2.1.5.2 Munitions Access – Land Mines

The proposed design for the land mines incorporates the units and processes used in the baseline reverse assembly process (see Appendix E of Volume 1 for details). Units and processes include reverse assembly machines, material handling conveyors, robotic loaders and handlers, elements of the MPF thermal treatment system, auxiliary systems, and facilities and support systems. Some of these units have been slightly modified from the baseline process, but the basic units and operations have been retained.

The land mines, with detached fuzes and activators, are contained in drums (three mines to a drum). First, the land mines would be removed from the pallet. Individual drums would be transported by using a forklift and mechanical lift to a mine glove box. The glove box would be an air-tight, enclosed area in the explosion-containment vestibule (ECV), where the drums would be manually unpacked. Fuzes and activators would be removed from the drums, and arming plugs would be removed from the mines. The fuzes, activators, and arming plugs would be placed in a fuze box that would be identical in size and shape to the mine casing. The fuze boxes and the land mine casing would then be placed sequentially on a conveyor leading to the explosion-containment room (ECR). The fuze boxes would be fed directly to the ERH. Disassembly of the land mine would continue in the ECR with the mine machine. Here, the land mine would be punched (through its side), and the agent would be drained by gravity and pumped to a holding tank at the toxic cubicle (TOX). Design requirements call for a minimum of 95% of the agent to be drained from the mine. Following draining, the central burster would be removed at the booster push-out station. The burster and the mine body would then be fed separately to the ERH.

3.2.1.5.3 Agent Treatment

The neutralization/SCWO system would incorporate the ATP neutralization system design currently being used at APG, with minor modifications to interface with other equipment. The neutralization system would be independent of the source of the agent (i.e., would process agent from rockets and land mines) and would include six CSTRs and associated support systems. The hydrolysis process used for neutralization/SCWO would be chemically identical to that used for neutralization/biotreatment (see Section 3.2.2) and for neutralization/GPCR/TW-SCWO (see Section 3.2.3); however, the physical processes and equipment used may be different.

Secondary treatment of the agent hydrolysate to remove Schedule 2 compounds would be accomplished by using a solid-wall SCWO unit. The SCWO system for PBA would be sized to process the hydrolyzed agent from the rockets and land mines. The hydrolysate would first be collected in tanks that are sufficiently large to handle 10 hours of continuous operation. A gas-fired preheater and auxiliary fuel system would be used to heat the reactor in the SCWO to the desired operating temperature (705°F [374°C]), and the unit would be maintained at an operating pressure of 3,400 psia (23 MPa). Hydrolysate flow would be initiated, and the auxiliary heat

would be discontinued. Auxiliary fuel and preheat power would not be required under steady-state conditions.

The SCWO system for PBA would be similar to that planned for NCD. The SCWO system would contain components needed to (1) accept and process hydrolysate piped from the hydrolysate holding tanks, (2) release brines to the BRA, and (3) release gaseous effluents to the plant ventilation system.

3.2.1.5.4 Energetics Treatment

The ERH would be the main element for primary treatment of energetics. The ERH is used for both rockets and land mines and treats primarily energetic materials. This unit would process energetics from rockets and land mines in an identical manner. The design of the PBA ERH is slightly larger than the design to be applied at PCD because of the larger throughput rate of energetics that is expected at PBA (i.e., because of the M28 propellant contained in the M55 rockets).

The ERH would replace the baseline DFS; however, it has been adapted to the same interfaces with other equipment as the DFS. The ERH is similar in design and operation to the PRH and receives energetics and metal parts containing energetics from the ECR. The ERH consists of a large rotary drum with an internal helical flight as well as lifting flights. The helical flight transports material along the axis of the drum and maintains batch separation. The lifting flights ensure agitation and mixing of the hydrolyzing solution with the energetics and metal parts. The drum is steam-traced on the outside surface of the drum to maintain an internal operating temperature of 212 to 230°F (100 to 110°C). At this temperature, energetics would be melted and the hydrolysis reaction would be enhanced. The materials would move through the hydrolyzer, where NaOH solution would continually be added at the feed end as energetics and metal parts are discharged by gravity into the drum, along with a flush solution. The helical flight would move a batch of hydrolyzing solution, energetics, and metal parts along the axis of the drum; each batch would contain several feeds of energetics and metal parts. At the discharge end of the hydrolyzer, a perforated section of the drum would permit the hydrolysate to discharge into a CSTR to complete hydrolysis of any remaining small particles of energetics. The hydrolysate would subsequently be pumped to continuously stirred holding tanks. The hydrolysate would then discharge to the energetics hydrolysate/ dunnage hydrolysate SCWO treatment system.

Air would be pulled through the ERH to remove hydrolysis vapors and fumes, including hydrogen produced from the hydrolysis of aluminum that makes up parts of the M55 rockets. Sufficient air flow would ensure that the hydrogen concentration remains well below the lower explosive limit (LEL) for hydrogen. The air would then discharge to an air treatment system consisting of a scrubber, condenser, and carbon filters and would eventually vent through the plant ventilation and carbon filter system.

Secondary treatment of the energetics hydrolysate and dunnage slurry (see dunnage treatment description below) would be accomplished by a solid-wall SCWO unit identical in design and capacity to the agent hydrolysate SCWO system described above. The SCWO units employed would be similar in design to the SCWO units planned for pilot testing at NCD. The major differences would be in the slurry feed and the high-pressure pump system.

3.2.1.5.5 Metal Parts Treatment

The metal parts from energetics treatment (land mine and rocket parts) would continue along the axis of the perforated section of the ERH drum and discharge through a chute to a separate HDC. In the HDC, metal parts would be heated to at least 1,000°F (538°C) for a minimum of 15 minutes. The metal parts would be treated to meet a 5X condition, thus destroying residual agent and energetics. Metal from the DSHS would be decontaminated to a 5X condition in the MPF.

3.2.1.5.6 Dunnage Treatment

Dunnage would be treated during the campaign to the extent possible. Material would be processed by shredding and slurring. The slurried dunnage would then be treated in the energetics hydrolysate/SCWO system. Although not all dunnage would be agent-contaminated, all dunnage would be treated on-site in this manner.

Nonmetallic dunnage materials—wood, paper, plastic, DPE suits, and spent carbon—would be size-reduced in a series of steps and fed to a commercial hydropulper and grinding pump that would slurry the material to a particle size of less than 0.04 in. (1 mm). Wood dunnage would be size-reduced in a dedicated low-speed shredder, hammer mill, and micronizer to achieve a fine particle size suitable for slurring. DPE suits and butyl rubber would be shredded in a dedicated low-speed shredder and then cryocooled and granulated to achieve adequate size reduction. Spent activated carbon would be wet-ground in a dedicated colloid mill. A dilute solution of NaOH would be added to decontaminate the size-reduced solids in the slurry. The resulting slurry would be expected to have a particle content of about 10% by weight. This slurry would then be blended with the energetics hydrolysate. At this point, additives would be used to ensure that the solids remain in suspension and that the slurry can be readily pumped and processed in the energetics SCWO system.

3.2.1.5.7 Effluent Management and Pollution Controls

The effluent management and pollution control systems used in neutralization/SCWO would be similar to systems used in the baseline incineration plant. These systems would be independent of agent and munition type. Elements of the system are described below.

The plant ventilation system is designed with cascading air flow from areas of less contamination potential to areas of more contamination potential. The ventilation system permits room air-change frequencies consistent with area-level designations²⁷ for normal as well as anticipated maintenance activities. Plant ventilation flow would be collected in the main plenum and directed to a bank of carbon filters. From there, the air would be filtered and monitored, passed through induction draft fans, and exhausted to the stack and the atmosphere. This system would be nearly identical to the baseline system.

The decontamination fluid supply system and spent decontamination fluid collection system would be the same as those in the baseline system. Decontamination fluid would be supplied to most rooms in the main plant area, and spent decontamination fluid would be collected in sumps that would be monitored and controlled. The spent decontamination fluid would be transferred to the spent decontamination system (SDS) treatment area, where it may be mixed with additional decontamination solution to ensure the complete destruction of agent.

The DPE supplied air and personnel support system would include maintenance air locks, donning/doffing support equipment, and facilities identical to baseline.

The BRA would be identical to that used in the baseline system except that it will be modified to handle brine salts from the SCWO process and water recovery (by condensation) for reuse in the plant. The BRA includes equipment for effluent drying in heated drums. If classified as hazardous waste, dried salts would be disposed of in a hazardous waste landfill.

The plant instrument air supply and steam supply systems would be identical to those employed in the baseline system.

Control rooms would be the same as those used in the baseline system, with changes as needed to accommodate the new systems and equipment.

The process for transferring munitions from storage to the unpack area would be similar to that used for the baseline system.

Personnel support, monitoring systems, and analytical laboratories would be similar to those used in the baseline system.

As indicated previously, elements of the baseline incineration process are included in the overview of baseline and ACWA system technologies provided in Volume 1 of this TRD (see Section 1.4). The baseline incineration process is also described in Appendix E of Volume 1.

²⁷ Level A, B, C, D, or E indicates the potential for contamination; Level A is highest and E is the lowest.

3.2.1.6 Common Elements – Other Systems

The neutralization/SCWO process has several elements that are identical or nearly identical to those of other systems:

- The munitions access system used for neutralization/SCWO employs much of the baseline reverse assembly system, as do the other ACWA systems.
- Neutralization/SCWO, neutralization/biotreatment, and neutralization/GPCR/TW-SCWO employ neutralization as a primary treatment for chemical agents and energetics.
- Neutralization/SCWO and neutralization/GPCR/TW-SCWO each employ SCWO systems. Although the solid-wall and transpiring-wall SCWO systems differ, they are interchangeable.

Facility structure; ventilation; decontamination fluid supply; personnel support; pollution abatement; water, air, and steam supply systems; control rooms; monitoring systems; and laboratory support would be identical or nearly identical to those employed in the baseline system.

3.2.2 NEUTRALIZATION/BIOTREATMENT

The neutralization/biotreatment technology system consists of neutralization of agents and energetics, and secondary treatment of neutralization residuals using biotreatment. This technology system, proposed by Parsons/Honeywell, is only fully applicable to ACW that contain mustard agent. During demonstration testing, biotreatment of nerve agent residuals (i.e., hydrolysates) was unsuccessful. Because PBA stores only ACW containing nerve agent, the neutralization/biotreatment process is not fully applicable to ACW at PBA. However, non-biotreatment elements of this technology system may be used in addition to or in place of elements of other technologies used in this system for the ACW at PBA that contain nerve agent. The following subsections provide a more detailed discussion of the technologies and processes involved in this system. The technology provider's technology demonstration report (Parsons/Allied Signal 1999) may be viewed for additional detail.²⁸

²⁸ Honeywell purchased Allied Signal in early 2000; General Electric purchased Honeywell in 2000. Parsons/Honeywell refers to its ACWA system as the WHEAT process.

3.2.2.1 Process Overview

Figure 3.8 shows the neutralization/biotreatment process as applied to the rockets and land mines at PBA. A modified baseline reverse assembly process would be used to disassemble munitions. In the proposed Parsons/Honeywell system, modifications would include fluid-abrasive cutting and fluid-mining. Agent would be neutralized/hydrolyzed by using NaOH solutions in units operated at temperatures of 194°F (90°C) and atmospheric pressure; energetics would be neutralized/hydrolyzed using a NaOH solution in units also operated at 194°F (90°C) and atmospheric pressure. Agent and energetic hydrolysates would be biotreated together in aerobic reactors called Immobilized Cell Bioreactors (ICBsTM) and would be supplementally treated with hydrogen peroxide/ferrous sulfate ($H_2O_2/FeSO_4$ [Fenton's reagent]). Metal parts and dunnage would be decontaminated to a 5X condition by using an electrically heated steam furnace. Gaseous discharges would be catalytically converted by using a catalytic oxidation (CatOx) system to remove trace organics, oxidizable nitrogen, and chlorine compounds (NRC 1999) before being discharged to the atmosphere. Emissions from the CatOx system do not require high-efficiency particulate air (HEPA) or carbon filtration (Parsons/Allied Signal 1999).²⁹

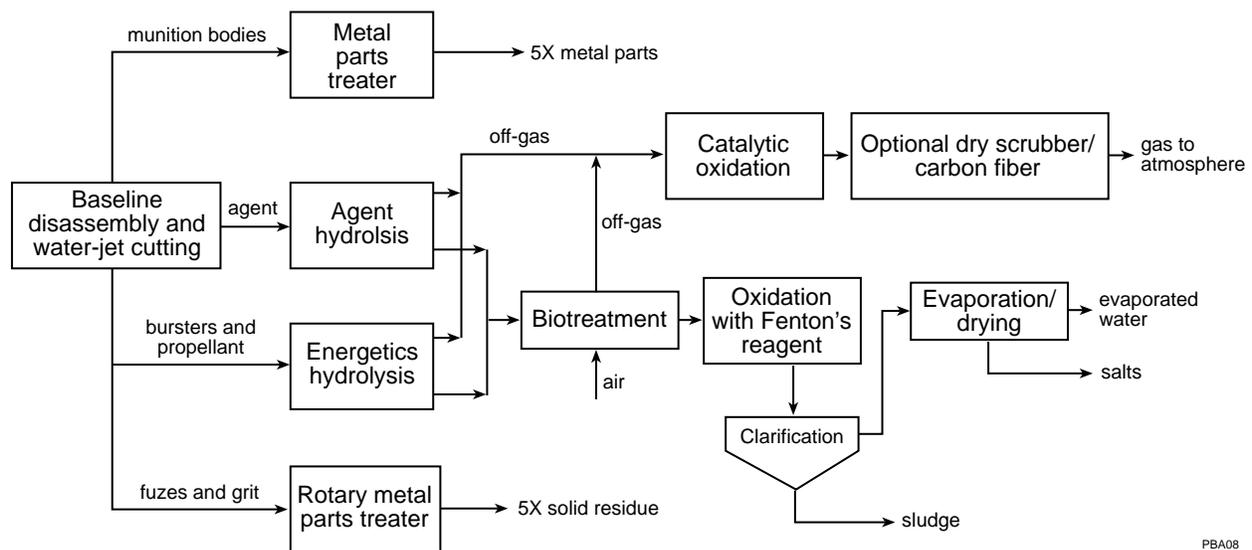


FIGURE 3.8 Overview of the Neutralization/Biotreatment Process for the Treatment of ACW at PBA (Parsons/Honeywell System) (Source: Adapted from NRC 1999)

²⁹ The terms ICB and CatOx are specific to Parsons/Honeywell. Conceptually, other processes that employ similar technologies could be substituted.

The elements of this process that may be used in addition to or in place of elements of other technologies include fluid-abrasive cutting and fluid-mining, 5X treatment of metal parts in an electrically heated steam furnace, and the CatOx system.

The neutralization/biotreatment system includes provisions for treatment of mortars and projectiles and for rockets. The technology provider (Parsons/Honeywell) did not supply any information for land mines.

3.2.2.2 History of Destructive Processes

Neutralization and biotreatment are the primary destructive processes employed in this technology. The histories of these processes are summarized below.

3.2.2.2.1 Neutralization of Agent and Energetics

Agent and energetics neutralization by hydrolysis were reviewed in Section 3.2.1.2.1. Since the history of neutralization of agent and energetics for neutralization/SCWO does not differ from the history of neutralization of agent and energetics for neutralization/biotreatment, this information is not repeated.

3.2.2.2.2 Biological Treatment

Because biotreatment of nerve agent hydrolysates was unsuccessful during demonstration testing, the history of this technology is not discussed here. A more detailed discussion on biotreatment can be found in Volumes 2, 4, and 5 of this TRD (ANAD, PCD, and BGAD, respectively).

3.2.2.3 Demonstration Testing³⁰

The neutralization/biotreatment technology was demonstrated during Demo I of the PMACWA demonstration test program. Demo I testing was conducted in spring 1999. This section provides a summary of demonstration testing for neutralization/biotreatment. Demo I testing results are provided in PMACWA (1999a).

³⁰ This material was derived from PMACWA (1999a) and refers to demonstration testing conducted during Phase I of the ACWA demonstration process. Because demonstration testing was intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

Baseline reverse assembly, carbon filtration, the BRA operations, and other technologies common to baseline operations were not evaluated during the ACWA demonstration testing of neutralization/biotreatment. In addition, the following unit operations proposed for neutralization/biotreatment were not selected by the PMACWA for demonstration for the reasons given below.

Continuous Steam Treater (CST). The CST is a new addition to the proposed full-scale process that was incorporated after demonstration was conducted. It is described as a rotary version of the metal parts treater (MPT).

Dunnage Processing (noncontaminated). The originally proposed noncontaminated dunnage processes (shredding, neutralization, and biotreatment) were not considered pertinent to ACWA mixed munitions demilitarization.

The reasons for selecting the neutralization/biotreatment demonstration unit operations, testing objectives, and significant deviations from the planned testing are described in the following subsections.

3.2.2.3.1 Agent Hydrolysis

The U.S. Army previously demonstrated agent hydrolysis extensively in its ATP. The PMACWA ran agent hydrolysis units primarily to provide representative feedstock for biotreatment and to characterize the intermediate product stream for residual agent, Schedule 2 compounds, and other substances required to verify the mass balance. The specific test objectives of these demonstration units were identical to those for neutralization/SCWO and included the following:

- Design, fabricate, and deliver GB and VX hydrolysate production systems with a production capacity of 100 gal (379 L) of hydrolysate per run;
- Use the hydrolysate recipes developed and tested by the Edgewood Chemical Biological Center (ECBC);
- Demonstrate that the agent concentration in the hydrolysate solution is less than the waste control limit by using the analytical methods developed and approved by the ECBC;
- Characterize solid, liquid, and gas process streams; and
- Provide agent hydrolysate in support of demonstration testing.

GB and VX hydrolysate were produced in a newly constructed 100-gal (379-L) stirred tank reactor at CAMDS. The design and manufacture of a hydrolysis system provided information on equipment and operational parameters that can be used for scale-up to a full-scale facility. VX and GB hydrolysate were produced for use in the ICB units at CAMDS.

HD hydrolysate was produced at the CTF at APG. The equipment used was not intended to be a model for scale-up to a full-scale facility, but was an expedient design suitable for use in the contained environment of the CTF. HD hydrolysate was produced for use in the ICB unit at the ECBC.

There were no significant deviations from the planned demonstration testing.

3.2.2.3.2 Energetics Hydrolysis

Other government agencies have previously evaluated energetics hydrolysis; however, further knowledge of the process was needed for evaluation, feedstock for biotreatment was required, and the characterization of the intermediate product streams for residual energetics and other substances was required to verify the mass balance. The specific test objectives for the demonstration units were identical to those for neutralization/SCWO and included the following:

- Produce energetics hydrolysate for use as feed in subsequent demonstration testing;
- Characterize solid, liquid, and gas process streams; and
- Gather process operation information to support the ACWA program and future scale-up.

M28 propellant was hydrolyzed with 6% NaOH to produce hydrolysate in one production run at the Radford Army Ammunition Plant, in Radford, Virginia. Composition B and tetrytol were hydrolyzed by using 6% NaOH at the Pantex Plant in Amarillo, Texas, and used as feedstock for the ICBs.

There were no significant deviations from the planned demonstration testing.

3.2.2.3.3 Rocket-Cutting and Fluid-Mining

Fluid-abrasive cutting and fluid-mining are reasonably well-established industrial operations; however, the ability to cut through the materials in an M55 rocket was not the

primary reason for demonstrating these operations. Rather, one reason for demonstrating these operations was to verify their application to accessing energetics in the ACW components. Another reason concerned adaptation of fluid-abrasive cutting to the baseline reverse assembly equipment. Fabrication of robotics for automating fluid-abrasive cutting was not viewed as a requirement; demonstrating the effectiveness of the system to access, extract, and wash out energetics, however, was required. In addition, characterization of the quantity and type of grit required, fluids produced, energetics remaining in the rocket, and the size distribution of energetic particles from rocket access and washout was considered important.

The rocket-cutting and fluid-mining unit operation was designed to demonstrate the fluid-abrasive cutting and fluid-mining of M55 rocket energetic components. The objectives of this demonstration unit included the following:³¹

- Demonstrate the ability to perform circumferential cuts of a rocket at required locations along the rocket length;
- Demonstrate effective fluid-mining and separate collection of rocket bursters, motor propellants, and residual agent simulant;
- Demonstrate the ability to maintain control of rocket metal and plastic parts from cutting and fluid-mining operations;
- Determine energetic particle size of fluid-mined rocket bursters and propellant; and
- Determine the requirements for separating used grit from the residual cutting solution.

The demonstration tests were conducted with ten 115-mm inert M60 rockets, which were filled with concrete and plaster of paris, and ten M61 rockets, which are identical to the M55 rockets but filled with ethylene glycol rather than agent. The demonstration unit employed fluid-abrasive cutting to remove the fuzes and cut the rocket casing, fluid-mining to wash out the burster energetics, and fluid-mining to remove the propellant. However, fluid-mining to remove the propellant was terminated prior to the start of validation testing.

Several aspects of the proposed fluid-abrasive, fluid-mining, or wash-out operations that the PMACWA had considered demonstrating were not included in the final demonstration testing matrix: fuze washout, fluid-abrasive cutting of mortars, and use of the process effluents

³¹ These objectives are potentially applicable to land mines stored at PBA.

for subsequent unit feeds. These items were determined to be unnecessary for a successful demonstration. Energetics in these items are expected to melt out in the MPT or CST.

3.2.2.3.4 Immobilized Cell Bioreactor and Catalytic Oxidation

Because biotreatment of nerve agent hydrolysates was unsuccessful during demonstration testing, this technology is not discussed here. A more detailed discussion on biotreatment can be found in Volumes 2, 4, and 5 of this TRD (ANAD, PCD, and BGAD, respectively). Three CatOx units were included as part of the ICB unit operation (one for each ICB). The CatOx units were included to validate their performance with the ICB gaseous effluent and to allow a detailed characterization of product gases for final treatment. The specific goals of demonstration testing for the CatOx units were as follows:

- Validate the ability of the CatOx to eliminate the volatile organic compounds (VOCs), semivolatile organic compounds (SVOCs), and Schedule 2 compounds specified in the Demonstration Study Plan from the ICB process gas streams;
- Determine the potential impact of operating conditions on the fouling and plugging of the CatOx; and
- Characterize the gas, liquid, and solid waste streams from the unit operations for the constituents specified in the Demonstration Study Plan.

Although CatOx testing was included as part of the ICB unit operation, this testing is pertinent to nerve agent stored at PBA, and, therefore, is included here.

3.2.2.3.5 Metal Parts Treater and Catalytic Oxidation

The MPT is a thermal treatment unit that decontaminates metal parts and dunnage to a 5X condition by maintaining the temperature above 1,000°F (539°C) for the required time (minimum of 15 minutes). The ability of the MPT to effectively treat metal parts to a 5X condition was not a primary reason for demonstrating the unit; it was demonstrated because of several issues raised during the initial evaluation. These issues included the ability to treat dunnage, the ability to control the agent driven from metal parts, and the need to characterize products for all process streams.

Because of the lack of information on the effluents from the MPT, it was considered important to test the unit with as many different feeds as possible. Therefore, the MPT was demonstrated by using mortar bodies containing a quantity of agent representing a 10% heel of

GB, VX, and HD. This was considered a worst-case scenario on the basis of the original approach of washing out the projectiles. The MPT was also tested with carbon, pentachlorophenol (PCP)-contaminated wood, fiberglass from rocket shipping and firing tubes, and DPE suit material.

Part of the gaseous effluent treatment for the MPT includes another CatOx unit followed by carbon filters. The most important reason for conducting the MPT demonstration was to characterize the effluents from the MPT. CatOx demonstration was also considered important because this unit has the potential to extend the life of carbon filters in a variety of demilitarization applications. If the MPT were to produce agent or Schedule 2 compounds in the gas phase, the CatOx could treat them; validation of this capability was a reason for the demonstration. A direct challenge of undiluted agent was considered the ultimate test of this unit; therefore, HD, VX, and GB were all directly fed into the unit to determine the ability of the CatOx unit to destroy any agent volatilized in the MPT.

The MPT unit operation demonstration was designed to test the capabilities of the MPT, its associated condensate recovery system (CRS), and the attached CatOx. The objectives of these demonstration units included the following:

- Validate the ability of the MPT process to treat dunnage;
- Determine what pyrolysis products are produced in the MPT during processing of dunnage and evaluate their impact on the downstream condenser;
- Characterize the liquid effluent from the MPT condenser to determine its suitability for processing in the agent hydrolysis reactor;
- Validate the ability of the MPT condenser and the CatOx to eliminate chemical agents and Schedule 2 compounds from the process gas stream;
- Determine the potential impact of operating conditions on fouling and plugging of the CatOx; and
- Characterize the gas, liquid, and solid waste streams from the MPT for the constituents and properties specified in the Demonstration Study Plan.

The MPT unit operation was tested with the following:

- M2A1 mortar body with 10% liquid agent heel,

- Wood pallet material spiked with 0.4% PCP,
- Carbon,
- Fiberglass shipping and firing containers, and
- Double-bagged DPE suits with boots and gloves.

The CatOx portion of the unit was also tested with direct GB, VX, and HD vapor feed.

There were no significant deviations from the planned demonstration testing.

3.2.2.3.6 Summary of Demonstration Testing

The neutralization/biotreatment system for fluid-abrasive cutting and fluid-mining was, for the most part, demonstrated during the demonstration test phase. M28 propellant, however, present only in M55 rockets, could not be adequately removed from munition items using fluid-mining. An alternative proposal is to push or pull the M28 propellant grain out of the rocket motor casing. The grain would then be sheared and shredded to produce a slurry. The destruction of agents and energetics by hydrolysis was validated during government testing. Use of hydrolysis, along with the thermal treatment of metal parts and other solid wastes, has been validated to effectively treat mustard agent and the energetic components of ACW. The agent hydrolysis process does, however, produce CWC Schedule 2 compounds. For munitions containing mustard agent, these Schedule 2 compounds were effectively treated in the ICB unit. The process of neutralization followed by biotreatment for the demilitarization of ACW containing mustard agent was validated during demonstration. Therefore, this process is considered a viable total solution for the demilitarization of ACW containing mustard agent. The process of neutralization followed by biotreatment for the destruction of ACW containing nerve agent was not validated during demonstration. Therefore, without further development, this process is not considered a viable total solution for the destruction of ACW containing nerve agent. The PMACWA reviews the quality of the data generated during demonstration testing in PMACWA (2001d).

On the basis of demonstration testing, Parsons/Honeywell indicated that a number of subsequent studies would be needed to optimize system components and to integrate them with baseline components that are included in the total system (Parsons/Allied Signal 1999). Process revisions, however, specifically applicable to PBA and the munitions stored there, were not proposed. Again, because biotreatment was not demonstrated for nerve agent, only those elements of this technology other than biotreatment are considered applicable to the ACW stored at PBA.

3.2.2.4 Engineering Design Studies³²

Although demonstration testing for the Demo I and Demo II technologies has been completed, EDSs are being implemented. The PMACWA determined that these studies were necessary in preparation for full-scale pilot design and permitting. While EDSs have been completed for the Demo I technologies, they have not been completed for the Demo II technologies. Thus, this TRD presents information on planned EDS studies only. EDS-I objectives were as follows:

- Provide information for the full-scale facility with respect to total life-cycle cost, schedule, and safety;
- Support preparation of the EIS and RCRA permit applications; and
- Support preparation of a RFP for a full-scale pilot plant facility.

PMACWA (2000a) provides an overview of the planned EDSs for neutralization/biotreatment. Figure 3.9 provides an overview of the neutralization/biotreatment process and shows unit operations that were evaluated during EDSs for projectiles and mortars. It is unclear whether carbon filtration would be employed in the final pilot-scale design. For demonstration and EDS testing, the carbon filter was employed as a safeguard because of uncertainty regarding performance of the CatOx system.

The following subsections discuss the EDS activities that were planned.

3.2.2.4.1 Energetics Hydrolysis³³

Planned EDS activities for energetics hydrolysis consisted of the following:

- Addressing PMACWA and NRC (NRC 2000) concerns regarding particle size, solubility, by-products that would be produced as a function of time, control strategies, mixtures of energetics, and caustic concentrations; and
- Acquiring information for scale-up.

³² Because neutralization/biotreatment was not demonstrated for nerve agents, EDSs for neutralization/biotreatment focused on ACW containing mustard agent. However, nonbiotreatment components of this technology system may be applicable to ACW containing nerve agent.

³³ This is the same testing planned for neutralization/SCWO and also is applicable to neutralization/GPCR/TW-SCWO.

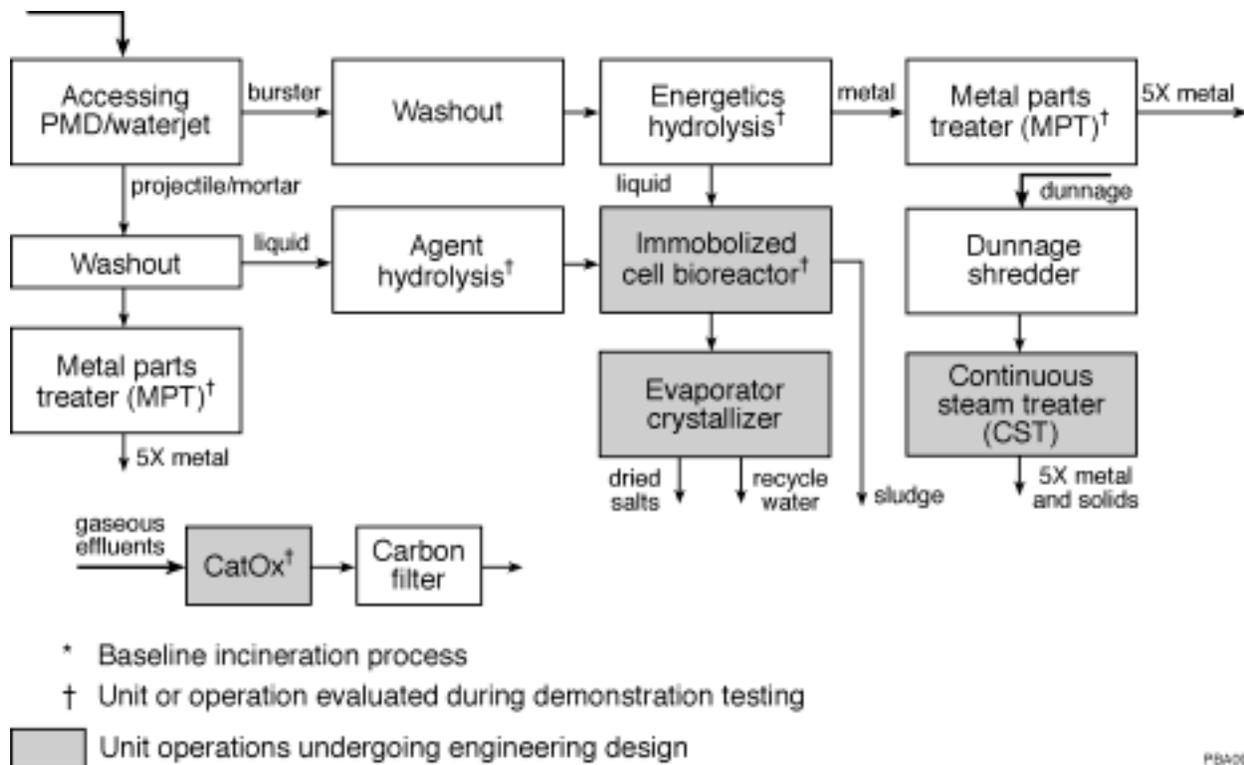


FIGURE 3.9 Flow Diagram of Neutralization/Biotreatment (Parsons/Honeywell System) Showing Units or Operations Undergoing Engineering Design — Projectiles and Mortars (Source: Adapted from PMACWA 2000a)

3.2.2.4.2 Agent Hydrolysis³⁴

Planned EDS activities for agent hydrolysis consisted of the following:

- Determining the potential to use 15% by weight mustard agent hydrolysate for feed to the ICB unit for increased throughput.

3.2.2.4.3 Immobilized Cell Bioreactor and Catalytic Oxidation

Biotreatment of nerve agent hydrolysates was unsuccessful during demonstration testing. This technology is not applicable to ACW containing nerve agent. A more detailed discussion of biotreatment can be found in Volumes 2, 4, and 5 of this TRD (ANAD, PCD, and BGAD, respectively). EDSs for the CatOx unit that may be used in any technology system focused on

³⁴ The same testing is planned for neutralization/SCWO and also is applicable to neutralization/GPCR/TW-SCWO as well.

confirming critical design parameters (e.g., aeration rate, CatOx loading) developed during demonstration testing.

3.2.2.4.4 Continuous Steam Treater (CST) and Catalytic Oxidation (CatOx)

Planned EDS activities for the CST and CatOx consisted of the following:

- Observing the long-term operability, reliability, and ease of material handling of the CST with wood (pallets), DPE suits, and carbon (filter trays);
- Observing the effectiveness of the proposed full-scale control strategy for the CST;
- Observing the ability of the CST to reach a 5X condition throughout the feed material;
- Verifying critical design parameters (e.g., temperature, steam flow rate, CatOx loading, feed throughput rate) developed during demonstration testing;
- Observing the ability of the CatOx unit to effectively treat the uncondensed gases over long-term operation.
- Determining the expected CatOx catalyst life under continuous CST operation; and
- Characterizing neutralized CST condensate for selected chemical constituents and physical parameters and the presence or absence of hazardous and toxic chemicals, including Schedule 2 compounds.

3.2.2.4.5 Catalytic Oxidation Unit

Planned ESD activities for the CatOx unit consisted of the following:

- Observing the long-term (500 hours) operation of the CatOx unit with HD,
- Determining whether the CatOx unit catalyst loses efficiency (as a result of poisoning, fouling, and/or plugging),

- Determining the expected CatOx catalyst life under continuous HD operation, and
- Determining (via characterization) the ability of the CatOx effluent to be treated by a downstream carbon bed.

Additional testing of the neutralization/biotreatment system was planned during EDSs and included the following:

- Water washout of mustard agent projectiles,
- Biotreatment of propelling charge hydrolysate, and
- MPT treatment of inert hardware.

The results of the EDSs for neutralization/biotreatment were not included in this TRD.

3.2.2.5 Detailed Process Description

During demonstration testing, biotreatment of nerve agents was unsuccessful. Because PBA stores only ACW containing nerve agent, the neutralization/biotreatment process is not applicable to ACW at PBA. However, nonbiotreatment elements of this system may be used in addition to or in place of elements of other technologies. For this reason, elements of the neutralization/biotreatment system that may be used in conjunction with rockets and other technologies are discussed.³⁵

Figure 3.10 illustrates the entire process flow for the neutralization/biotreatment process. The process for projectiles and mortars (not present at PBA) and for rockets is shown. Only the portions of the diagram that are applicable to rockets are pertinent to PBA. As shown in this figure, the rocket drain station (RDS) would be used to access and drain the agent cavity. Fluid-abrasive cutting and fluid-mining would be used to access the propellant and other energetic components. Propellant grain would be reduced in particle size by using the propellant macerator device.

Munition hardware (e.g., fuzes), dunnage, and other solid wastes would be thermally decontaminated to a 5X condition in either the MPT, an inductively heated vessel with a

³⁵ The technology provider (Parsons/Allied Signal) did not propose a process for land mines.

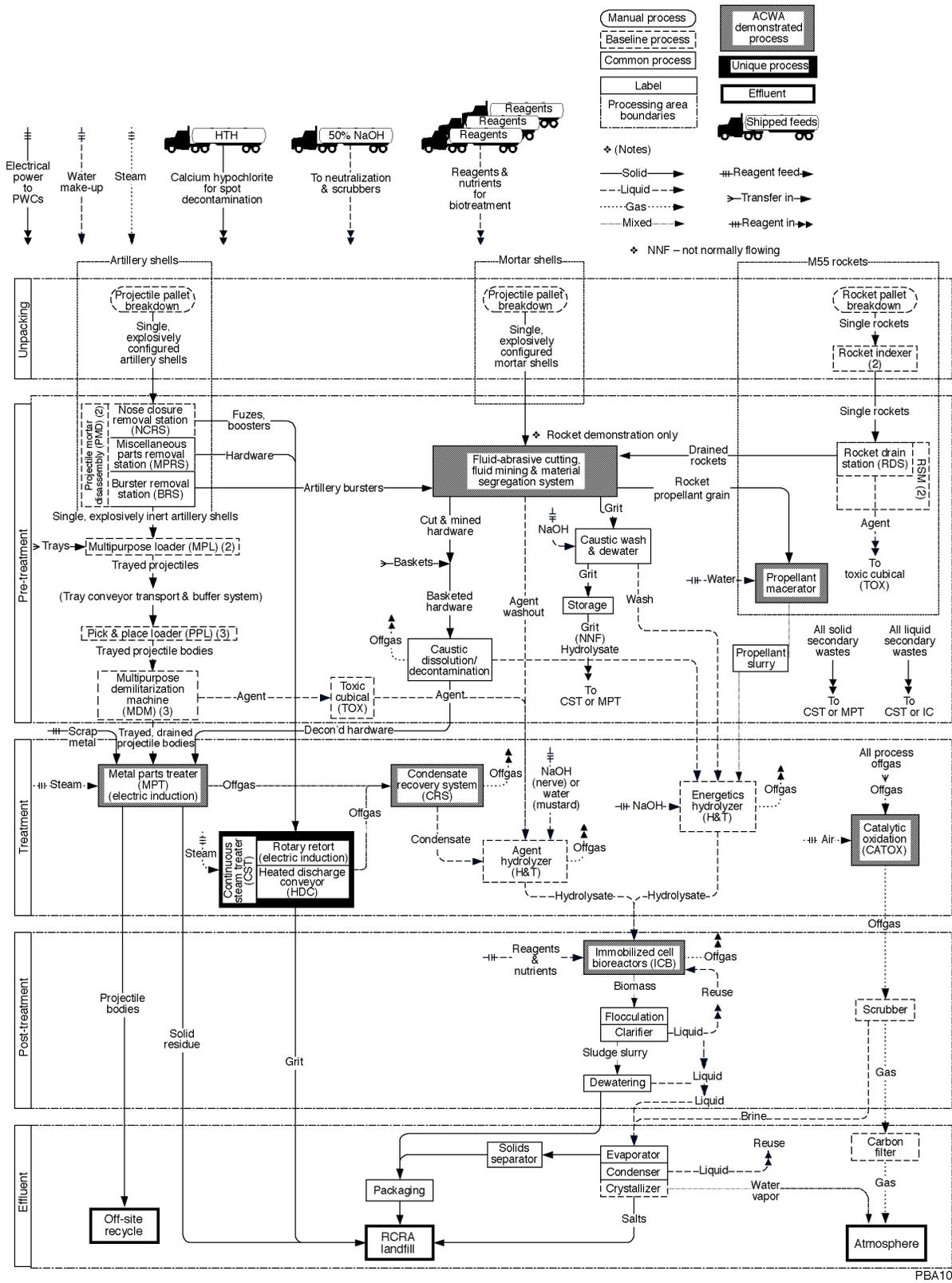


FIGURE 3.10 Flow Diagram of Entire Neutralization/Biotreatment Process at PBA (Adapted from PMACWA 1999b)

superheated steam reactive environment, or the CST, a rotary version of the MPT with a structure similar to that of the baseline DFS. Steam would be condensed from the MPT or CST off-gas and sent to the CRS. NaOH solutions would be used to neutralize nerve agents and energetics in CSTRs, similar to the U.S. Army's ATP process. Drained agents and CRS effluents would be treated in the agent hydrolyzer, while slurried energetics (from cutting, mining/washing) and spent abrasive wash would be treated in the energetics hydrolyzer.

Agent and energetic hydrolysates would be adjusted for pH, combined, and mixed with reagents and premixed nutrients for aerobic digestion (biotreatment) in the ICB. As indicated previously, biotreatment has not been demonstrated for nerve agent hydrolysates.

All process off-gas would be mixed with air and catalytically converted by the CatOx technology, followed by release to the atmosphere. Oxidized liquid and scrubber brine would be dried in the following process: they would first be concentrated by evaporation, the water would be condensed and reused, the remaining material would be crystallized, water vapor would be released to the atmosphere, and dry salts would be sent to a RCRA facility for further treatment, if necessary, and disposal. Treated munition bodies (5X condition) could be commercially recycled, and treated solid wastes (3X or 5X condition) would be disposed of as either hazardous or nonhazardous waste, depending on regulatory requirements.

Short descriptions of each of the unit processes included in the neutralization/biotreatment system that may be applicable to rockets are provided below. As indicated previously, only those nonbiotreatment elements of the neutralization/biotreatment process that may be used in conjunction with rockets are discussed. Parsons/Allied Signal (1999), which includes detailed process flow diagrams, may be viewed for additional detail.

3.2.2.5.1 Munitions Access – Rockets

The proposed design for munitions access for rockets incorporates the units used in baseline reverse assembly (see Appendix E of Volume 1 for details). Units include reverse-assembly machines, material handling conveyors, robotic loaders and handlers, HDCs, elements of the MPF thermal treatment system, auxiliary systems, and facilities and support systems. Some of these units have been slightly modified from the baseline process, but the basic unit and operations have been retained. The major units are summarized below.

Rockets would be disassembled while still in their shipping/firing tube. A rocket would be placed in the rocket indexer, which would position the rocket for the RDS. At the RDS, the agent cavity would be punched, and the agent would be drained. The fuze would be separated from the rocket, and the rocket propellant would be accessed. Fluid-mining, using high-pressure hot water, would remove the burster energetics. Propellant would be pushed out of the propellant cavity, further reduced in size, and slurried by the propellant macerator device.

The fuzes and other solid components would be sent to the MPT or the rotary version of the MPT, the CST. Agent would be transferred by conveyor to holding tanks in the TOX, where it would be stored prior to introduction to the agent hydrolyzer. Energetics washout would be conveyed to the energetics hydrolyzer.

3.2.2.5.2 Agent Treatment

An agent hydrolyzer would be used for agent treatment. Hydrolysis would be conducted in a CSTR, which is similar to the unit used for energetics treatment. The feed would be added to the CSTR, which would contain water at the required reaction temperature. Batches would be adjusted, as necessary, and then released to storage prior to biotreatment. The neutralization technology would incorporate the ATP neutralization system design that will be used at APG, with minor modifications to interface with other equipment. It would be chemically identical to that used in neutralization/SCWO (see Section 3.2.1) and in neutralization/GPCR/TW-SCWO (Section 3.2.3).

Secondary treatment of the agent hydrolysate to remove Schedule 2 compounds would be accomplished using biotreatment. Both the agent hydrolysate and energetics hydrolysate would be treated in the same bioreactor. Because biotreatment of nerve agent hydrolysate was not demonstrated during the demonstration testing, it is not discussed further here.

3.2.2.5.3 Energetics Treatment

The energetics hydrolyzer would be the main element for primary treatment of energetics. The energetics hydrolyzer would replace the baseline DFS but has been adapted to the same interfaces with other equipment as the DFS. The energetics hydrolyzer would be similar in design and operation to the agent hydrolyzer and would receive washed-out energetics from the multistation fluid-accessing machine.

The feed would be added to the hydrolyzer, which would contain NaOH solution at the required reaction temperature. After the required reaction time, a sample of the hydrolysate would be taken and analyzed for agent and energetics. Batches would be additionally treated, as necessary, and then released to storage prior to biotreatment. As indicated above, biotreatment is not discussed further.

3.2.2.5.4 Metal Parts Treatment

The metal parts from munitions access would be processed in the MPT, which would either be a tube-type or rotary device that is induction heated. In the MPT, projectile and mortar

bodies would be decontaminated to a 5X condition in a superheated steam atmosphere. Induction coils would be used to ramp up the temperature through a prescribed cycle. Volatile liquids would be vaporized and removed by the steam, which would be condensed downstream in the CRS.

The liquid condensate from the CRS would be transferred to the SDS, where it would be diluted with a low-concentration alkaline solution of the spent decontamination fluid and subsequently added as makeup water to the agent hydrolyzer. Noncondensable gases would be processed through catalytic converters (the CatOx system).

Energetic hardware — specifically, fuzes, nose closure plugs, projectile burster casings, and fuze booster cups — would be processed through a similar device, the CST. As indicated previously, this unit would be a modified version of the MPT and can operate in continuous feed mode.

3.2.2.5.5 Dunnage Treatment

Dunnage would be treated during the campaign to the extent possible. The dunnage would be thermally treated in a steam atmosphere in the MPT. Although not all dunnage would be agent-contaminated, all dunnage would be treated on-site in this manner.

3.2.2.5.6 Effluent Management and Pollution Controls

The effluent management and pollution control systems used in neutralization/biotreatment would be similar to those used in the baseline incineration plant (see Appendix E of Volume 1). Included are scrubbers, condensers, and carbon filters, which would be used to remove residual organics from contaminated areas prior to discharge to the atmosphere. The neutralization/biotreatment system would also include a CatOx system, which would be used to treat organic constituents within the air stream.

Incoming air streams would be heated electrically to reduce moisture and to condition the gas to the CatOx operating temperature. The catalytic matrix within the device is designed to reduce organic materials to basic elements. The CatOx unit used in the neutralization/biotreatment process may vent to the scrubber/carbon filter system.

All other systems would be identical to the baseline system, including the supplied air and personnel support systems, the plant instrument air supply and steam supply systems, control rooms, the process for handling ACW from storage to the facility, personnel support, monitoring systems, and the analytical laboratories.

3.2.2.6 Common Elements – Other Systems

The neutralization/biotreatment process has several elements that are identical or nearly identical to those of other systems. Commodities with other applicable technology systems include the following:

- The munitions access system used for neutralization/biotreatment employs much of the baseline reverse assembly system, as do the other ACWA systems.
- Neutralization/SCWO (see Section 3.3.2), Neutralization/biotreatment (see Section 3.2.2), and neutralization/GPCR/TW-SCWO (see Section 3.2.3) systems employ neutralization of chemical agents and energetics.
- The neutralization/biotreatment process and the electrochemical oxidation process each employ fluid-abrasive cutting and fluid-mining to access munitions. In addition, both technology systems employ superheated steam treatment for metals and solids treatment to achieve a 5X condition.
- The neutralization/biotreatment, neutralization/GPCR/TW-SCWO, and electrochemical oxidation processes each employ the catalytic oxidation technology as well.

Facility structure; ventilation; decontamination fluid supply; personnel support; pollution abatement; water, air, and steam supply systems; control rooms; monitoring systems; and laboratory support would be identical or nearly identical to the baseline system.

3.2.3 NEUTRALIZATION/GPCR/TW-SCWO

The neutralization/GPCR/TW-SCWO technology system consists of neutralization of agents and energetics, gas-phase chemical reduction of solids and gases, and secondary treatment of neutralization residuals using transpiring wall (TW) supercritical water oxidation (SCWO). This technology is applicable to all ACW stored at PBA, including both rockets and land mines. These ACW contain nerve agent only (GB and VX). No ACW at PBA contain mustard agent.

This technology system was proposed by Foster Wheeler/Eco Logic/Kvaerner (2000).³⁶ While the PMACWA and the technology provider supplied detailed information regarding

³⁶ Foster Wheeler, Eco Logic, and Kvaerner were originally part of a larger team under the coordination of Lockheed Martin (PMACWA 1997, 2001a). Lockheed Martin is no longer part of the technology provider team.

application of this technology to rockets, no information was presented regarding application of this technology to land mines. Similarly, the PMACWA demonstration testing did not address land mines in particular. It is assumed that munitions access for the land mines would follow the baseline or a modified baseline munitions access process. Following munitions access, treatment of agent and energetics from the land mines is assumed to follow a process similar to that for removing agent and energetics from the rockets.

The following subsections provide a more detailed discussion of the technologies and processes involved in this system. The technology provider's technology demonstration report (Foster Wheeler/Eco Logic/Kvaerner 2000) may be viewed for additional detail.

3.2.3.1 Process Overview

The neutralization/GPCR/TW-SCWO process, as applied to rockets and land mines stored at PBA, is summarized in Figure 3.11. The rockets at PBA would be disassembled using a modified baseline reverse assembly process. The baseline RSM would be used; however, it has been modified (MRSM) for this application. Agent would be drained from the rockets using a punch and drain process. Then, the rocket would be sheared to access the fuze and burster. A tube cutter would be used to section the fiberglass rocket firing tube just forward of the threads of the fin assembly, and the fin assembly would be unscrewed to access the propellant. Propellant would be pulled from the rocket motor, size-reduced in a grinder, and slurried. As indicated above, the treatment process for land mines using this technology system was not addressed. It is expected, however, that a process similar to the baseline process would be used to access agent and energetics in the land mines (See Appendix E of Volume 1).

Munitions casings and other hardware would be processed through the Continuously Indexing Neutralization System (COINS™). Using this system, munition casings and other solids would be placed in hanging baskets that are dipped in caustic baths to separate the energetics from metal parts, followed by spray washing.

The drained nerve agents (GB and VX) would then be neutralized/hydrolyzed by using a NaOH solution in systems operated at 194°F (90°C) and atmospheric pressure. Energetics would also be neutralized/hydrolyzed by using a caustic solution, in systems also operated at 194°F (90°C) and atmospheric pressure. Hydrolysates would be treated in a TW-SCWO unit. TW-SCWO differs from solid-wall SCWO (see Section 3.2.1) in that a boundary layer of clean water is dispersed from the sides of the SCWO unit as a means of limiting corrosion and solids buildup (Foster Wheeler/Eco Logic/Kvaerner 2000). TW-SCWO also differs from the solid wall unit in that the TW-SCWO can treat agent and energetic hydrolysates simultaneously.

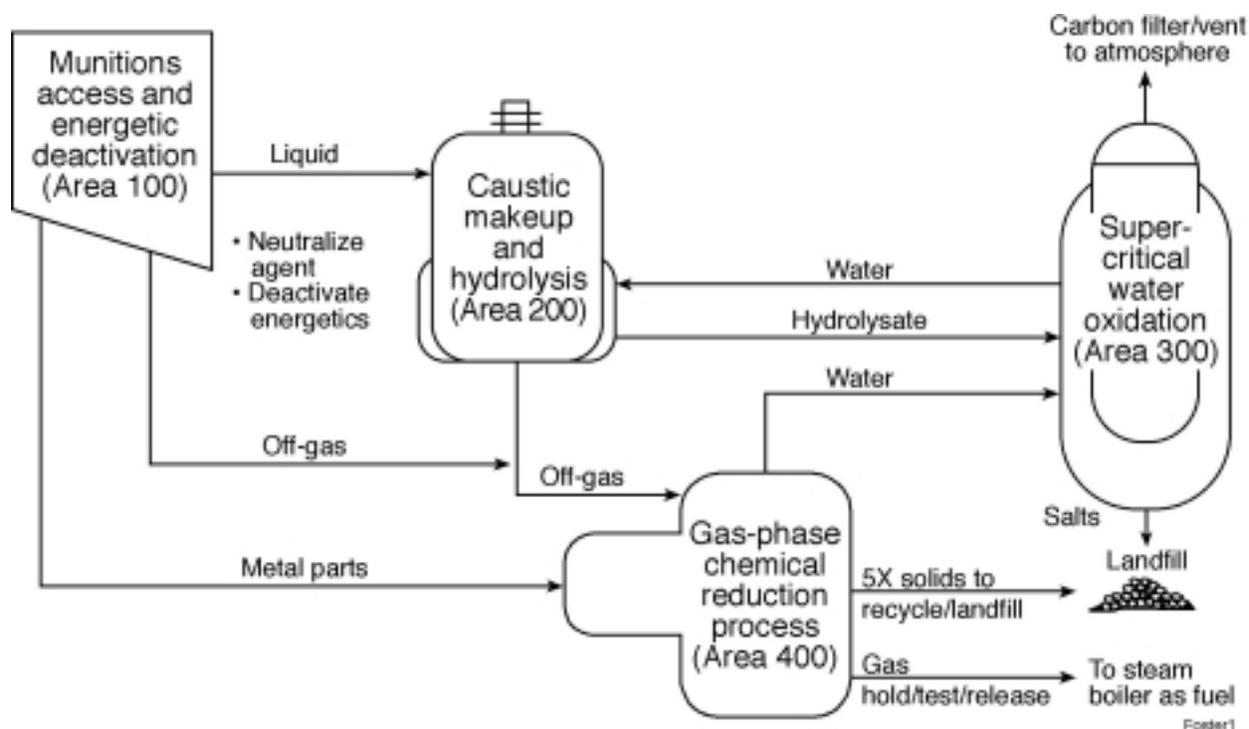


FIGURE 3.11 Overview of Neutralization/GPCR/TW-SCWO Process (Foster Wheeler/Eco Logic/Kvaerner System) for the Treatment of ACW at PBA (Source: Adapted from NRC 1999)

Dunnage and metal parts (e.g., from COINS) would be treated using GPCR. GPCR is a thermal system operated at temperatures above 1,560°F (850°C) that uses hydrogen in a steam atmosphere to reduce organic compounds to methane (CH₄), CO₂, carbon monoxide (CO), and acid gases. The system includes solids treatment in a thermal reduction batch processor (TRBP), which uses a flame-heated batch evaporator to volatilize organic materials to the main GPCR reactor. The TRBP treats metal parts and dunnage to a 5X condition.³⁷ A batch or continuous mode TRBP may be employed, depending on the nature of the munitions being treated. The technology provider indicates that recovered gas from the GPCR may be able to be used as auxiliary fuel for a steam boiler or industrial furnace (BIF) (NRC 1999). (See Section 3.3.5.3.4 for information on recovered gas content.)

Each of these operations is performed in a different area of the destruction facility, as shown in Figure 3.12.

³⁷ The definition of 5X is provided in Volume 1 of this TRD (see Section 1.2.2.4).

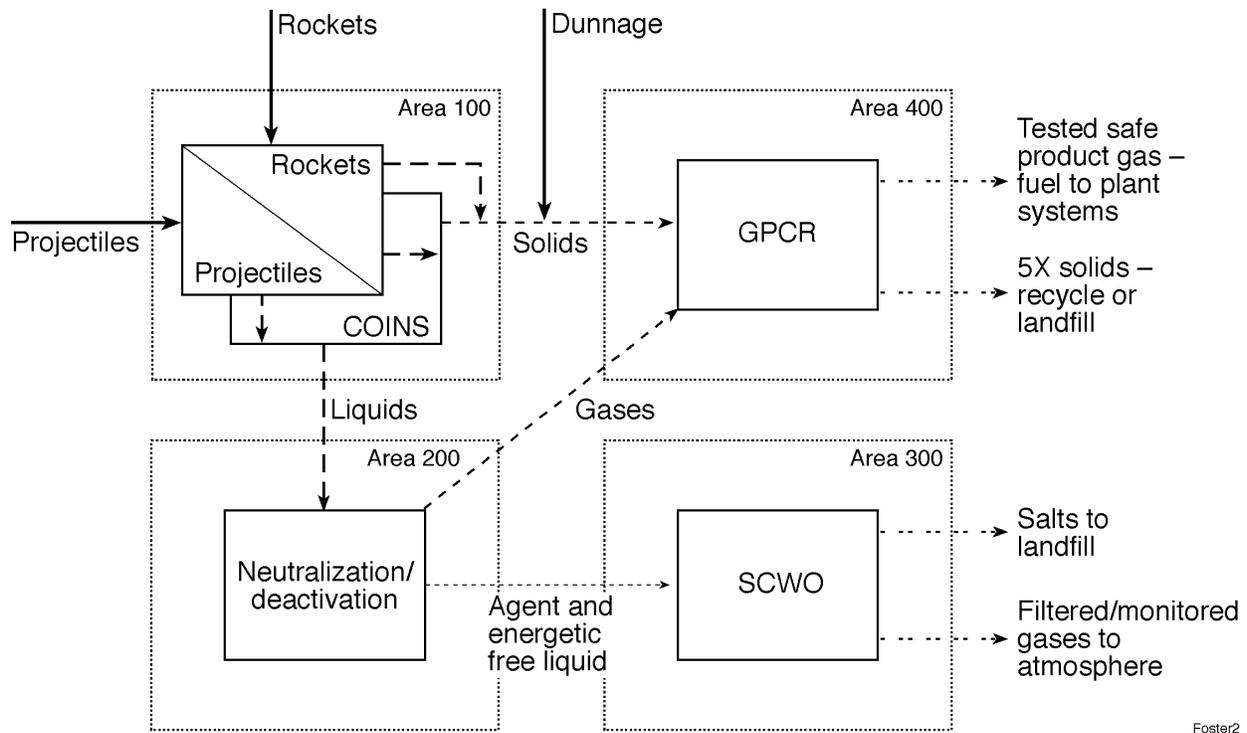


FIGURE 3.12 Neutralization/GPCR/TW-SCWO Process Overview Showing Different Areas of the Destruction Facility (Source: Foster Wheeler/Eco Logic/Kvaerner 2000)

3.2.3.2 History of Destructive Processes

Neutralization, GPCR, and TW-SCWO are the primary destructive processes employed in this technology. The history of these processes is summarized below.

3.2.3.2.1 Neutralization of Agent and Energetics

Agent and energetics neutralization were reviewed in Section 3.2.1.2. Because the history of neutralization of agent and energetics for neutralization/GPCR/TW-SCWO does not differ from other technologies, this information is not repeated.

3.2.3.2.2 Gas-Phase Chemical Reduction

GPCR is used in this technology system as a means of treating solid materials (metal parts and dunnage) and gases from other parts of the facility (from neutralization reactors). The process was developed and patented by Eco Logic (NRC 1999). Figure 3.13 is a simplified flow diagram for a typical GPCR process (Foster Wheeler/Eco Logic/Kvaerner 2000).

GPCR has a history of use in treating waste steams. This technology has been used to treat electrical equipment contaminated with PCBs (NRC 1999). In addition, the process has been used in both Canada and Australia (NRC 1999). The Australian plant currently processes organochlorine pesticide wastes; the major component of which is DDT³⁸ (Eco Logic 2001). Eco Logic, Inc., indicates that its process was demonstrated at the Middleground Landfill in Bay City, Michigan, under a Toxic Substances Control Act (TSCA) research and development permit during October and November 1992. The test was performed using PCB-contaminated wastewater, waste oil, and soil from the site. Test results yielded a 99.99% DRE for PCBs during all runs; a 99.99% DRE for a tracer compound (e.g., perchloroethylene); and a net destruction of trace feedstock dioxin and furan compounds during all runs (U.S. Environmental Protection Agency [EPA] 1994). Eco Logic has also evaluated the ability of this process to treat chemical agents and energetics considered in the ACWA program, including HD and VX (Eco Logic 1995). The PMACWA indicates that GPCR is expected to gain regulator acceptance (PMACWA 2001b).

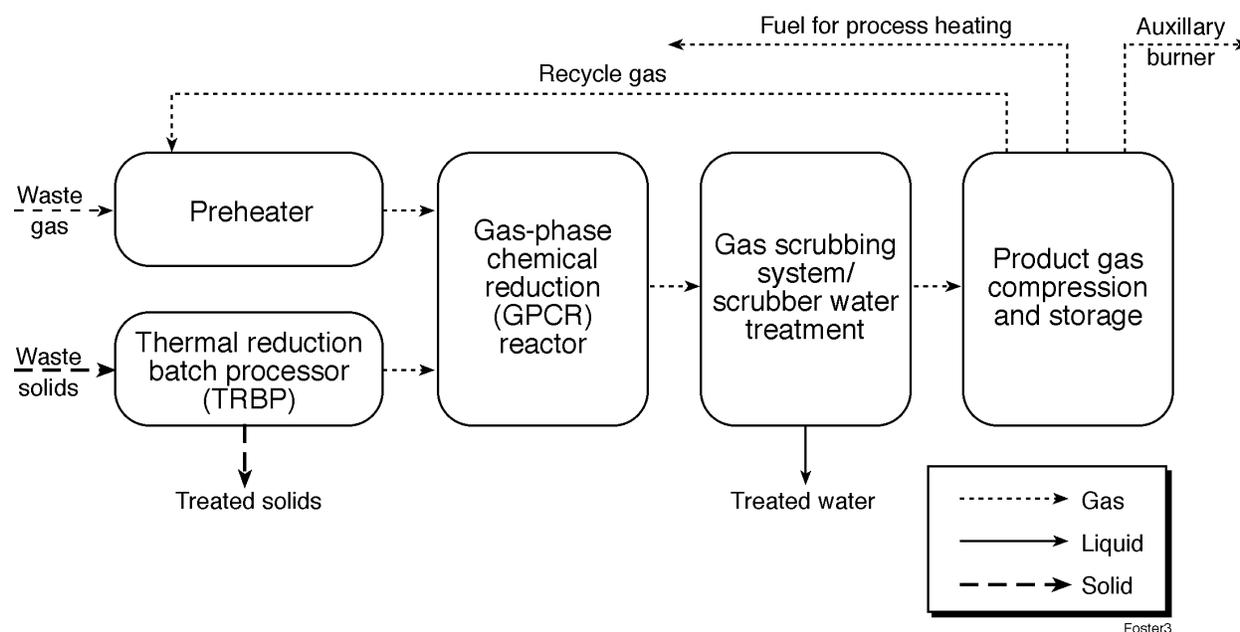


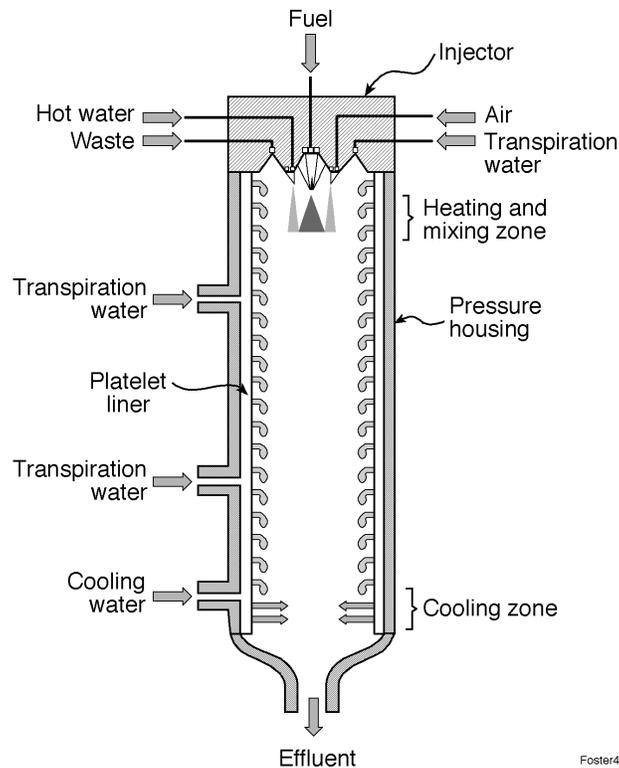
FIGURE 3.13 Flow Diagram of Gas-Phase Chemical Reduction (GPCR) (Source: Foster Wheeler/Eco Logic/Kvaerner 2000)

³⁸ DDT is a banned pesticide otherwise known as dichlorodiphenyltrichloroethane.

3.2.3.2.3 Transpiring-Wall Supercritical Water Oxidation

Supercritical water oxidation was reviewed in Section 3.2.1.2. The Foster Wheeler/Eco Logic/Kvaerner approach, however, involves a TW-SCWO unit, as opposed to the solid-wall unit. Figure 3.14 is a schematic of the TW-SCWO unit. The core technology with respect to organic oxidation for TW-SCWO differs only slightly from that of solid-wall SCWO. NRC (1998) and NRC (1999) provide information on both processes. Thus, the bulk of the information presented in Section 3.2.1.3 is not repeated here; only that which is unique to TW-SCWO is discussed.

TW-SCWO is a type of SCWO unit that was developed to overcome plugging and corrosion problems associated with conventional SCWO (NRC 1999). The premise behind the TW unit is that maintaining a layer of clean water between the unit wall and the primary oxidation reaction limits corrosion and associated plugging. The unit, called a transpiring platelet wall reactor, was developed and patented by GenCorp/Aerojet and Foster Wheeler/Eco Logic/Kvaerner (NRC 1999). The unit has two walls; an inner TW that is contained within an outer



Foster4

FIGURE 3.14 Transpiring-Wall (TW) SCWO Reactor (Source: Foster Wheeler/Eco Logic/Kvaerner 2000)

wall. The inner wall consists of a series of platelets that permit transpiration of deionized water on a continuous basis into the unit (NRC 1999). Additional details on the device are provided in NRC (1999). NRC (1998) also provides an overview of the SCWO process (including TW-SCWO) and presents the results of testing VX and other hydrolysates at PBA. To date, the TW technology has not been commercially used.

3.2.3.3 Demonstration Testing³⁹

As discussed for the other technology systems presented in this TRD, baseline reverse assembly, carbon filtration, and the BRA were not demonstrated as part of the demonstration program. Other unit operations proposed for the neutralization/GPCR/TW-SCWO system were also not selected for demonstration. The following unit operations proposed for neutralization/GPCR/TW-SCWO were not selected for demonstration by the PMACWA for the reasons given below.

Punch Machine. The projectile punch machine (PPM) is a new addition to the proposed full-scale process and was incorporated after demonstration had been conducted.

Projectile Burster Washout. This operation is substantially similar to the burster washout technology previously validated by the PMACWA.

MRSM. The MRSM is a new addition to the proposed full-scale process and was incorporated after demonstration had been conducted. It is also based on the existing baseline RSM process.

Propellant Grinding. Several ACWA technologies will require size reduction of M28 propellant. Therefore, the PMACWA has elected to conduct a single design study to address this requirement for these technologies.

COINS. Originally, during the initial preparations for Demo I in 1998, the technology provider (led by Lockheed Martin) proposed demonstration of caustic hydrolysis of energetic materials contained in fuzes, bursters, and propellant from rockets and projectiles. However, after the team was reformed in late 1999, the PMACWA decided to discontinue the demonstration of caustic hydrolysis on the basis of the success of Demo I. Data gathered during the PMACWA's Demo I activities demonstrated the ERH system (PMACWA 1999b) and the batch energetics hydrolysis at Pantex and the Radford Army Ammunition Plant (PMACWA 1999b).

³⁹ This material describes the Demo II PMACWA program and was derived, in part, from PMACWA (2001b). Because demonstration testing was intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

The reasons for selecting the neutralization/GPCR/TW-SCWO demonstration unit operations, testing objectives, and significant deviations from the planned testing are discussed in the following subsections.

3.2.3.3.1 Agent Hydrolysis

The PMACWA previously demonstrated agent hydrolysis extensively in its ATP and during Demo I. For Demo II, the PMACWA ran agent hydrolysis units to provide representative feedstock for TW-SCWO and to characterize the intermediate product stream for residual agent, Schedule 2 compounds, and other substances required to verify the mass balance. The specific test objectives of these demonstration units included the following:

- Use the hydrolysate recipes developed and tested by the ECBC;
- Characterize solid, liquid, and gas process streams; and
- Provide agent hydrolysate in support of demonstration testing.

During Demo I, GB and VX hydrolysate were produced in the 100-gal (379-L) batch reactor at CAMDS. The design and manufacture of a hydrolysis system provided information on equipment and operational parameters for use in scale-up to a full-scale facility (PMACWA 1999b). Also, VX and GB hydrolysate remaining from Demo I were shipped to DPG for the TW-SCWO demonstration.

For Demo II, 15% HD hydrolysate was produced in a campaign of 16 batch runs at the CTF (APG). The equipment used was not intended to model scale-up to a full-scale facility, but was an expedient design suitable for use in the contained environment of the CTF. HD hydrolysate was shipped to DPG for the TW-SCWO demonstration (Dalton 2000).

There were no significant deviations from the planned demonstration testing.

3.2.3.3.2 Energetics Hydrolysis

Other government agencies have previously demonstrated energetics hydrolysis. Energetics hydrolysis was also demonstrated during Demo I for a variety of feedstocks (PMACWA 1999b). Hydrolysis of M28 propellant, Composition B, and tetrytol (using 6% or 12% NaOH) was validated during Demo I.

During Demo II, feedstocks were similarly required for the TW-SCWO testing. The specific test objectives of these demonstration units included the following:

- Produce energetics hydrolysate for use as feed material in subsequent demonstration testing;
- Characterize solid, liquid, and gas process streams; and
- Gather process operation information to support the ACWA program and future scale-up.

Tetrytol and cyclotol hydrolysate were produced at Pantex and shipped to DPG for the TW-SCWO demonstration. Cyclotol was an alternate for Composition B since it contains comparable amounts of cyclotrimethylenetrinitramine (RDX) and 2,4,6-trinitrotoluene (TNT).

The Radford Army Ammunition Plant produced 16.7% M28 propellant in 12% caustic hydrolysate. M28 hydrolysate was shipped to DPG for the TW-SCWO demonstration.

There were no significant deviations from the planned demonstration testing.

3.2.3.3.3 TW-SCWO Energetics/Agent Hydrolysate

The basic ability of SCWO to destroy agent and energetics hydrolysates separately was demonstrated previously (PMACWA 1999b). TW-SCWO was demonstrated to validate the effectiveness of the transpiring wall unit design for the treatment of combined hydrolysate of agent and energetics.

The TW-SCWO reactor mixes feed materials, water, oxidant, and fuel under supercritical conditions. At supercritical conditions, these four materials are completely miscible and form a single phase with physical properties (high density, low viscosity) that are conducive to rapid oxidation. The TW-SCWO platelet reactor is designed to protect the walls from corrosion and to minimize plugging of the unit. Clean, high-pressure water is forced through passages in the wall and is metered through thousands of injection points in the perforated liner. The injected water is supposed to form a barrier between the liner and reaction products flowing through the reactor. Near the exit of the reactor, water at 60°F (15°C) is injected into the reactor to rapidly quench the effluent to 600°F (315°C). This causes most precipitated salts exiting the reactor to redissolve into the water. The cooled effluent then enters a flash gas separator. Gaseous effluents are scrubbed in carbon filters and released to the atmosphere. Liquid effluents containing soluble and insoluble salts and metal oxides were collected and analyzed. The demonstrated TW-SCWO operated with a hydrolysate feed rate of 60 lb/h (27 kg/h); 46 to 87 lb/h (21 to 87 kg/h) of

auxiliary fuel (kerosene) was added (depending on the feed) to increase the heating value of the feed. VX hydrolysate simulant was processed for 100 hours.

Characterization of gaseous, liquid, and solid effluents and verification of operating parameters were required. The objectives of the demonstration testing included the following:

- Demonstrate long-term, continuous operability of TW-SCWO with respect to salt plugging and corrosion in the reactor, effects of operation on the TW liner, and erosion of the pressure control valve;
- Determine whether aluminum from the energetic hydrolysis process can be processed by TW-SCWO without plugging;
- Demonstrate the ability of TW-SCWO to destroy Schedule 2 compounds present in the hydrolysate feed; and
- Characterize the gas, liquid, and solid process streams from TW-SCWO.

Four different mixes of agent hydrolysate simulant or mixed agent/energetics hydrolysate were processed through TW-SCWO. Continuous, long-term (100 hours) runs were intended to be performed to meet the objectives. The length of these continuous runs required quantities of feed that exceeded the DPG treatability study permits; therefore, the agent hydrolysates were supplemented by simulants. The feeds included the following:

- VX Hydrolysate Simulant. 13.2% dimethyl methylphosphonate (DMMP), 15.3% sodium isothionate, 9.8% diethanolamine, 3.1% isopropanol (70% solution), 18.0% NaOH (50% solution), and 40.6% water.
- HD/Tetrytol/Aluminum Hydrolysate. Simulated combined agent (HD) and energetic (tetrytol) hydrolysate obtained from an M60 105-mm projectile. Actual agent hydrolysate was used for the first 19 hours, at which time it was replaced by a mixture of 10.01% thiodiglycol and 9.58% sodium chloride (NaCl) in water; NaOH was added to bring the pH of the mixture to 11.
- GB/Cyclotol/Aluminum Hydrolysate. Simulated combined agent (GB) and energetic (cyclotol) hydrolysate obtained from an M426 8-in. projectile. Actual agent hydrolysate was used for the first 28 hours, at which time it was replaced by a mixture of 6.37% DMMP, 2.15% sodium fluoride (NaF), 2.60% NaOH, 1.03% isopropanol, and 0.77% tri-n-butylamine in water.

- VX/Cyclotol/M28 Propellant/Aluminum Hydrolysate. Simulated combined agent (VX) and energetic (cyclotol and M28 propellant) hydrolysate obtained from an M55 rocket. Actual agent hydrolysate was to be used for the first 79 hours, at which time it was to be replaced by VX hydrolysate simulant.

Significant deviations from the planned demonstration testing included the following:

- The HD/tetrytol/aluminum hydrolysate test was terminated after 55 hours because of concern over the remaining life of the reactor upper liner. During the earlier workup run with this feed, a region at the top of the upper liner (unprotected by transpiring water) cracked and had to be replaced. It was replaced with a spare lower liner segment modified for use as the upper liner. At the end of 55 hours of the validation test, the new upper liner exhibited significant deformation in the form of a bulge near the top of the liner.
- The GB/cyclotol/aluminum hydrolysate was run continuously for only 50 hours rather than the 100 hours objective; this was a planned change made at the end of the previous run.
- The VX/cyclotol/M28 propellant/aluminum hydrolysate validation run was terminated just short of 26 hours primarily because of continued feed flow problems, high effluent temperatures from heat exchanger fouling, and trouble with the reactor injector ports. No serious corrosion or salt plugging occurred within the reactor.

3.2.3.3.4 Gas-Phase Chemical Reduction Reactor

The GPCR technology consists of the TRBP and the reactor, which can be characterized as an electrically heated cyclone.⁴⁰ GPCR was demonstrated to validate the effectiveness of the process for heating metal parts and dunnage to 5X conditions in the TRBP and for treating the gaseous effluent in the hot, reducing environment of the reactor to destroy any residual agent and energetics.

In the TRBP, contaminated materials and metal parts are heated to 1,110°F (600°C). Organic compounds are volatilized and swept into the reactor by the hydrogen purge gas that is maintained in the TRBP. Metal parts are held at temperatures above 1,000°F (538°C) for at least 15 minutes to achieve a 5X condition. In the GPCR reactor, the gas-phase reduction of organic compounds occurs in the presence of hydrogen at temperatures above 1,560°F (850°C). Organics

⁴⁰ A cyclone is a device that is designed to spin a gas stream at a high rate of speed in order to remove entrained particles by using centrifugal force.

are reduced to CH₄, acid gases, and small amounts of simple hydrocarbons. Blister agents (H, HD, and HT) and nerve agents (VX and GB) are chemically reduced to CH₄, hydrogen chloride (HCl), hydrogen sulfide (H₂S), phosphoric acid (H₃PO₄), steam, N₂, and hydrogen fluoride (HF).⁴¹ Although not demonstrated, nitrogen oxides (NO_x) produced from the decomposition products of propellants and explosives should be converted to gaseous nitrogen and steam. Process gas leaving the top of the reactor is scrubbed in two caustic scrubbers to remove acid gases, water, heat, and fine particulate. The acid gases are neutralized to form common salts. The setup for GPCR included three TRBPs of various sizes and one reactor with a common gas scrubber system.

Characterization of gaseous, liquid, and solid effluents and verification of operating parameters were required. The objectives of the demonstration testing included the following:

- Demonstrate the ability of GPCR to achieve a 5X condition for metal parts and dunnage;
- Demonstrate the effectiveness of GPCR for the treatment of the gases generated during the processing of metal parts and dunnage;
- Validate the ability of GPCR to achieve a DRE of 99.9999% for HD and GB;
- Demonstrate the ability of GPCR to produce a gas effluent that meets EPA, Syngas, or BIF requirements;
- Characterize gas, liquid, and solid process streams from GPCR for selected chemical constituents to determine the absence or presence of hazardous, toxic, agent, and Schedule 2 compounds.
- Determine the need for stabilization of residual dunnage solids on the basis of toxicity characteristic leaching procedure (TCLP) results.

GPCR was tested with the following material:

- 150-lb (68-kg) carbon trays (1 tray for each of 3 runs),
- 66-lb (30-kg) wood spiked with 4,000 ppm of PCP (22 lb [10 kg] for each of 3 runs),

⁴¹ HF is produced only when GB is treated.

- 54-lb (241-kg) double-bagged DPE with butyl rubber to simulate boots and gloves (16.5-lb [7.5-kg] DPE suits with 1.65-lb [0.75 kg] butyl rubber and 4 plastic bags for each of 3 runs),
- 12-lb (5-kg) fiberglass storage and firing container tubes (1/4 tube, or 4 lb [2 kg] for each of 3 runs),
- 32-lb (15-kg) GB (10.8-lb [4.9 kg] agent for each of 3 runs), and
- Two mortars filled with a 30% HD heel (15.5-lb [7.0 kg] metal with 1.8-lb [0.81-kg] HD per mortar).

Significant deviations from the planned demonstration testing included the following:

- The first validation run with DPE was terminated before a 5X condition was achieved, because a rise in system pressure was observed due to a blockage that formed in the gas line between the TRBP and the reactor.
- The third validation run with a mortar and HD heel was not conducted because of schedule constraints.
- The product gas stream and the stack gas stream could not be completely characterized. The results of agent analysis in the gas stream were inconclusive; consequently, the gas samples could not be sent off-site to contract laboratories for analysis of nonagent-related constituents and, therefore, were analyzed by nonstandard analytical methods. Most of the stack gas analyses (all except oxygen [O₂], CO₂, and CO) and some of the product gas analyses (phosphine, HF, and hydrogen cyanide) were not conducted during the GB and HD validation runs.

3.2.3.3.5 Summary of Demonstration Testing

In summary, demonstration testing during Demo II was not as extensive as testing during Demo I because of the similarity of some of the unit processes and technologies. Agent hydrolysis and energetics hydrolysis objectives were met. Much of the agent testing of the TW-SCWO unit was performed with agent simulant rather than with agent. Operational problems with the TW-SCWO unit included liner integrity, feed flow problems, high effluent temperatures, and plugging of the reactor injection ports. Scaling/lining of the equipment downstream of the SCWO reactor was also shown to be problematic during demonstration testing. However, there was no serious corrosion or salt plugging observed within the reactor. The GPCR unit performed with minor problems; however, the product gas and stack gas streams

could not be adequately characterized for chemical agents or nonagent-related constituents because of difficulties with on-site analyses. Most of the stack gas analyses and some of the product gas analyses were not conducted for GB and HD validation runs. The PMACWA reviews the quality of the data generated during demonstration testing in PMACWA (2001d,e,f).

On the basis of demonstration testing, the technology provider plans to make the following changes to the neutralization/GPCR/TW-SCWO technology (Foster Wheeler/Eco Logic/Kvaerner 2000):

- Identify and finalize an analytical device and method to evaluate product gas from the GPCR unit for the presence of chemical agent;
- Demonstrate the effectiveness, operability, and cleanout cycles of the new GPCR device; and
- Incorporate equipment downstream of the TW-SCWO unit to remove aluminum and other solids.

3.2.3.4 Engineering Design Studies⁴²

During the demonstration testing described above, neutralization/GPCR/TW-SCWO was demonstrated to be a viable technology system for destruction of ACW, in accordance with the requirements of the PMACWA. However, the PMACWA determined that further studies would be necessary in preparation for full-scale pilot design and permitting. Therefore, EDSs will be conducted to provide this information. EDS-II objectives were as follows:

- Provide information for the full-scale facility with respect to total life-cycle cost, schedule, and safety;
- Support the EIS and permit application preparation under RCRA; and
- Support preparation of a RFP for a full-scale pilot plant facility.

⁴² This material describes EDSs for the technologies evaluated in the Demo II PMACWA program and was derived, in part, from PMACWA (2001a). EDSs for Demo II technologies are designated EDS-II. Because demonstration testing was intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

Agent and energetics neutralization studies that were planned for EDS-I are applicable to the neutralization/GPCR/TW-SCWO technology. These included activities discussed in the following two subsections.

3.2.3.4.1 Energetics Hydrolysis

Planned EDS activities for energetics hydrolysis consisted of the following:

- Addressing PMACWA and NRC (NRC 2000) concerns regarding particle size, solubility, by-products that would be produced as a function of time, control strategies, mixtures of energetics, and caustic concentrations; and
- Acquiring information for scale-up.

3.2.3.4.2 Agent Hydrolysis

Planned EDS activities for agent hydrolysis consisted of the following:

- Determine the potential to use 15% by weight mustard agent hydrolysate for feed to the SCWO unit for increased throughput.⁴³

EDS-II studies are expected to be under way on or about the date of publication of this document. Consequently, only preliminary plans for EDS-II are discussed here. Plans for EDSs were summarized from PMACWA (2000a). Figure 3.15 provides an overview of the neutralization/GPCR/TW-SCWO process and shows units or operations that were planned for EDS-II. Planned evaluations of units or operations would be independent of munition type or agent fill.

The following EDS-II activities were planned for neutralization/GPCR/TW-SCWO.

3.2.3.4.3 Munitions Access

Planned EDS-II activities for munitions access included the following:

- Grinding of M28 propellant.

⁴³ 15% hydrolysate mustard loading of the TW-SCWO unit was demonstrated during Demo II.

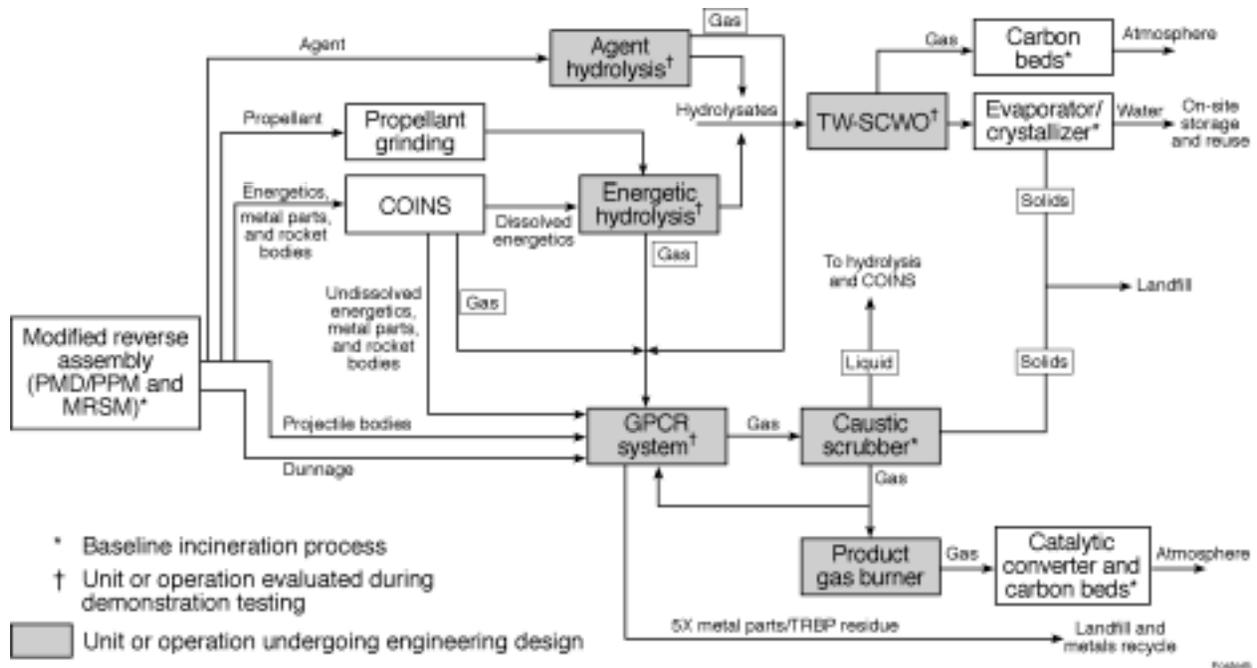


FIGURE 3.15 Flow Diagram of Neutralization/GPCR/TW-SCWO Process (Foster Wheeler/Eco Logic/Kvaerner System) Showing Units or Operations Undergoing Engineering Design (Source: Adapted from PMACWA 2001a)

3.2.3.4.4 TW-SCWO

Planned EDS-II activities for TW-SCWO included the following:

- Optimization and operability (500-hour runs) tests,
- Effluent salt cake characterization (evaporator/crystallizer),
- Methods and process monitoring development.

3.2.3.4.5 GPCR

Planned EDS-II activities for GPCR included the following:

- Agent methods and process monitoring development,
- Materials of construction 500-hour tests, and
- Explosivity tests.

As indicated previously, the results of EDSs for neutralization/GPCR/TW-SCWO are not included in this TRD.

3.2.3.5 Detailed Process Description

This section presents a detailed process description for neutralization/GPCR/TW-SCWO, as applied to PBA and the ACW stored there, on the basis of demonstration testing results. The equipment used in a pilot-scale facility may vary in nomenclature and design from that described here, on the basis of the system selected and system requirements.

Figure 3.16 illustrates the entire process flow for the neutralization/GPCR/TW-SCWO process as applied to PBA and the ACW stored there. As indicated previously in Figure 3.11, the technology system is segregated into four primary areas.⁴⁴ Munitions access and initial treatment of munitions hardware (e.g., land mine casings) would be conducted in Area 100. Munitions access would use modified baseline reverse assembly. M28 propellant from the M55 rockets would be pulled out of the rocket motor for subsequent neutralization in Area 200. Energetics from the rocket burster and other munitions hardware would be treated with caustic in the COINS system to extract and initiate neutralization of energetics, as well as to neutralize agent remaining after the drain process. As indicated previously, the treatment process for land mines using this technology system was not addressed. It is expected, however, that a process similar to the baseline process would be used to access agent and energetics in the land mines (See Appendix E of Volume 1).⁴⁵ Following munitions access in Area 100, the process for treating specific agents and energetics would be largely independent of munition type and agent fill.

Drained agents and M28 propellant from the M55 rockets would be neutralized in Area 200. Caustic hydrolysis using NaOH would be used to neutralize nerve agent and energetics. Neutralization would be performed in a series of CSTRs. Gases generated in these closed vessels would be piped to the GPCR unit in Area 400. Hydrolysate produced in Area 200 would be piped to Area 300 where it would be further treated with the TW-SCWO unit to remove Schedule 2 compounds and other organics. The agent and energetics hydrolysates may be treated in the same TW-SCWO processing train. Dunnage and other solids from rockets would also be treated using GPCR unit in Area 400. Solids would first be placed in the TRBP to drive off organic compounds and to complete treatment to a 5X condition. Gases would flow from the TRBP to the GPCR unit where they would be reduced in a hydrogen environment. Processing of land mine components would be similar to components of projectiles, as shown in Figure 3.16.

⁴⁴ A fifth process area, Area 500, would be established for infrastructure and support systems.

⁴⁵ It is also possible that land mine components could be processed using the COINS.

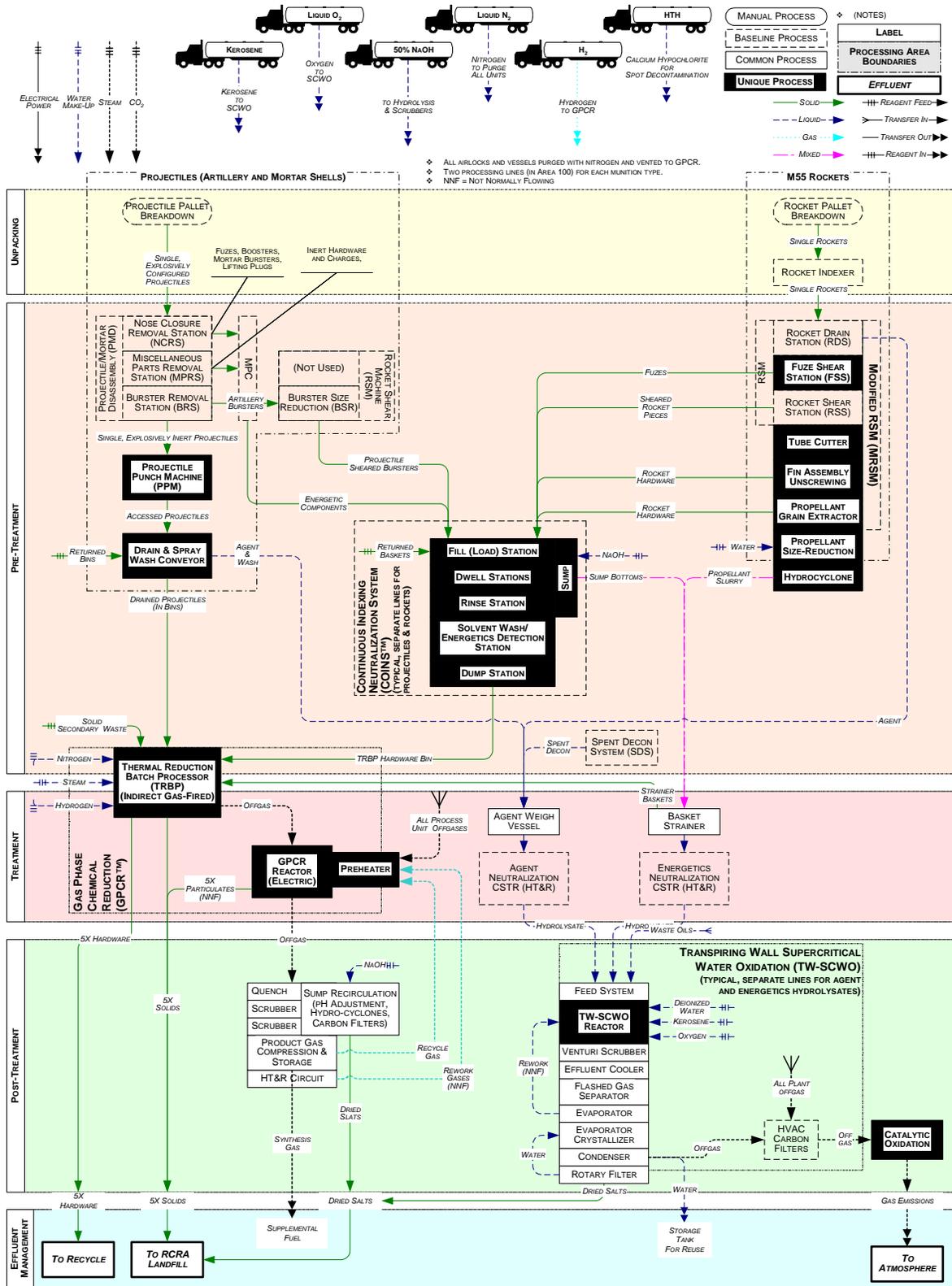


FIGURE 3.16 Flow Diagram of Entire Neutralization/GPCR/TW-SCWO Process at PBA (Source: Adapted from PMACWA 2001b,c)

Munition bodies (land mines) decontaminated to a 5X condition can be commercially recycled or disposed of as solid waste. Nonmetal solid waste that is treated to a 5X condition, if defined as hazardous waste, can be placed in a hazardous waste landfill.⁴⁶ If defined as nonhazardous wastes, these solid wastes may be disposed of in a nonhazardous waste landfill. Liquid from the SCWO units would be evaporated to drive off water and would leave a crystallized salt. The water would be condensed and recycled to the hydrolysis units, and the salts would be sent to a RCRA hazardous waste landfill.⁴⁷ Off-gases from process units (except the TW-SCWO) would vent to the GPCR unit. Off-gases from the GPCR unit would be processed through a series of scrubbers and compressors. The resulting liquified product gas may be used as a fuel gas in Area 400, assuming it meets regulatory acceptance criteria for BIFs. TW-SCWO off-gas would pass through carbon filters and would be released to the atmosphere.

Short descriptions of each of the unit processes included in the neutralization/GPCR/TW-SCWO process as applied to rockets stored at PBA are provided in the following subsections. Because the technology provider did not supply any information specific to land mines, a separate description of the munitions access process for land mines is not provided. However, as indicated above, it is anticipated that land mines would be processed in a manner similar to the baseline process. However, COINS, which the technology provider described for other munition components, may also be applied to land mines. Thus, the COINS process is described below. The remaining process descriptions (for agent and energetics treatment, dunnage treatment, metal parts treatment, and effluent management and pollution controls) apply to both rockets and land mines. Foster Wheeler/Eco Logic/Kvaerner (2000) includes detailed process flow diagrams and may be reviewed for additional detail.

3.2.3.5.1 Munitions Access – COINS

The reverse assembly operation would be segregated into a dry area and a wet area. ACW would be reverse assembled in the Area 100 dry area. The COINS would be housed in the Area 100 wet area. Munition parts would be processed in COINS, which is unique to this technology system. Munition parts would enter from the dry area through a fill chute with double-explosive doors. The parts would be dropped into baskets that would be processed through COINS on a conveyor system. The conveyor would immerse the baskets and the parts in caustic baths (dwell stations), followed by a wash station and a dump station. Parts would be held in the dwell stations until energetics had been dissolved and deactivated. Residual solids (including metal parts) that were not dissolved in COINS would be dumped in a TRBP bin, where they would be

⁴⁶ Solids treated to a 5X condition to remove residual agent may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in 40 CFR 260.21 – 260.24).

⁴⁷ While these salts are not known to contain chemical agent, they may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in 40 CFR 260.21 – 260.24. Typically, these salts contain heavy metals and exhibit the RCRA toxicity characteristic (40 CFR 261.24). In some states, the salts would be regulated as listed hazardous wastes because of their association with chemical agent. These salts could be “delisted” and not considered hazardous waste if regulatory delisting criteria are met.

tested for remaining energetics. If the residual solids met requirements, they would be sent to the GPCR unit in Area 400 for treatment to a 5X condition. Liquid and sludge from the COINS would be pumped to Area 200, where they would be further treated. Off-gases produced in COINS would be sent to the GPCR unit in Area 400 for further treatment. Additional information on the COINS, including several schematics, is provided in Foster Wheeler/Eco Logic/Kvaerner (2000).

3.2.3.5.2 Munitions Access – Rockets

The proposed design for munitions access for rockets incorporates many of the units and processes used in the baseline reverse assembly processes (see Appendix E of Volume 1 for details). Units and processes include reverse assembly machines, material handling conveyors, robotic loaders and handlers, auxiliary systems, and facilities and support systems. Some of these units have been slightly modified from the baseline process, but the basic unit and operations have been retained. The major differences, as compared with the baseline process and the process for projectiles, are summarized below.

Rockets would also be processed through the Area 100 dry and wet areas (including COINS), as described above. However, a MRSM would be used to shear the rocket. In the modified system, the same procedures as applied in the baseline RSM would be used, except in a different order. The modified RDS punches, drains, and washes out the rockets. One rocket shear station (RSS) shears the fuzes, and another RSS then shears the rocket body into sections. A tube cutter cuts the shipping and firing tube and the fin assembly is unscrewed from the rocket motor to access the propellant grain. The M28 propellant grain is then pulled out of the motor case in its entirety and size-reduced with a grinder into a slurry. Slurried propellant material from the rockets would be transferred to a number of holding tanks for feed to neutralization (Area 200). Agent and spray wash water would be transferred to a buffer area similar to the baseline TOX. The sheared rocket parts (fuze, burster, and ignitor) would be treated in the COINS as described above.

3.2.3.5.3 Agent Treatment

Agent treatment would be conducted in Area 200 in a treatment train separate from treatment of energetics. Nerve agent would be neutralized by reacting with NaOH (20% solution). Testing would confirm total neutralization. If testing detects residual agent, additional time would be allowed for agent treatment. Once the reaction is completed, treated hydrolysate would be pumped to surge tanks in Area 300, where the hydrolysate would await further treatment by TW-SCWO. Additional NaOH would be added while the hydrolysate is in these surge tanks to maintain appropriate pH. This eliminates the potential for agent reformation. All neutralization in the Area 200 reactors would be conducted under a nitrogen blanket. Nitrogen would be vented to Area 400 for treatment using GPCR.

Agent hydrolysate would be further treated to destroy Schedule 2 and other organic compounds using TW-SCWO. The TW-SCWO system would be designed to oxidize remaining organic materials in hydrolysates, including CWC Schedule 2 compounds, to water, CO₂, and inorganic salts. The TW-SCWO system is similar to the solid wall SCWO system discussed in Section 3.2.1.5, except that the unit incorporates a TW design. The TW is designed to place a layer of deionized water on the reactor's inner wall as a means of limiting corrosion and reducing generation and buildup of salts and other solids that the technology provider claims can clog conventional systems. TW-SCWO also differs from the solid wall unit in that the TW-SCWO can treat agent and energetic hydrolysates simultaneously.

After establishing system pressure, the system would initially be heated by startup water passed through a preheater. When the preheater temperature reached approximately 1,100°F (593°C), startup fuel and oxygen would be pumped to the reactor to initiate the oxidation reaction. With ignition achieved, the startup fuel and startup water would be decreased (but not stopped), while the hydrolysate feed, diluent water, kerosene spike (auxiliary fuel), caustic, and oxygen would be introduced to the reactor. The use of auxiliary fuel would minimize operational fluctuations resulting from incoming hydrolysate variability. The caustic solution would be used to neutralize any acidic species that might form during the oxidation reaction. Two TW-SCWO reactors would be operated in parallel.

Near the exit of the reactor, water at 60°F (15°C) would be injected to rapidly quench the effluent to 600°F (315 °C), causing most precipitated salts exiting the reactor to redissolve. After this, the effluent would pass through a backpressure regulator valve to reduce system pressure before entering a knockout drum. Hot effluent liquid and vapors would be separated in the knockout drum, which includes a scrubber to remove particulate solids from the vapor. The hot vapors would flow to an effluent cooler where they would be cooled to 120°F (49°C). The cooled effluent would then flow to a flashed gas separator where the vapor fraction (flue gas) would be separated and filtered through carbon filters and would be vented to the atmosphere. The flue gas would be continually monitored for CO, CO₂, nitrogen oxides (NO_x), nitrous oxide (N₂O), and O₂. Effluent would be analyzed for the presence of residual organics. If it met total organic carbon (TOC) specifications, it would be pumped to an evaporator/crystallizer system where water would be recovered and subsequently reused. If the effluent did not meet TOC requirements, it would be reintroduced into the TW-SCWO unit. Crystallized solids would be sent to a bin. If determined to be hazardous waste, the salts would be treated, as necessary, and disposed of as hazardous waste. As indicated previously, these salts could be delisted from being hazardous waste.

3.2.3.5.4 Energetics Treatment

Energetics treatment would be conducted in Area 200 in two separate treatment trains. One treatment train would be used for M28 propellant, and the other would be used for all other energetics, including energetic material from bursters and fuzes. The M28 propellant would be neutralized after it was size-reduced with a grinder. The other energetic materials would be

partially hydrolyzed in the COINS prior to bulk neutralization. As with nerve agent, neutralization would be conducted by reacting with NaOH (20% solution). Energetic material deactivation would be monitored by high-pressure liquid chromatography (HPLC). All other energetic treatment operations in Area 200 would be identical to that used for agent.

Following energetics neutralization, the energetics hydrolysate would be further treated in the TW-SCWO unit. Treatment there would be identical to that for agent hydrolysate.

3.2.3.5.5 Metal Parts and Dunnage Treatment and Process Off-Gas Treatment

Metal parts from Area 100 (land mine bodies), residual solids from COINS, and all dunnage would be treated in Area 400. Area 400 would also be used to treat process gases from other units that are part of this technology system, except for gases from the TW-SCWO unit. Area 400 would house the GPCR operation. In addition to the GPCR unit, the process would consist of a preheater unit for incoming process gases and a TRBP for 5X treatment of metal parts and dunnage. Gases from the TRBP would flow directly to the GPCR unit. In addition, the process would include a multistage system for gas scrubbing to remove inorganic contaminants and light hydrocarbons. The scrubber system would result in a process stream containing CH₄ and other hydrocarbons; this stream may be able to be used as fuel for a BIF.⁴⁸ Area 400 would also contain a product gas compression and storage unit.

Process gases from other units that are part of this technology system (except TW-SCWO), including recycled gases from the GPCR product gas compression and storage unit, would go to the GPCR preheater. There the gases would be preheated prior to processing in the GPCR.

The TRBP is a device used to heat metal parts and dunnage, thereby volatilizing organic materials from these solids. The device also vaporizes organic materials such as cellulose and plastics. TRBPs have a capacity of 47 yd³ (36 m³), and two of these devices are designed to operate in parallel. Each TRBP would operate in batch mode and, for dunnage, would have 3 trays capable of holding 15 waste-bearing drums for a maximum weight of 11,023 lb (5,000 kg) for each batch treated. Air would be purged from the device using nitrogen. Then preheated hydrogen and superheated steam would be injected into each tray of the unit at a temperature of 1,382°F (750°C), through individual flexible hoses. The TRBPs would operate in a batch cycle from 32 to 48 hours, depending on the agent and campaign. Gases would then be swept from the TRBP and into the GPCR unit by a preheated hydrogen sparging stream. Toward the end of the 32- to 48-hour period, the TRBP would be heated up to a temperature in excess of 1,112°F (600°C) for 30 minutes or more to help ensure that a 5X condition has been obtained. Finally, the TRBP would be cooled and purged with nitrogen and steam to end the cycle. Remaining 5X

⁴⁸ It is unclear whether the product gas would meet BIF acceptance criteria (40 CFR Part 266, Subpart H).

solids would be removed, and new solids would be loaded; removal and loading would take place through separate doors to prevent cross-contamination.

The GPCR reactor is designed to heat incoming waste streams and chemically reduce organic contaminants. Incoming streams would include preheated hydrogen, superheated steam, Area 100 and 200 off-gases, and volatilized waste from the TRBPs. These streams would be mixed in static mixers and enter the unit at a temperature of 650 to 750°C. Residence time for incoming streams would be between 2.5 and 10 seconds. The hydrogen and steam would react with the organic contaminants to produce HCL, HF, phosphorous oxides, H₂S, and CH₄. A secondary steam reforming reaction would produce CO, CO₂, and H₂.

The GPCR also includes a gas scrubbing, water treatment, and compressing/storage system. The reduced gas from the GPCR would be processed through a series of scrubbers where caustic neutralizes acid gases. Inorganic salts would be precipitated from solution and filtered from the effluent. Naphthalene and solid particulates would be removed before the gas, which has now been cooled to near ambient conditions, goes to compressors. The gas compressors would consist of a series of coolers for liquid separation. Liquid and gas would be stored in product gas storage tanks where the product would be tested to ensure complete treatment. The product gas is intended for reuse as supplemental fuel in the Area 400 process burners or Area 500 support services (heating) boiler. In the event that any gas fails to meet treatment criteria, it can be reprocessed in the GPCR. A final level of emission control redundancy would be provided by use of a catalytic converter. This would ensure that all of the fuel gas and product gas combusted in the process would be fully converted to CO₂ and water.

3.2.3.5.6 Effluent Management and Pollution Controls

The effluent management and pollution control systems used in neutralization/GPCR/TW-SCWO would be similar to systems used in the baseline incineration plant. These systems would be independent of agent and munition type. Elements of the system are described below.

The plant ventilation system is designed with cascading air flow from areas of less contamination potential to areas with more contamination potential. The ventilation system permits room air-change frequencies consistent with area-level designations⁴⁹ for normal as well as anticipated maintenance activities. Plant ventilation flow would be collected in the main plenum and directed to a bank of carbon filters. Two HEPA filters would also be used in series to remove particulates from the air streams. From here, the air would be filtered and monitored, passed through induction draft fans, and exhausted to the stack and the atmosphere. This system would be nearly identical to the baseline system.

⁴⁹ Level A, B, C, D, or E indicates the potential for contamination; Level A is the highest, and E is the lowest.

The decontamination fluid supply system and spent decontamination fluid collection system would be the same as the baseline system. Decontamination fluid would be supplied to most rooms in the main plant area, and spent decontamination fluid would be collected in sumps that would be monitored and controlled. The spent decontamination fluid would be transferred to the hydrolysis treatment area (Area 200) where it may be mixed with additional decontamination solution to ensure complete destruction of agent.

The DPE-supplied air and personnel support system would include maintenance air locks, donning/doffing support equipment, and facilities identical to baseline.

Rather than the baseline BRA, the evaporator/crystallizer would be used. This system would be similar to the BRA unit used in the baseline system, except that it would be modified to handle brine salts from the TW-SCWO process and water recovery by condensation for reuse in the plant. The evaporator/crystallizer would include equipment for effluent evaporization. If classified as hazardous waste, dried salts would be disposed of in a hazardous waste landfill. Dried salts may also be delisted, as indicated previously.

The TRBP portion of the GPCR would result in treated metal and other solids which the TRBP is intended to treat to a 5X condition. While metals may be recycled, treated solids would be treated further, if necessary, and disposed of in a solid or hazardous waste landfill in compliance with regulatory requirements.

The plant instrument air supply and steam supply systems would be identical to those employed in the baseline system.

Control rooms would be the same as those used in the baseline system, with changes as needed to accommodate the new systems and equipment.

The process for handling munitions from storage to the unpack area would be similar to that used for the baseline system.

Personnel support, monitoring systems, and analytical laboratories would be similar to those used in the baseline system.

As indicated previously, elements of the baseline incineration process are included in the overview of baseline and ACWA system technologies provided in Volume 1 of this TRD (see Section 1.4). In addition, the baseline incineration process is described in Appendix E of Volume 1.

3.2.3.6 Common Elements – Other Systems

The neutralization/GPCR/TW-SCWO process has several elements that are identical or nearly identical to other systems. Commonalities with other applicable technology systems include the following:

- The munitions access system used for neutralization/GPCR/TW-SCWO employs much of the baseline reverse assembly system, as do most of the other ACWA systems.
- Neutralization/GPCR/TW-SCWO employs essentially the same process as neutralization/SCWO and neutralization/biotreatment for neutralization as a primary treatment for chemical agents and energetics.
- The SCWO and TW-SCWO processes are comparable processes since they both involve oxidation of organics at supercritical conditions. Different ancillary equipment would be required for each type of SCOW unit, however.

Facility structure; ventilation; decontamination fluid supply; personnel support; pollution abatement; water, air, and steam supply systems, control rooms; monitoring systems; and laboratory support would be identical or nearly identical to the baseline system.

3.2.4 ELECTROCHEMICAL OXIDATION

The electrochemical oxidation technology system uses modified baseline reverse assembly to access agent and energetics. Agents and energetics are then mineralized using SILVER II, an electrochemical oxidation process that uses silver nitrate (AgNO_3) in concentrated nitric acid (HNO_3). Hardware and solids are thermally decontaminated.

The technology provider under Demo II refers to its electrochemical oxidation process as the SILVER II process. This neutralization process takes place in a standard industrial electrochemical cell and relies on the oxidizing capability of Ag^{2+} ions in a solution of HNO_3 . The Ag^{2+} ions mineralize organics primarily to CO_2 , inorganic salts, water, and acids. Electrochemical oxidation differs from the other technologies evaluated in this TRD in that no secondary treatment to address Schedule 2 compounds is needed.

This technology is applicable to all ACW stored at PBA, including both rockets and land mines, and the technology provider reports that it is as effective for energetics (AEA/CH2MHILL 2000). Although the technology provider supplied detailed information regarding application of this technology to rockets, little information was supplied regarding application of the technology to land mines. Similarly, the PMACWA demonstration testing did

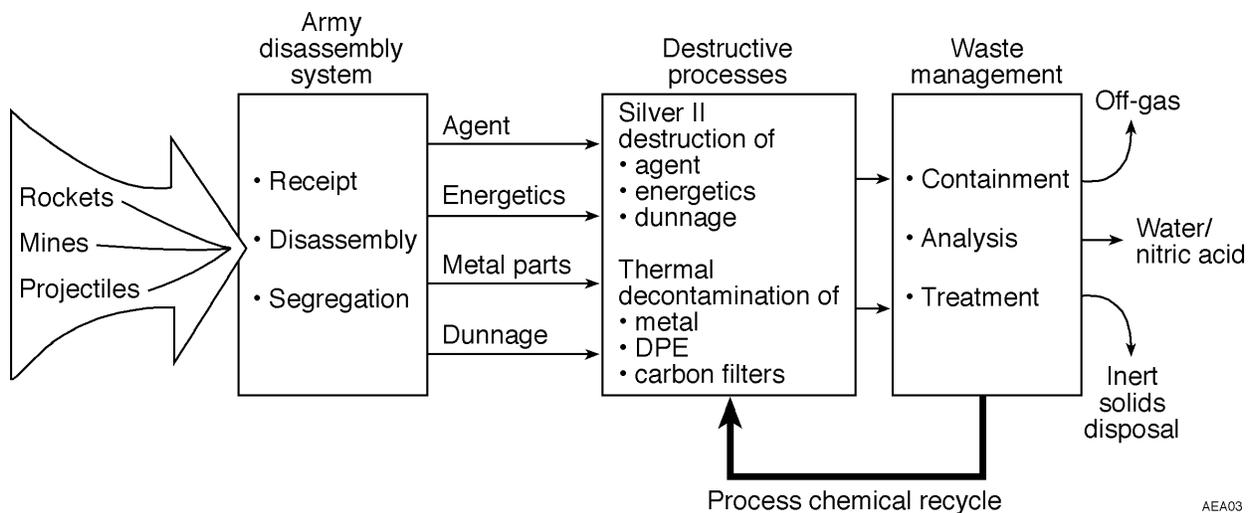
not address land mines in particular. It is assumed that munitions access for the land mines would follow the baseline or a modified baseline munitions access process. Following munitions access, treatment of agent and energetics from the various types of ACW would be largely independent of munition type and agent fill.

SILVER II was proposed by AEA Technology/CH2MHILL, though similar systems may also be considered. The following subsections provide a more detailed discussion of the technologies and processes involved in this system. The technology provider's technology demonstration report (AEA/CH2MHILL 2000) may be viewed for additional detail.

3.2.4.1 Process Overview

Figure 3.17 provides an overview of the electrochemical oxidation technology system using SILVER II. ACW at PBA would be disassembled using a modified baseline reverse assembly process. As indicated above, the PMACWA or the technology provider did not address the treatment process for land mines using this technology system. However, elements of the baseline or modified baseline munitions access process may be applied to land mines.

Fluid-abrasive cutting and fluid-mining employing water and grit would be used to access the rockets. Spent grit would be filtered from the water and sent to thermal treatment; the water would be reused for fluid-abrasive cutting. A RDM would replace the baseline RSM. The RDM is a new machine that performs the same function as the existing RSM. The rocket processing begins with the automatic feeding of the rocket, contained in its firing tube, to the punch and



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FIGURE 3.17 Overview of the AEA/CH2MHILL SILVER II Treatment Process (Source: Adapted from NRC 1999)

drain station. The RDM would punch and drain the rockets, and steam would be used to wash the agent reservoir. The agent would be drained and pumped to buffer storage tanks. The rocket would then be fluid jet cut into three sections. The fuze, warhead, motor, shipping and firing tube, and fin assembly would then be separated. Bursterns would be fluid-mined to remove the explosive charges. The M28 propellant grain would be pulled out of the motor case in its entirety and size-reduced with a two-stage grinder into a slurry. The rocket parts and fiberglass shipping/firing tube would be transferred to thermal treatment.

Fuzes and supplementary charges from all ACW at PBA would be sent to a detonation chamber. The detonation chamber is a thermally initiated, contained detonation device that initiates the energetics by exposing them to heat. As indicated above, the treatment process for land mines using this technology system was not addressed. It is anticipated, however, that a process similar to the baseline process would be used to treat energetics in the land mines (See Appendix E of Volume 1). Alternatively, the detonation chamber could be used for this purpose.

Slurried explosive material from the ACW (20% by weight) would be sent to a number of holding tanks for feed to the SILVER II reactor. Agent would be pumped to a buffer area similar to the baseline TOX holding system. Solid secondary wastes (i.e., dunnage) would be size-reduced using two-stage shredders. Metal components, including projectile and mortar bodies, would be thermally treated to a 5X⁵⁰ condition in a MPT, and dunnage would be thermally treated in a batch rotary treater (BRT). All process off-gases would pass through a catalytic oxidation unit and through carbon filters prior to release to the atmosphere.

Agents and energetics would be fed into separate SILVER II reactors. A 2-kW unit for agents and a 12-kW unit for energetics were used during demonstration testing. SILVER II is an aqueous electrochemical process that uses AgNO₃ in concentrated HNO₃, in which an electrochemical cell is used to generate a reactive material (Ag²⁺) that readily oxidizes organic substrates. End products of this oxidation process are primarily CO₂, inorganic salts, water, and acids. Elements present in the organic substrate, such as nitrogen, sulfur, or phosphorous, are oxidized to nitrate ions, sulfate ions, or phosphate ions. Silver compounds (e.g., chloride) would be recycled or recovered off-site, after which they could be returned to the process.

3.2.4.2 History of Destructive Processes

The electrochemical oxidation process is a relatively new technology with respect to destruction of agent or energetics in the stockpile of ACW. The SILVER II process has yet to be

⁵⁰ The definition of 5X is provided in Volume 1 of this TRD (see Section 1.3.2.4).

used commercially for waste treatment, although a number of tests have been conducted on various materials. The type of electrochemical cell used in the SILVER II process is, however, used commercially in the chlor-alkali industry (NRC 1999).

Prior to the PMACWA demonstration, the largest pilot-scale tests for waste treatment have been conducted using a 4-kW cell consisting of a single anode-cathode pair. The most extensive tests have been conducted with spent tributyl phosphate dissolved in kerosene. These tests ran continuously for up to 14 days, and 40 gal (150 L) of feed material was destroyed. The electrochemical oxidation technology was also successfully tested on 0.35-oz (10-g) batches of agent at a pilot plant in Porton Down, United Kingdom. The Porton Down unit is similar in design to the system being proposed for the ACWA program. It includes anolyte and catholyte feed circuits, an anolyte off-gas condenser, an NO_x reformer system⁵¹ and a modified version of the off-gas treatment circuit, including a NaOH scrubber (NRC 1999).

Additional testing on VX has been conducted at Porton Down. The test involved a continuous run of 6.5 days. At the end of the test, no agent residuals could be detected. The DRE was calculated at 99.99998%, in terms of organic carbon. With respect to TOC, the DRE was calculated at 88.7% (NRC 1999).

The NRC has expressed concerns over the electrochemical oxidation process, particularly in the case of scaling up to meet production schedules and the wide diversity of ACW to be destroyed. The NRC expressed concern over the ability to maintain appropriate temperatures in a scaled-up system. The set point of the process is 194°F (90°C), and since the process employs large amounts of electricity, there is a potential problem in controlling those temperatures. The second concern comes from the size of particles. In commercial production, particles are expected to be larger than those experienced in tests. According to NRC (1999), larger particles tend to limit the feed rates. The NRC indicated that these concerns must be addressed in future tests, particularly when approaching commercial scale (NRC 1999). Demonstration testing, described below, was intended, in part, to address these concerns.

3.2.4.3 Demonstration Testing⁵²

As discussed for the other technology systems presented in this TRD, baseline reverse assembly, carbon filtration, and the brine reduction operation were not demonstrated as part of the demonstration test program. Other unit operations proposed for electrochemical oxidation

⁵¹ A NO_x reformer is an add-on pollution control device designed to remove NO_x after formation. The device uses water to form HNO₃.

⁵² This material describes the Demo II PMACWA program and was based, in part, on PMACWA (2001a). Because demonstration testing was intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

were also not selected for demonstration. The following unit operations proposed for SILVER II were not selected for demonstration by the PMACWA for the reasons given below:

- Shredder (size reduction). This is common commercial equipment used for marginal size reduction of solid secondary wastes for feed to the BRT. Extensive size reduction capabilities were previously validated by the PMACWA as part of Demo I and EDS-I.
- RDM. The RDM is a new addition to the proposed full-scale process and was incorporated after Demo II was conducted (AEA/CH2MHILL 2000). The punch and drain stations are based on the existing baseline RSM.
- Cutting Station. These fluid-abrasive cutting and fluid-mining operations are substantially similar to the rocket-cutting and fluid-mining technologies previously validated by the PMACWA as part of the neutralization/bio-treatment technology (PMACWA 1999a,b).
- M28 Propellant Grinding. Several ACWA technologies require size reduction of M28 propellant. Therefore, the PMACWA elected to conduct a single design study (during EDSs) to address this requirement.
- PDWM. The PDWM for projectiles is a new addition to the proposed full-scale process and was incorporated after Demo II was conducted (AEA/CH2MHILL 2000).
- Projectile Burster Washout. This operation is substantially similar to the burster washout technology previously validated by the PMACWA as part of the neutralization/biotreatment technology (PMACWA 1999a,b).
- Steam Spray Wash. Water spray washout of ton container vessels and steam washing of ton container tubing was demonstrated at the ECBC, Aberdeen Proving Ground, Maryland.
- Detonation Chamber. This device is a contained blast chamber and is a commercially available, indirect, electrically heated vessel.
- MPT and BRT. The MPT and BRT are similar to the MPT previously validated by the PMACWA as part of the neutralization/biotreatment technology (PMACWA 1999a,b).

- Catalytic Oxidation System. The catalytic oxidation system is commercially available; it is also similar to the CatOx previously validated by the PMACWA as part of the neutralization/biotreatment technology (PMACWA 1999a,b).
- Agent Impurities Removal System (AIRS) and Energetics Impurities Removal System (EIRS). These are new additions to the proposed full-scale process and were incorporated after Demo II was conducted (AEA/CH2MHILL 2000).

The reasons for selecting the electrochemical oxidation demonstration unit operations, testing objectives, and significant deviations from the planned testing are discussed in the following subsections. Demonstrations with a 2-kW SILVER II unit (for agents) and a 12-kW SILVER II unit (for energetics) are discussed separately.

3.2.4.3.1 2-kW SILVER II Unit (Agent)

A 2-kW SILVER II unit was demonstrated to validate destruction of the agents contained in ACW and to correlate with the 12-kW SILVER II unit through testing with agent simulants. The 2-kW SILVER II unit was demonstrated at Building E3566 at the Edgewood Area of APG, Maryland. The demonstration system was an integrated unit consisting of the following:

- Feed System. The agent for each run is pumped from a steel container into two premix vessels for metering into the anolyte vessel at an appropriate rate, according to the destruction efficiency of the particular organic material.
- Electrochemical Process. The electrochemical cell contains titanium electrodes that are electroplated with platinum. It is designed to operate at a maximum current of 1,000 amps per electrode face; power supply voltage is automatically varied to maintain the set current. The electrochemical cell consists of two cathodes flanking an anode. The electrodes are separated into anolyte and catholyte compartments by membranes made of a perfluoro ion-exchange polymer. The organic feed is metered into the anolyte vessel that contains 8-M HNO₃ and 10% AgNO₃. Fluids from the anolyte circuit flow through the channels and are exposed to the anode in the cell. When the current is turned on, the Ag²⁺ ions generated oxidize the organic feed. Some Ag⁺ ions and water (as hydrated protons) pass through the electrochemical cell membrane and flow into the catholyte vessel, which contains 4-M HNO₃. The cathodic reaction reduces the HNO₃ to NO_x and water in the catholyte vessel.

- **Particulate Removal and Treatment.** Silver chloride (AgCl) precipitates when chlorinated feeds (i.e., mustard agent) are exposed to HNO₃ and AgNO₃. The particulate removal process is integrated into the electrochemical process unit; a hydrocyclone⁵³ on the anolyte circuit removes the AgCl before it reaches the electrochemical cell. The AgCl accumulates in a separate evaporator oven for 5X treatment. The vapor from the oven passes to a condenser, and the condensate is returned to the anolyte vessel. The AgCl is then removed as a solid cake for silver reclamation.
- **NO_x Reformer Circuit.** The reactions with Ag²⁺, which occur in the anolyte circuit, release CO₂, CO, and NO_x. The reactions occurring in the catholyte circuit release NO_x. Off-gas from both circuits passes through a condenser to remove some of the NO_x vapors and then travels to the NO_x reformer. Because of facility size restrictions, the 2-kW plant included a NO_x reformer with a single column for absorption and distillation. As the gas travels up the column, water running down the column reacts with NO_x in the gas to form dilute HNO₃. The dilute HNO₃ is heated to evaporate water and produce concentrated HNO₃. The evaporated water is condensed and produces very dilute HNO₃, which is recycled to the anolyte vessel or disposed of as waste. The concentrated HNO₃ is recycled to the catholyte vessel or can be used commercially.
- **Caustic Scrubber Circuit.** Off-gas from the NO_x reformer is sent to the caustic scrubber tower to remove any residual NO_x before release of the gas to the facility ventilation system.

Laboratory-scale testing of a SILVER II agent unit has previously been performed with GB. Destruction of HT and VX has previously been tested at a scale similar to that of the demonstration unit. Characterization of gaseous, liquid, and solid effluents during demonstration testing and verification of operating parameters were required during demonstration testing. The test objectives of this demonstration unit included the following:

- Validate the ability of the 2-kW SILVER II unit to achieve a DRE of 99.9999% for mustard, GB, and VX agents.
- Determine the impact of operations on construction materials to be used in a full-scale system.
- Demonstrate the operation and performance of the following key process components for future scale-up:

⁵³ A hydrocyclone, also known as a water cyclone, is a device used to separate fluids with different densities.

- Instrumentation, valves, pumps, etc.
- Hydrocyclone (to determine its ability to deal with solids in the anolyte circuit).
- Electrochemical cell (electrodes and membranes).
- Develop operational data to allow comparison of the 2-kW SILVER II unit with the 12-kW SILVER II unit for use in scaling up SILVER II.
- Characterize silver-bearing residuals. Determine potential silver recovery and determine disposal options (via characterization) for residuals from silver recovery operation (mustard agent only).
- Characterize gas, liquid, and solid process streams from SILVER II for selected chemical constituents and physical parameters, and the presence or absence of hazardous, toxic, agent, agent simulant, and Schedule 2 compounds.

Significant deviations from the planned demonstration testing included:

- Reduction in the VX validation run quantity (from 22 lb to 9 lb [from 10 to 4 kg]) and duration because of schedule constraints, and
- Elimination of the chloroethyl ethyl sulfide (CEES) validation run because of difficulty in obtaining CEES in the quantity needed and schedule constraints.

3.2.4.3.2 12-kW SILVER II Unit (Energetics)

A 12-kW SILVER II unit was demonstrated to validate destruction of the energetics contained in ACW and to correlate with the 2-kW SILVER II unit through testing with simulants. The 12-kW SILVER II unit was demonstrated at the Fire Safety Test Enclosure at the Aberdeen Test Center, Aberdeen Area of APG, Maryland. The demonstration system was an integrated unit consisting of the following:

- Feed System. The energetics feed system is designed to maintain the energetics material in a 20% slurry with water by storing it in a continuously mixed feed vessel. Two forms of agitation ensure that the energetics remain in the slurry: an air-driven mixer and a recirculation loop. The energetics slurry

is fed to the analyte vessel by bleeding off a slipstream from the recirculation loop.

- SILVER II System. The SILVER II system of the 12-kW unit is the same as that for the 2-kW SILVER II unit but without the particulate removal and treatment system.⁵⁴ It does, however, have a complete NO_x reformer circuit, that includes separate absorption and distillation columns. As gas travels up the absorption column, water running down the column reacts with the NO_x in the gas to form dilute HNO₃. The dilute HNO₃ leaves the bottom of the absorption column and enters the distillation column, where it is heated to evaporate water and produce concentrated HNO₃.

Energetics testing in a laboratory-scale SILVER II unit was previously performed with RDX, TNT, tetryl, and a double-base propellant similar to M28. Characterization of gaseous, liquid, and solid effluents and verification of operating parameters were required during demonstration testing. The test objectives of this demonstration unit included the following:

- Validate the ability of the 12-kW SILVER II unit to achieve a DRE of 99.999% for Composition B (RDX and TNT), tetrytol (tetryl and TNT), and M28 propellant.
- Validate the ability of the 12-kW SILVER II unit to achieve a DRE of 99.9999% for DMMP, a VX/GB simulant.
- Determine the impact of operations on construction materials to be used in a full-scale system.
- Demonstrate the operation and performance of the following key process components for future scale-up:
 - Instrumentation, valves, pumps, etc.;
 - Electrochemical cell (electrodes and membranes);
 - Full-height NO_x reformer/silver recovery boiler (ability to maintain H₂O balance); and
 - Off-gas scrubber operating in conjunction with an NO_x reformer.

⁵⁴ No chlorinated feeds were processed in this unit; thus, the particulate removal and treatment system was removed from the unit.

- Develop operational data to allow comparison of the SILVER II 2-kW agent system with the 12-kW energetics SILVER II system for use in scaling up the SILVER II agent system.
- Demonstrate the ability or inability to recycle, reuse, or dispose of HNO₃.
- Characterize gas, liquid, and solid process streams of SILVER II for selected chemical constituents and physical parameters and for the presence or absence of hazardous and toxic compounds.

Significant deviations from the planned demonstration testing included the following:

- Elimination of the CEES validation run because of difficulty in obtaining CEES in the quantity required and schedule constraints,
- Reduction of the quantity of M28 propellant (from 440 to 308 lb [200 to 140 kg]) because of schedule constraints, and
- Elimination of planned Composition B testing because of schedule constraints.

3.2.4.3.3 Summary of Demonstration Testing

In summary, demonstration testing during Demo II was not as extensive as testing during Demo I because of the similarity of some of the unit processes and technologies. The 2-kW and 12-kW systems were each evaluated during the demonstration. Schedule constraints, however, prevented the PMACWA from completing demonstration testing with VX, some of the energetics, and CEES simulant. Nevertheless, the PMACWA has determined that SILVER II is effective in destroying agents and propellant at the targeted levels. However, the curtailed tetrytol demonstration and lack of any demonstration data for Composition B prohibits the complete validation of the process. The technology includes operations to effectively process metal parts and dunnage. Although Composition B has not been demonstrated, greater than 99.999% destruction of the constituents of Composition B and tetrytol in laboratory experiments indicates the likely effectiveness with these energetic compounds (PMACWA 2001b). The PMACWA reviews the quality of data generated during demonstration testing in PMACWA (2001f).

On the basis of demonstration testing, the technology provider plans some substantive changes to the electrochemical oxidation SILVER II technology. One concern with regard to process operability, is the treatment of burster energetics (tetrytol and Composition B) in the SILVER II system. A limitation of SILVER II was discovered when tetrytol was fed to the

12-kW SILVER II demonstration unit at the originally planned feed rates (AEA/CH2MHILL 2000). Because SILVER II had problems decomposing an intermediate product, material began to precipitate within the anolyte circuit. Consequently, the system had to be shut down to clear the lines. The technology provider's solution to the precipitation problem was to add a hydrocyclone and a high-speed mixer in the anolyte circuit (AEA/CH2MHILL 2000). According to PMACWA (2001b), there was also a buildup of organics in the catholyte. The catholyte circuit was periodically drained, and the drained catholyte solutions were never reintroduced into the anolyte; thus, it is possible that the intermediate product that was concentrating within the catholyte was only partially treated. A catholyte-to-anolyte recycle stream has been proposed to reduce the buildup of organics within the catholyte.

In addition to the above, the technology provider has added a RDM for munitions access of rockets and a PDWM for munitions access for projectiles. An AIRS and an EIRS have also been added to the agent and energetic SILVER II units. These are new additions to the proposed full-scale process and were incorporated after Demo II was conducted (AEA/CH2MHILL 2000).

Upon incorporation of these changes, the technology provider believes that feed rates can be increased to the originally planned values. While these proposed improvements all have merit, optimization studies may be required (PMACWA 2001b). Additional details of the results of demonstration testing may be obtained from AEC/CH2MHILL (2000) and PMACWA (2001b,c).

3.2.4.4 Engineering Design Studies⁵⁵

During the demonstration testing described above, electrochemical oxidation was demonstrated to be a viable technology system for destruction of ACW, in accordance with the requirements of the PMACWA. However, the PMACWA determined that further studies would be necessary in preparation for full-scale pilot design and permitting. Therefore, EDSs will be conducted to provide this information. EDS-II objectives were as follows:

- Provide information for the full-scale facility with respect to total life-cycle cost, schedule, and safety;
- Support the EIS and permit application preparation under RCRA; and
- Support preparation of a RFP for a full-scale pilot plant facility.

⁵⁵ This material describes EDSs for the technologies evaluated in the Demo II PMACWA program and was derived, in part, from PMACWA (2001a). EDSs for Demo II technologies are designated EDS-II. Because demonstration testing was intended to apply to a variety of ACW from all storage sites, this section does not discriminate with regard to munition type and storage installation.

As of the preparation of this report, EDS II plans were not firm and are likely to change as the program proceeds. However, EDS for this technology are expected to be ongoing at about the same time that this report is published. According to the PMACWA (2001a), EDS II, as planned, included further investigation of the following issues associated with electrochemical oxidation:

- Modifications to 12-kW plant energetics feed and ancillary systems,
- 500-hour runs of agent simulant and Composition B/M28 propellant with the 12-kW plant,
- Laboratory-scale testing on cell membrane life and feeds containing fluoride,
- Testing of hydrocyclones, high shearing mixing, and organic transfer mechanism, and
- Paper studies on projectile burster wash and energetic slurry concentration.

Table 3.4 provides further information on planned EDS II activities for electrochemical oxidation. Figure 3.18 is an overview of the electrochemical process and shows unit operations that may be further evaluated during EDS II. Planned evaluations of unit operations would be independent of munition type or agent fill.

3.2.4.5 Detailed Process Description

This section presents a detailed process description for electrochemical oxidation, as applied to ACW stored at PBA, on the basis of demonstration testing results. The equipment used in a pilot-scale facility may vary in nomenclature and design from that described here, depending on the system selected and system requirements.

Figure 3.19 shows the entire process for electrochemical treatment of ACW at PBA. Munitions access would use modified baseline reverse assembly. Fuzes, boosters, and supplementary charges would be treated in a detonation chamber. Metal parts from the detonation chamber, munitions hardware, dunnage, and other solid wastes would be thermally decontaminated to a 5X condition in either the MPT, an inductively heated vessel with a superheated steam reactive environment, or the BRT, a rotary version of the MPT with a structure similar to that of the baseline DFS. Steam would be condensed from the MPT or BRT and treated in the SILVER II process. Agents would be drained from the ACW, and energetics would be removed and slurried.

TABLE 3.4 Potential Further Studies under Engineering Design Study-II

Test Elements	Objectives
Modifications to 12-kW and ancillary systems	Provide extended, reliable feed of energetics.
Anolyte and catholyte circuits	Implement and demonstrate selected improvements to vessels, piping heating, controls, mixing, and separation.
Cell membrane life	Confirm membrane life over an extended period of operation.
Fluoride containing feedstock	Confirm transport of fluoride w/in process and investigate methods to mitigate impact on materials of construction.
Hydrocyclone testing	Optimize design for removal of process intermediates.
High shear mixer testing	Investigate mixing performance for optimal destruction of organics and overall process performance.
Organic transfer across cell membrane	Investigate migration of organic species across cell membranes for long-term system performance.
Projectile burster washout	Confirm proof of concept and identify design parameters for projectile burster washout.
Energetic slurry concentration safety	Assemble and summarize available information to guide energetic slurry management.

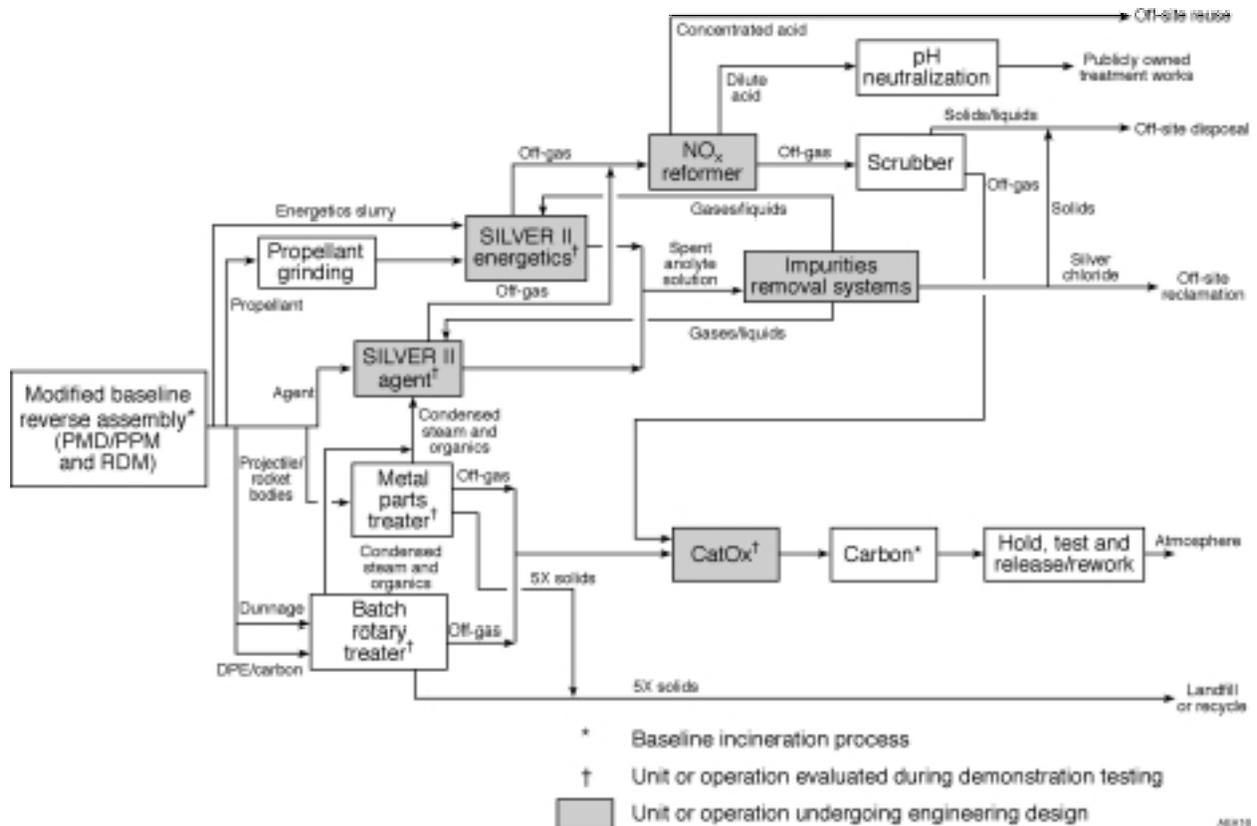


FIGURE 3.18 Flow Diagram of Electrochemical Oxidation SILVER II Process (AEA/CH2MHILL System) Showing Units or Operations Undergoing Engineering Design (Source: Adapted from PMACWA 2001a)

Drained agents and slurried energetics would be treated in separate SILVER II processes. These processes would mineralize the agent and energetics with electrochemical oxidation facilitated by Ag^{2+} ions. The SILVER II process would be supported by an agent impurities removal system (AIRS) and an energetic impurities removal system (EIRS). These units would each generate process solids that would be treated further, as necessary, and disposed of off-site in a RCRA hazardous waste landfill. Silver would be reclaimed off-site, and HNO_3 would be generated for reuse in the process. Dilute acid by-product from SILVER II is intended for treatment in an on- or off-site wastewater treatment plant.

All process off-gas would be mixed with air and catalytically converted by the catalytic oxidizer technology, followed by carbon filtration, and release to the atmosphere. Treated munition bodies (5X condition) would be commercially recycled. Treated solid wastes

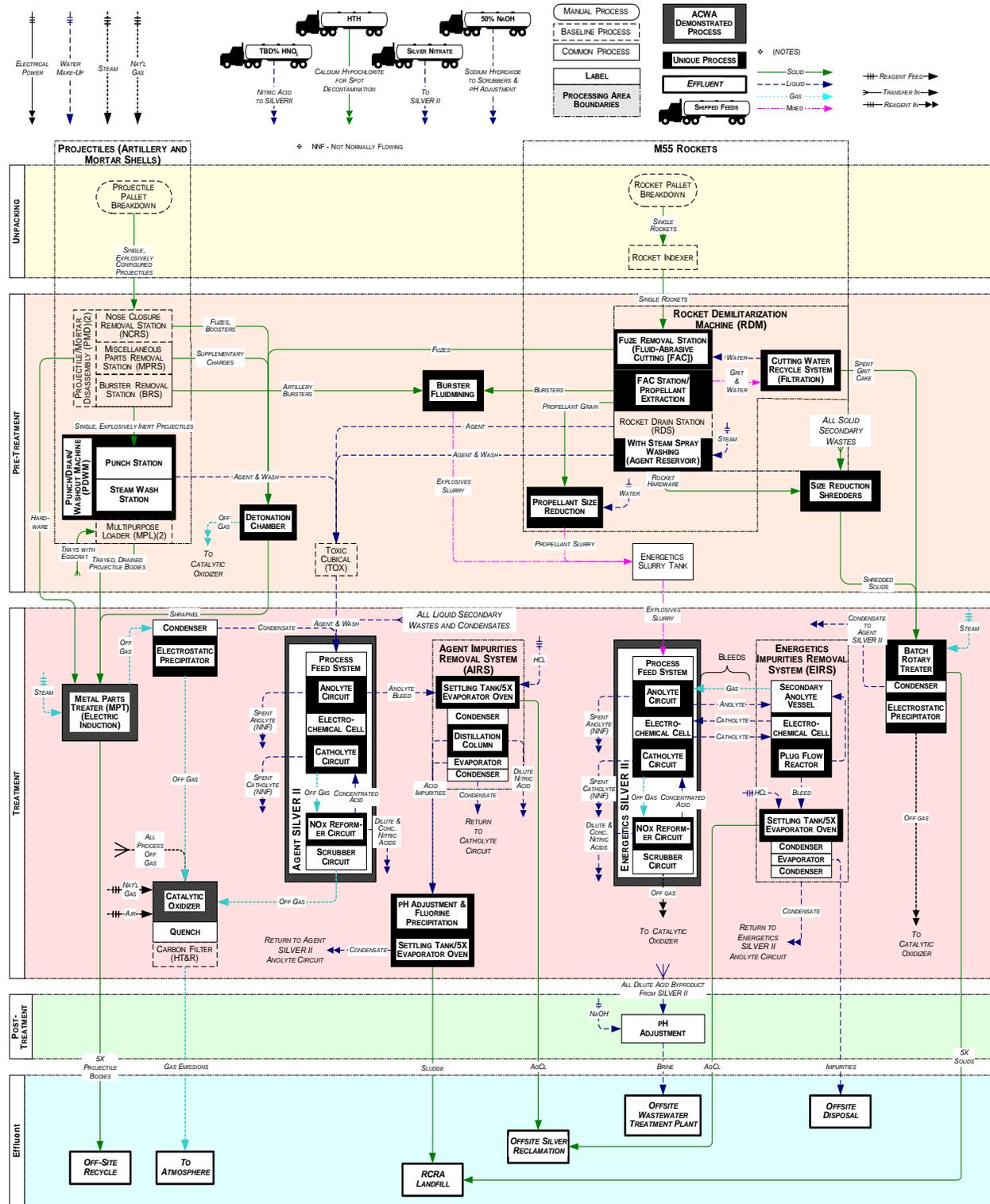


FIGURE 3.19 Flow Diagram of Electrochemical Oxidation Using the SILVER II Process at PBA (Source: PMACWA 2001b,c)

(5X condition) would be treated further, as necessary, and placed in a landfill as RCRA hazardous waste or disposed of as nonhazardous waste in accordance with regulatory requirements.^{56,57}

Short descriptions of each of the unit processes included in the electrochemical oxidation technology system are provided below. As indicated previously, the technology provider did not address the treatment process for land mines using this technology system. It is anticipated, however, that a process similar to the baseline process would be used to access agent and energetics in the land mines (see Appendix E of Volume 1). Following munitions access, the process for treating agents and energetics would be largely independent of munition type and agent fill.

3.2.4.5.1 Munitions Access – General

The SILVER II process would use modified baseline reverse assembly and fluid accessing (fluid-abrasive cutting and fluid-mining using water) for ACW pretreatment. Spent grit would be filtered from the water and sent to thermal treatment; the water would be reused for fluid-abrasive cutting. Slurried explosive material from the ACW (20% by weight) would be sent to a number of holding tanks for feed to the SILVER II reactor. Agent would be pumped to a buffer area similar to the baseline TOX system. Solid secondary wastes (e.g., dunnage) would be size-reduced using two-stage shredders. Metal parts and dunnage would be treated thermally to a 5X condition, in a manner similar to methods used in other technologies. Details for handling projectiles and mortars and rockets are presented below.

3.2.4.5.2 Munitions Access – M55 Rockets

M55 rockets would be transported to the unpack area and loaded into the rocket loading device in the same manner as the existing baseline system. Two identical parallel rocket disassembly lines, each contained in separate ECRs, would be used. The individual rocket would be conveyed through the air lock and into the ECR, which contains the rocket demilitarization machine (RDM). The RDM is a new machine that performs the same function as the existing RSM. The rocket processing would begin with the automatic feeding of the rocket, contained in its firing tube, to the punch and drain station. This would be based on the existing punch and

⁵⁶ Solids treated to a 5X condition to remove residual agent may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in 40 CFR 260.21–260.24.

⁵⁷ While these solid wastes are not known to contain chemical agent, they may be defined as hazardous waste if they exhibit any of the characteristics of hazardous waste as defined in 40 CFR 260.21 – 260.24. These solids may contain heavy metals and exhibit the RCRA toxicity characteristic (40 CFR 261.24). In some states, the solids would be regulated as listed hazardous wastes because of their association with chemical agent. These solids could be “delisted” and not considered hazardous waste if regulatory delisting criteria are met.

drain process, but with the addition of a final steam-out to remove residual agent. The agent would be drained and pumped to buffer storage tanks, the same as for the projectiles and mortars. The rocket would then be fluid jet cut into three sections. A fuze cut would be made to separate the fuze and expose the burster section. A tail cut would be made to separate the tail section and expose the bottom end of the propellant grain for subsequent extraction. Disposition of individual rocket components would be as follows:

- The fuze sections would be deposited in mesh containers and conveyed to the detonation chamber for destruction.
- The warhead section would be conveyed to the burster washout station where the burster would be washed out. This would result in an energetic slurry with a nominal maximum particle size of 0.02 in. (0.5 cm) and a slurry concentration not to exceed 20% by weight. The slurry would feed directly to SILVER II, though some quantity may also be pumped to the energetics storage tank as previously discussed. The warhead section would then be deposited in a container tray and conveyed to the metal parts treatment process. The container tray would typically hold 10 to 15 warhead sections.
- The rocket motor and tail section would be conveyed to the propellant removal station where the M28 propellant grain would be pulled from the motor casing. The motor and tail section would be deposited in a container tray for subsequent metal parts washing. The propellant would be conveyed to the propellant size reduction station.
- Fiberglass firing tube sections would be deposited in a container tray and conveyed to the dunnage treatment process for thermal treatment to a 5X condition.

3.2.4.5.3 Munitions Access – Land Mines

The technology provider did not address how it would pretreat land mines in preparing for either agent or energetics treatment. Without this information, it is assumed that agent and energetics would be accessed from the land mines in a manner similar to the baseline technology (see Volume 1, Appendix E for a detailed discussion). In addition, elements of the munitions access process for projectiles and mortars could be applied to land mines. Of the four sites being evaluated in this TRD, only ANAD and PBA contain land mines.

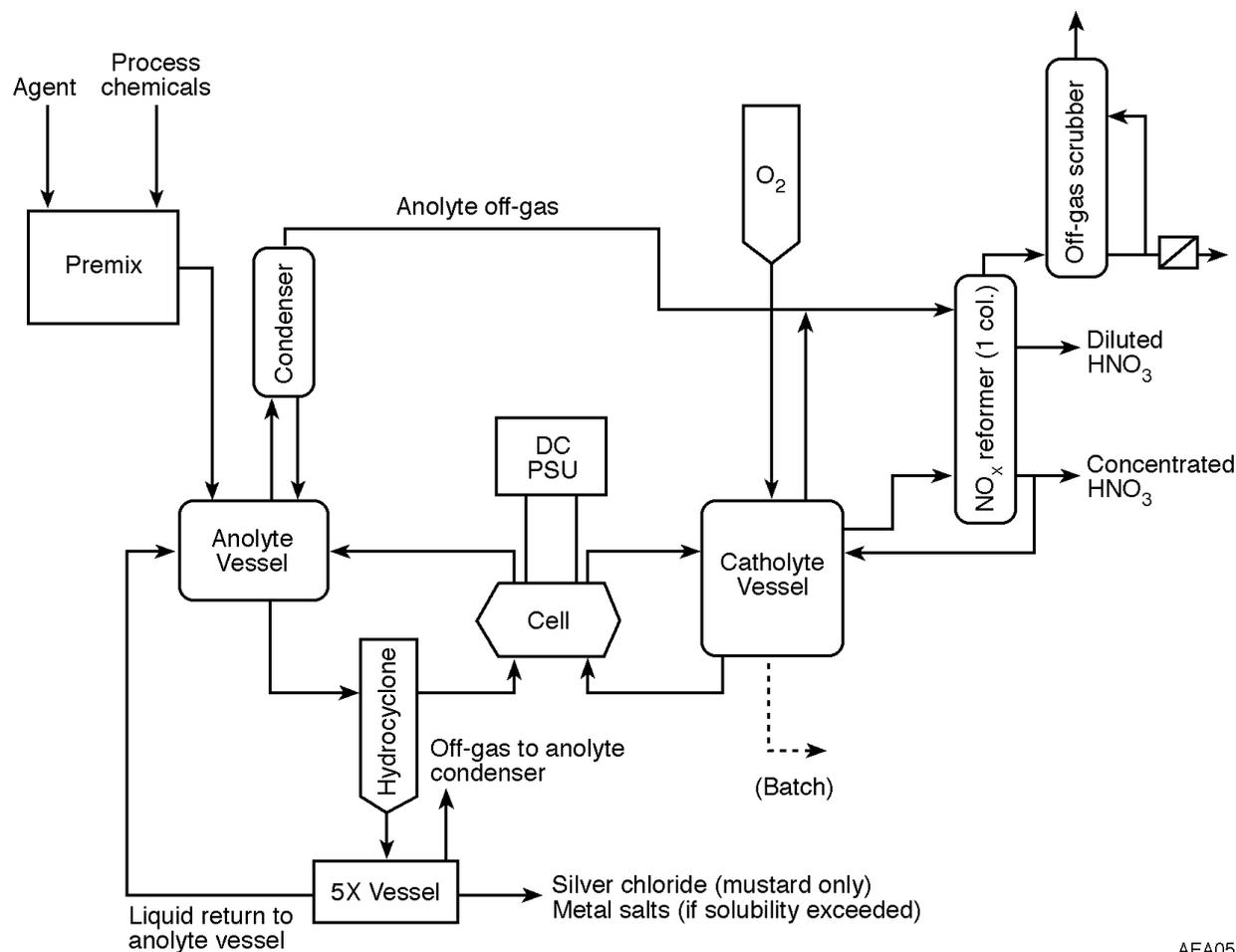
3.2.4.5.4 Agent and Energetics Treatment

Agents and energetics would be destroyed using electrochemical oxidation in the SILVER II process. SILVER II is a mediated electrochemical oxidation process using Ag^{2+} ions in aqueous HNO_3 (formed by an electrochemical cell) that is circulated through CSTRs (anolyte and catholyte circuits). The electrochemical oxidation process uses essentially the same system for destroying both agent and energetics. During demonstration testing, agents were destroyed in a 2-kW electrochemical cell (Figure 3.20) and energetics were destroyed in a 12-kW cell (Figure 3.21). Drained agent, along with liquids condensed from the BRT and MPT (see below), would be destroyed in the agent SILVER II unit. Propellant and high explosives (from bursters) would be destroyed in the energetics SILVER II unit. It is probable that the same kW systems would be used for agent and energetics in the pilot-scale design.

The SILVER II unit would consist of a feed system, an anolyte circuit, and a catholyte circuit integrated with a NO_x reformer and agent and energetics impurities removal systems (AIRS and EIRS, respectively). It is operated at a temperature of 190°F (90°C) and near atmospheric pressure. SILVER II, originally a semicontinuous batch process, is made a continuous process through a “bleed” to impurities removal systems. The AIRS and EIRS are used for impurities removal.

In these removal systems, a purge stream would be withdrawn from the anolyte reservoir. The rate is designed to limit the concentration of impurities in the anolyte to approximately 1-M phosphate and sulfate in order to avoid precipitation of their silver salts. Other impurities of lower flux (such as iron, aluminum, etc.) would be maintained at significantly lower concentrations as a result. In order to recover the silver for reuse, hydrochloric acid would be added to precipitate it as the chloride (AgCl). The silver would be recovered by either gravity settling or in a hydrocyclone. As AgCl may contain small traces of agent, AgCl would be treated to a 5X condition prior to being sent for silver recovery. The condensate from this process would be returned to the catholyte of the SILVER II system. The precipitator overflow would then be fractionally distilled to recover water and HNO_3 for recycle to the SILVER II catholyte (to create the AIRS and EIRS purge flow returns). The evaporator bottoms would contain some residual HNO_3 as well as enriched phosphoric and sulfuric acids. These, together with the HF stream, would subsequently be neutralized with lime to precipitate insoluble fluoride, phosphate, and sulfate salts of calcium. This stream could then be treated to a 5X condition. The condensate would be returned to the catholyte of the SILVER II system.

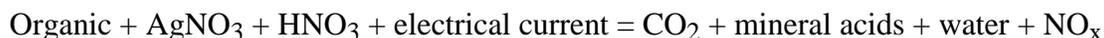
The SILVER II process is based on the highly oxidizing nature of Ag^{2+} ions in a HNO_3 solution. Ag^{2+} ions are among the strongest oxidizing agents known; while HNO_3 also makes a significant contribution to the oxidizing process (NRC 1999). The Ag^{2+} ions are produced at the



AEA05

FIGURE 3.20 Process Flow Diagram for a SILVER II 2-kW Agent Plant Used in Demonstration Testing (Source: Adapted from AEA/CH2MHILL 2000)

anodes of an electrochemical cell (NRC 1999). The overall chemical reaction can be summarized as follows:



Generation of Ag^{2+} ions depends entirely on the electrical current, and it stops when the power is switched off. This process ensures that the reaction is easily controllable. Electrical power to the cell can be shut off safely at any time (e.g., from safety interlocks at other stages of the overall process). A standard industrial electrochemical cell is at the heart of the SILVER II process. Figure 3.22 is a schematic of the 2-kW electrochemical cell used in demonstration testing; Figure 3.23 is a schematic of the 12-kW system used in demonstration testing. Again, it is probable that the same anode/cathode arrangement may be used for agent and energetics in the pilot-scale design.

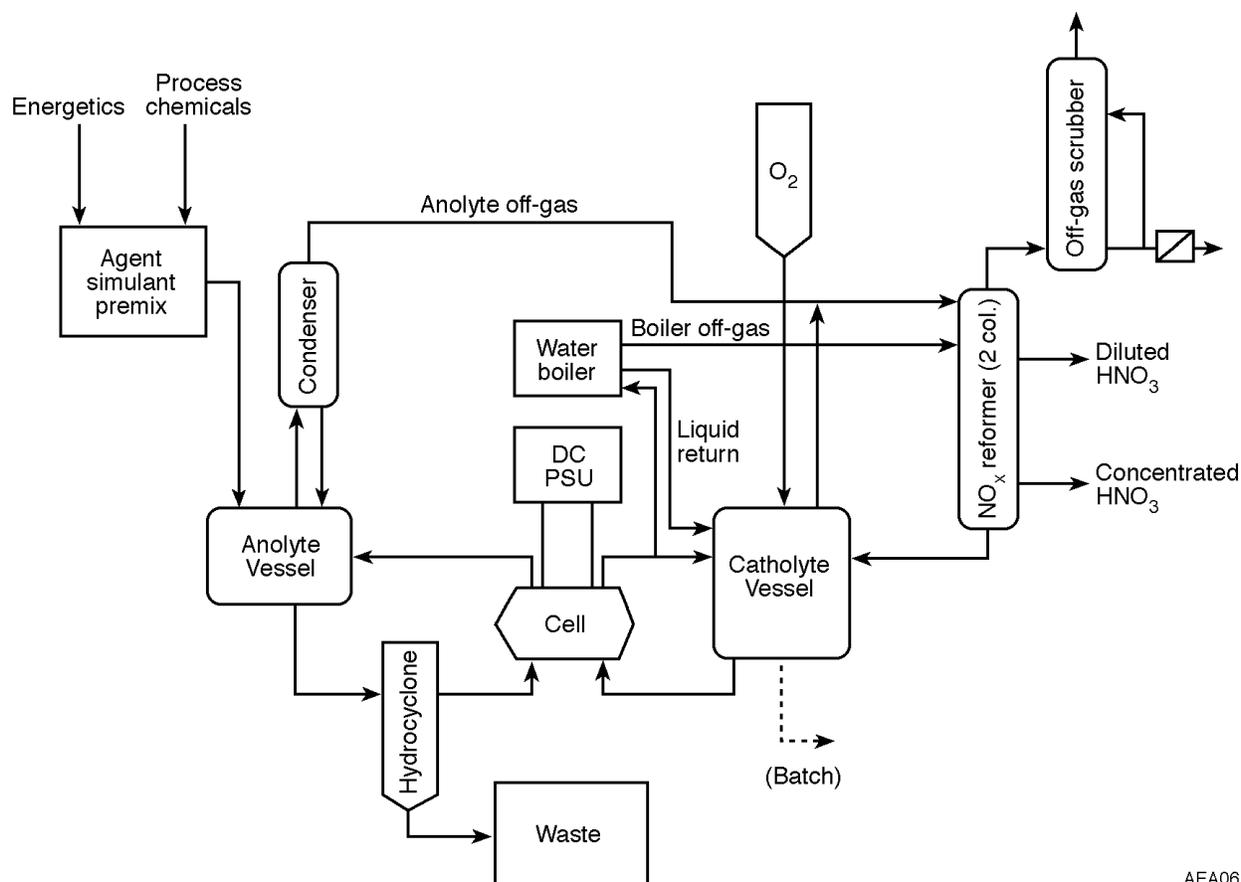


FIGURE 3.21 Process Flow Diagram for a SILVER II 12-kW Energetics Plant Used in Demonstration Testing (Source: Adapted from AEA/CH2MHILL 2000)

The anode and cathode compartments of this cell are separated by a permeable membrane that prevents bulk mixing of the anolyte and catholyte solutions. These solutions are circulated around separate closed loops between the cell and their reaction vessels. The organic material for destruction is continuously metered into the anolyte tank to match the rate of destruction.

Ag^{2+} ions generated at the anode of the electrochemical cell react with the water and HNO_3 of the anolyte solution to form a range of other oxidizing radicals ($\cdot\text{OH}$, $\cdot\text{NO}_3$). In turn, the Ag^{2+} ions and other oxidizing species react with the organic material delivered into the anolyte vessel and are reduced to Ag^{1+} ions, nitrate ions, and water. The organic material is oxidized to CO_2 , NO_x (from the direct reaction with the acid), and traces of CO and protons (H^+ , not hydrogen gas), and inorganic salts. Off-gas from the reaction passes from the anolyte vessel via a condenser (to return HNO_3 and organic vapors) to a NO_x reformer.

To balance the electrochemical reaction in the anolyte, a supporting cathode reaction occurs that involves reducing HNO_3 to nitrous acid and water, while other reduction reactions

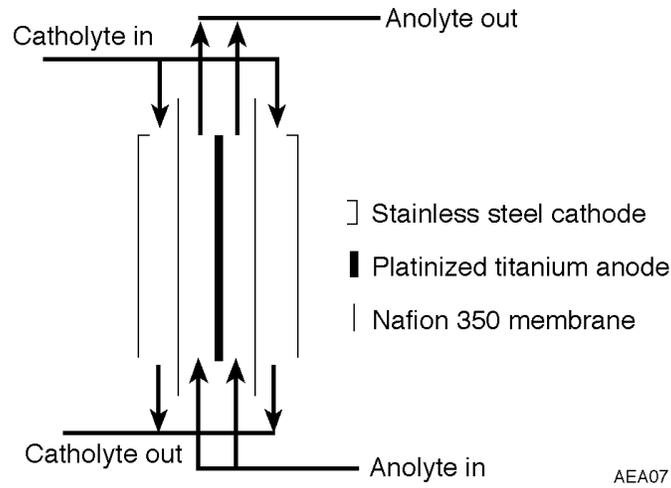


FIGURE 3.22 2-kW Anode/Cathode Arrangement Used in Demonstration Testing (Source: Adapted from AEA/CH2MHILL 2000)

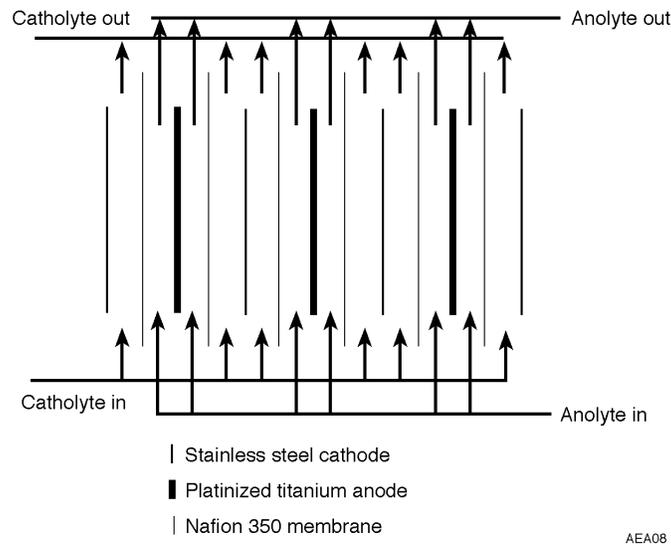


FIGURE 3.23 12-kW Anode/Cathode Arrangement Used in Demonstration Testing (Source: Adapted from AEA/CH2MHILL 2000)

generate nitrogen oxide/nitrogen dioxide (NO/NO₂). The gases pass from the catholyte tank to the NO_x reformer.

The process is operated at a temperature of approximately 190°F (90°C) and at atmospheric pressure. As a result of the electrochemical reaction, HNO₃ is consumed in the catholyte circuit resulting in the formation of gaseous NO_x and water is transferred across the membrane in the electrochemical cell from the anolyte to the catholyte. In addition, Ag¹⁺ ions are also transferred across the cell membrane, together with a small amount of organic material, depending on the organic feed to SILVER II. To maintain steady-state operating conditions, the operation incorporates internal recycle streams to return the silver and organic material to the anolyte circuit. This ensures that a buildup of organic material or silver in the catholyte does not occur, and that steady-state conditions can be maintained.

The off-gas streams from the anolyte and catholyte circuits are combined and sent to the NO_x reformer system. The reformer recovers the NO_x by removing it from the gas stream and recycles it into concentrated HNO₃ for return to the anolyte and catholyte circuits as required; or alternatively, the excess can be marketed as a product. A dilute HNO₃ stream of less than 1% weight is also produced. The technology provider plans to send this material to either an on- or off-site wastewater treatment plant. The dilute HNO₃ stream may also be recycled within the plant.

The post-treatment portion of SILVER II also consists of a caustic scrubber circuit and a number of CSTRs for pH adjustment. NO_x in the off-gas is collected by a NO₃ absorber column and reformed to HNO₃ that is concentrated in a packed bed distillation column. The remaining off-gas from the NO_x reformer goes to a caustic scrubber for acid neutralization. Hydrofluoric acid distilled by the AIRS is neutralized with lime in a CSTR. Similarly, dilute HNO₃ waste is pH neutralized with caustic.

After leaving the NO_x reformer, all off-gas passes through a caustic scrubber to remove very low levels of residual NO_x, thus leaving a stream of CO₂, oxygen, and water vapor. The off-gas is then tested to ensure that no agent is released from SILVER II. This off-gas stream is then processed through the catalytic oxidation process as a polishing step to ensure that trace organics are destroyed. Silver chloride (AgCl) is precipitated when mustard agent is exposed to the HNO₃ and AgNO₃ in the anolyte vessel. In the anolyte circuit, a hydrocyclone is used to continuously remove the AgCl from the recirculating liquid before it reaches the electrochemical cell.

The AgCl is accumulated in a settling vessel and discharged into an oven for 5X treatment on a batch basis. The vapor from the oven is passed to a condenser, and the condensate is returned to the anolyte vessel for destruction of any organic material that may be present. The AgCl is then removed as a solid cake for silver reclamation. Silver reclamation may be conducted on- or off-site.

3.2.4.5.5 Metals Parts Treatment

Metal parts would be treated to achieve a 5X condition in the MPT, as explained previously. The objective of this unit operation would be to elevate the temperature of the parts to over 1,000°F (538°C) for a period of at least 15 minutes. The PMACWA previously demonstrated this concept at CAMDS and during the ACWA Demo I. Metal parts treatment would be accomplished in a chamber designed to receive the various metal parts containers, such as the projectile casing conveyance trays. The metal parts containers would be automatically conveyed into the chamber. The chamber would use electrical heating elements to achieve the design temperature. Steam would be passed through the chamber to enhance the exposure of metal to elevated temperatures and to establish the conditions of 5X treatment. The discharged steam would be condensed, and the off-gas would be sent to the catalytic oxidation process for destruction of trace organic compounds, and then to carbon filtration, before discharge to the atmosphere. Two decontamination chambers would be used so that one chamber would be in load and 5X treatment phase, while the second chamber would be in the cool-down and unload phase. Decontaminated metal parts would be transported off-site for either recycle or disposal, in accordance with regulatory requirements.

The specific design of the detonation chamber would be optimized during EDS II. The conceptual design, however, indicates that two detonation chambers would be sufficient to provide adequate capacity and to provide redundancy to deactivate fuzes, boosters, and supplemental charges. The chamber would be loaded with a preapproved number of fuzes and detonation charges. The controlled detonation would deactivate the fuzes. The resulting metal fragments would be conveyed to the metal parts treatment process. Off-gas from the chamber would be processed through the catalytic oxidation process and subsequently through carbon filters prior to discharge.

3.2.4.5.6 Dunnage Treatment

Dunnage treatment would use the same principle as that for metal parts to achieve 5X decontamination. Contaminated dunnage would be stored in a silo contained within the MDB and would be fed to a two-stage shredder for size reduction to nominal 2- to 3-in. (5- to 8-cm) particle sizes. This would be accomplished using commercially available shredding equipment. The shredded dunnage would be mechanically conveyed to the BRT. As indicated previously, this is essentially the same as the MPT, except that it is a rotary oven that operates as a continuous process. The chamber would be designed to expose the shredded dunnage to the design temperature for a resident time of 30 minutes to provide a reasonable safety factor. Treated dunnage would be discharged into a storage hopper for subsequent placement in a landfill in accordance with regulatory requirements.

The BRT thermally treats fluid-cutting grit and size-reduced, solid (mostly nonmetallic) secondary wastes (dunnage and rocket shipping and firing containers). The BRT is similar to the MPT; however, it operates in continuous mode. Off-gas from the MPT and the BRT (mostly

steam) would be condensed and sent to SILVER II for treatment. All process off-gas would be mixed with air, treated with a catalytic oxidation system, and passed through carbon filters before release to the atmosphere.

3.2.4.5.7 Effluent Management and Pollution Controls

The SILVER II process produces various types of waste. The process off-gases would be passed through a catalytic oxidation unit, carbon filtered, and tested (with carbon filter rework as necessary) before exhausting to the atmosphere. Liquids would be separated by evaporator/condensers and would be reused (on- or off-site) or sent off-site for treatment as necessary, and disposal. Evaporator bottoms from the impurities removal systems would be treated as necessary and disposed of off-site. The pH-adjusted acid streams would undergo on- or off-site wastewater treatment. Solids from HF neutralization would be dewatered in a filter press, treated as necessary, and placed in a landfill. Metals that have been decontaminated to a 5X condition would be recycled, and 3X and 5X solids would be treated as necessary and placed in a landfill. All waste management would be conducted in compliance with regulatory requirements. As indicated previously, wastes determined to be hazardous may be delisted from being hazardous waste if regulatory delisting criteria are met.

Silver is used to catalyze the oxidation of organics. Normally, this silver remains in solution, except in those instances when compounds containing chlorine are present. Silver combines with chlorine (contained in mustard agent) to create AgCl, which must be removed from the system. This is accomplished by using hydrocyclones that separate the precipitated AgCl from the anolyte solution in the plant. The material is then decontaminated in a 5X oven. The resulting material would be collected and transported off-site. Silver would be reclaimed at a commercial facility. If necessary, this reclamation process can occur on-site.

Concentrated HNO₃ is a product of the SILVER II process when treating energetic materials that contain nitrogen. Materials can be transported off-site for reuse in the manufacture of energetics. Dilute HNO₃ is also produced. This material could be recycled within the system. Any unrecycled dilute HNO₃ would be neutralized with scrubber waste and discharged to an on- or off-site wastewater treatment plant. Any materials sent off-site would need to meet U.S. Army safety standards.

3.2.4.6 Common Elements – Other Systems

The electrochemical oxidation process has several elements that are identical or nearly identical to other systems. This commonality is particularly evident in pretreatment processes. Commonalities with other applicable technology systems include the following:

- The munitions access system used for electrochemical oxidation using SILVER II employs much of the baseline reverse assembly system, as do most of the other ACWA systems.
- Similar to the neutralization/biotreatment process, the munitions access system for the M55 rockets employs fluid jet cutting and fluid-mining to access energetics.
- Process off-gas is passed through catalytic oxidation units prior to carbon filtration and release to the atmosphere. This is also similar to the neutralization/biotreatment process and the neutralization/GPCR/TW-SCWO process.
- Dunnage would be size-reduced and treated in a manner similar to the neutralization/biotreatment technology.
- Decontamination of metal parts would occur thermally to a 5X condition using steam. The process would subject the parts to temperatures in excess of 1,000°F (538°C) for a period of more than 15 minutes. This process is similar to that used in the neutralization/biotreatment technology.

Facility structure; ventilation; decontamination fluid supply; personnel support; pollution abatement; water, air, and steam supply systems; control rooms; monitoring systems; and laboratory support would be identical or nearly identical to the baseline system.

3.2.5 COMBINATION TREATMENT TECHNOLOGIES

Given the commonalities of the various technology systems, the elements of the various unit operations could be combined into different, but viable, ACW treatment alternatives. A number of different combination technologies may be considered. The following are examples of several combination technologies that could be employed:

- The fluid-abrasive cutting and fluid-mining technologies of neutralization/biotreatment can be used with any system;

- The specific units proposed for agent and energetic hydrolysis in neutralization/SCWO, neutralization/biotreatment, or neutralization/GPCR/TW-SCWO systems can be interchanged;
- The metal parts treatment technologies proposed for neutralization/SCWO, neutralization/biotreatment, or neutralization/GPCR/TW-SCWO are interchangeable;
- The CatOx unit used in neutralization/biotreatment, neutralization/GPCR/TW-SCWO, and in electrochemical oxidation can be employed with any technology system; and
- Carbon filtration as used in the baseline process and in most of the ACWA technologies may be used with any technology system.

3.3 SUPPLEMENTAL INFORMATION FOR ASSEMBLED SYSTEMS AT PINE BLUFF ARSENAL

This section provides supplemental information for pilot testing ACWA technology systems at PBA. Included are facility descriptions, system inputs and resource requirements, routine emissions and wastes, and activities and schedules. This section addresses construction and operation of the facility. As the pilot-scale facility designs mature, deviations are expected. However, it is anticipated that the final design would result in estimates similar to those provided in the tables in this section.

3.3.1 GENERAL FACILITY LOCATION AND FOOTPRINT

For the purposes of NEPA assessment, it has been assumed that all ACWA program facilities would be constructed within the north-central portion of PBA, adjacent to the chemical demilitarization area, where ACW are stored. Figure 3.24 shows two possible sites (Sites A and B) for the demilitarization facility within this area. Site C, as shown in Figure 3.24, has been set aside for other purposes and is not available for ACWA activities. Figure 3.24 also shows a portion of the northern part of the facility (north of Area B) that is not part of PBA. Ownership of this portion of the facility is being transferred to the U.S. Food and Drug Administration.

Site A is adjacent and to the east of the existing ACW storage area. Site B is located approximately $\frac{3}{4}$ mi (1.2 km) northeast of the ACW storage area. This analysis focuses on the potential location of the ACWA facility within Area A or B. The exact location of the destruction facility within these areas has yet to be determined. It is possible that multiple ACWA technologies could be tested at PBA.

In general, the physical size of the destruction facility for ACW at PBA is expected to be comparable to that required for baseline incineration. For each technology system, the facility is expected to cover approximately 20 to 30 acres (8 to 12 ha), with an additional land area of up to 20 acres (8 ha) for construction support facilities. Additional acreage may be required for access roads and utilities; the area required would be determined on a site-specific basis. The facility size may differ slightly as a function of the technology system alternative. Table 3.5 provides approximate distance information for each of the sites. Table 3.6 provides land area requirements during operations.



FIGURE 3.24 Map Showing Two Potential Facility Locations for the Demilitarization Facility at PBA (Note: Site C is not available for ACWA activities.)

TABLE 3.5 Approximate Distances from Potential Demilitarization Facility Locations A and B to PBA Installation Boundaries^a

Location	Distance to North PBA Boundary	Distance to South PBA Boundary	Distance to East PBA Boundary	Distance to West PBA Boundary
A	1.1	5.6	3.0	1.1
B	0.2	6.5	2.3	1.5

^a Distance (in miles) determined from the approximate midpoint of Areas A and B, respectively, as shown in Figure 3.25.

TABLE 3.6 Land Area Requirements during Technology System Operations

Technology	Land Area for Operations (acres)
Baseline incineration	20
Neutralization/SCWO ^a	20–30
Neutralization/biotreatment ^b	20
Neutralization/GPCR/TW-SCWO ^c	25
Electrochemical oxidation	20

^a Based on Figure 4.4-8 in General Atomics (1999).

^b Based on Figure 4.3.1-1 in Parson/Allied Signal (1999) and stated similarity to incineration facility layout.

^c Based on PMACWA (2001c).

The land area required during construction may be greater than that required during operations because of the need for the following:

- A construction lay-down area for temporary storage of construction materials such as structural steel, pipe, lumber for concrete forms, and electrical conduit;
- Temporary construction offices for housing on-site engineering, construction supervision, and management personnel;
- Temporary parking for construction workers and support personnel;

- Temporary holding basins for control of surface water runoff during construction; and
- Areas for installing required temporary utilities and services, including construction service water, sanitary facilities, electrical power, and vehicle fuels.

The additional land area needed for construction-related activities would, in general, be about 10 to 20 acres (8 to 12 ha). This analysis conservatively assumes that a total of 50 acres (20 ha) would be required for construction purposes. Examination of the available land area at Sites A and B indicates that the above construction-related areas would be readily available at each of these locations.

For Site A, existing security fencing along the perimeter of the current chemical storage area would be extended to include the proposed ACW destruction site, thereby creating a contiguous fenced area around the storage area and the destruction site. The storage area and destruction site would be separated by security fencing to control access. Site B would be surrounded by separate security fencing.

A buffer area around the proposed destruction site would be established as defined by the Public Access Exclusion Distance required by the U.S. Army. This distance is defined as the greater of either the fragmentation hazard distance or the 1% lethality distance (U.S. Army 1997). Site personnel not directly associated with the demilitarization operation would be excluded from the buffer area defined by this distance, or provision would be made for their protection or evacuation.

Construction of the demilitarization facility would involve small amounts of excavation and fill work. Construction debris would be transported off-site to a commercial disposal facility. A drainage system would be established for the facility to divert surface runoff from the plant site and prevent erosion and accumulation of surface water on the facility. Moderate clearing and earthwork would be required in Areas A, B, and C.

3.3.2 NEUTRALIZATION/SCWO

This description of the neutralization/SCWO facility is based on preliminary design information provided in General Atomics (1999). The PMACWA and the technology provider have provided information on application of this technology to PCD and BGAD (PMACWA 1999a). The technology provider did not supply specific information for application of the technology to PBA (General Atomics 1999). The information and estimates provided for this installation are based, in part, on information provided for application of this technology to PCD and BGAD. Many of the estimates provided in that facility design information refer comparatively to the U.S. Army baseline incineration process, which indicates, in general, that estimates are comparable to those

for the baseline incineration process (General Atomics 1999). Thus, another of the primary sources of information for this section of the TRD is the EIS for disposal of chemical agents and munitions stored at Pine Bluff Arsenal, Arkansas (PMCD 1997). That EIS is the most recent EIS that the U.S. Army has prepared for baseline incineration of chemical munitions.

In addition to the above, mass balance estimates, air emission estimates, and solid waste estimates for application of the neutralization/SCWO technology at PBA have been developed (Mitretek 2001b). Air emissions and solid waste estimates for neutralization/SCWO, as discussed below, are based on Mitretek inputs, along with appropriate assumptions on filtration systems and plant operations and schedule (Mitretek 2001b). Figure 3.25 provides an input/output material balance for the major streams generated during neutralization/SCWO of ACW containing nerve agent.

Many of the figures and tables referred to in the facility description for this technology system contain estimates (e.g., emissions resources consumed) associated with processing ACW with a specified agent; these estimates are given on an annual basis (e.g., tons/yr). In some cases, the estimates have been converted from other units (e.g., lb/d) by accounting for the number of days of operation required for processing a specific type of ACW. This time period is referred to as a campaign; a campaign is agent-specific. The values in many of the following figures and tables are based on the number of days in the campaign required to process ACW containing a specific agent. It was assumed that there are 276 operating days in a year. If the campaign is less than or equal to 276 days, annual quantities equal total quantities. If the campaign is greater than 276 days, quantities in the figures and tables are for 276 days of processing. In the latter case, the estimates provided are less than total quantities. Daily (or other) quantities may be obtained by adjusting for the number of days in the campaign.

3.3.2.1 General Facility Description

The proposed neutralization/SCWO facility is designed to fit approximately into the same space and general configuration as the baseline incineration process. Munitions access and disassembly, neutralization, and SCWO operations have been substituted for baseline incineration operations. The physical plant would consist of a two-story building constructed of noncombustible materials, with a concrete structural frame and a low-slope concrete roof.

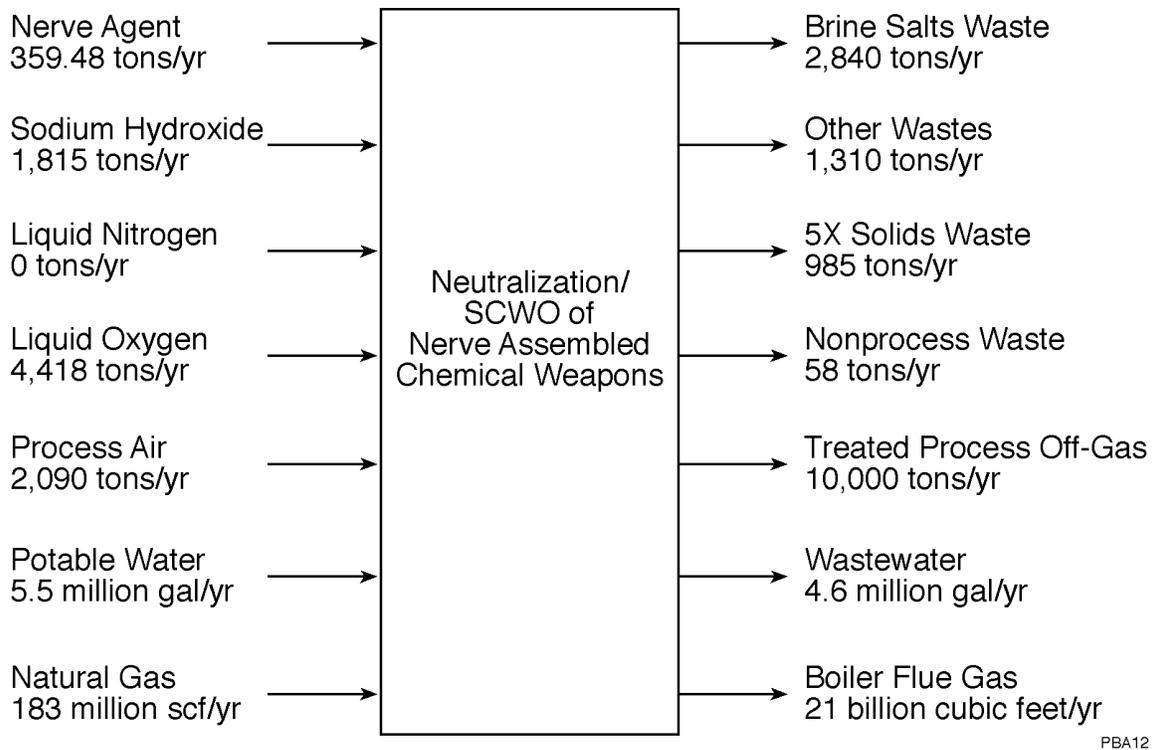


FIGURE 3.25 Input/Output Material Balance for Neutralization/SCWO of ACW Containing Nerve Agent at PBA

The site layout for neutralization/SCWO is shown in Figures 3.26 through 3.28. Figure 3.26 shows the general facility layout, Figure 3.27 shows the layout of the first floor, and Figure 3.28 shows the layout of the second floor.

3.3.2.2 Construction Phase

The schedule for destruction of the stockpile at PBA calls for construction of the selected alternative to begin following issuance of the EIS Record of Decision (ROD) and receipt of the RCRA and any other environmental permits, as necessary. It is anticipated that the construction schedule for the neutralization/SCWO facility would not differ significantly from that required for baseline incineration. Construction would take approximately 32 months (PMCD 1999b), including a two-month design and procurement verification period. However, the PMACWA is investigating means of shortening the construction phase.

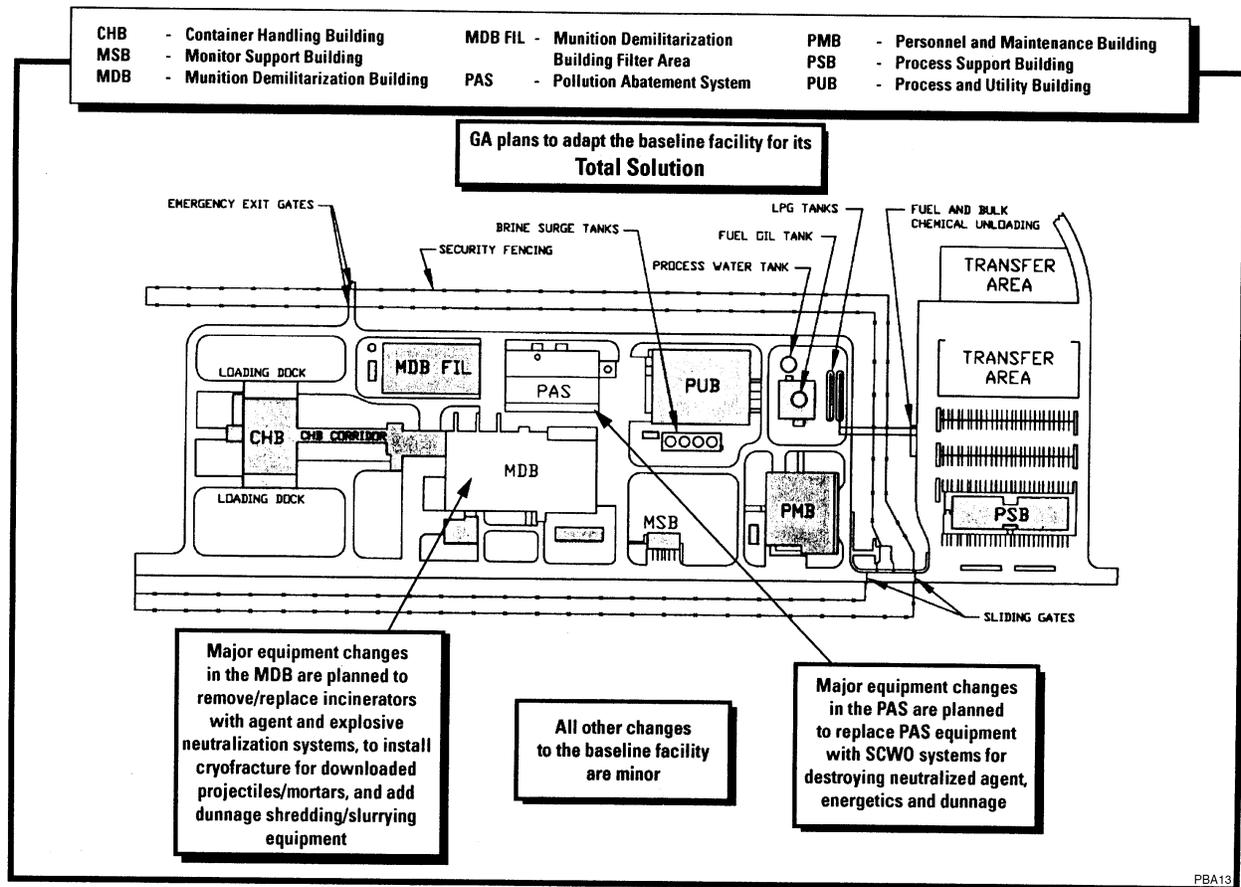
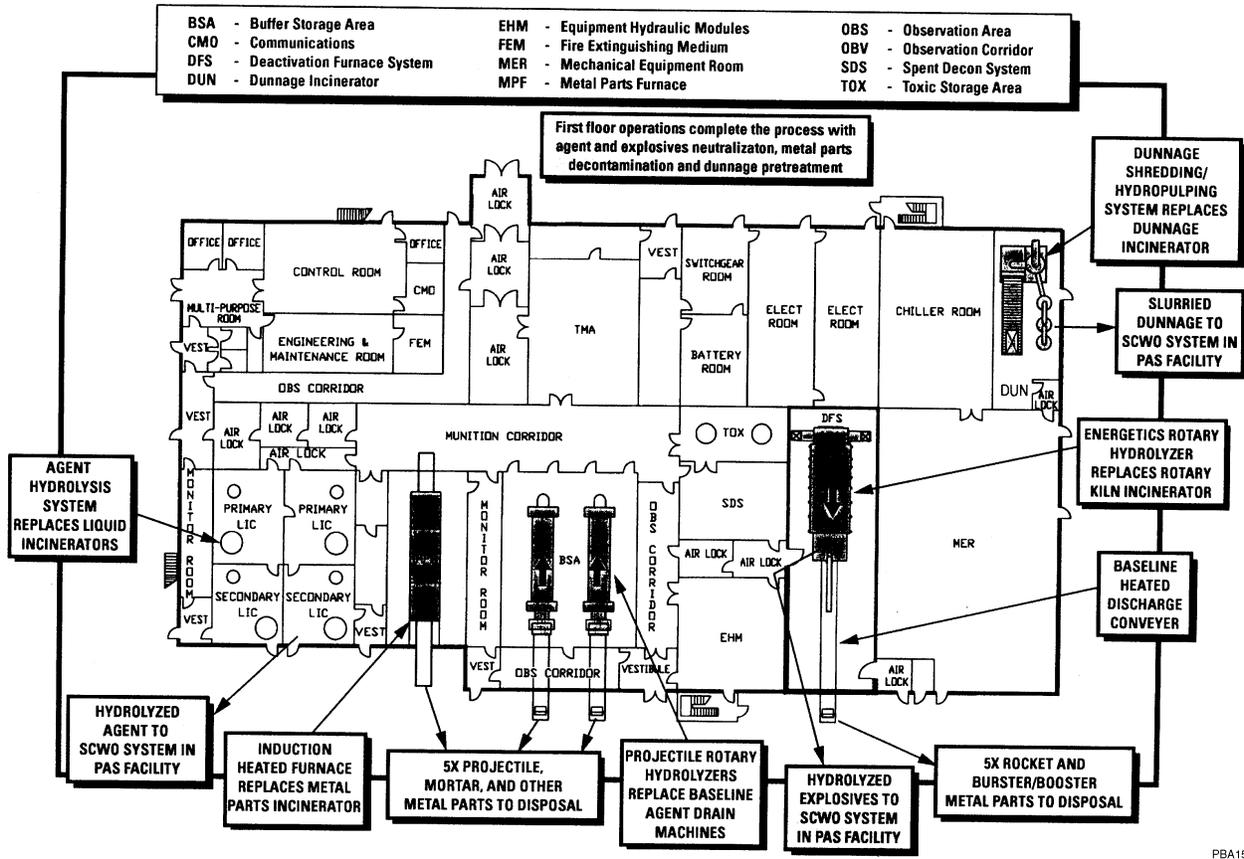


FIGURE 3.26 Neutralization/SCWO Facility Arrangement at PBA (Source: General Atomics 1999)

On January 15, 1999, Arkansas regulators approved permit applications for the PBA incinerator. The same day, the U.S. Army issued a construction notice to proceed at the PBA site to Raytheon Engineers and Constructors, Inc., of Cambridge, Massachusetts (Wright 1999). The incinerator facility at PBA is expected to start operations in 2003 to destroy 12.3% of the nation’s original stockpile of chemical weapons (Findtner 2000).

Construction of the destruction facility on the PBA installation would result in vehicle exhaust emissions, fugitive dust, noise, destruction of wildlife habitat and native vegetation, increased employment, increased demand for public services, and occupational health hazards.



PBA15

FIGURE 3.28 Layout of Second Floor of the Munitions Demilitarization Building for the Neutralization/SCWO Facility at PBA (Source: General Atomics 1999)

The process equipment would be purchased from equipment vendors. Specialty materials, such as Inconel or Monel, do not appear to be required. However, the SCWO reactors may require platinum or an alternative specialty material as an anticorrosive barrier in the final design (PMACWA 1999a).

Table 3.8 provides an order-of-magnitude estimate of the number of shipments of construction materials to the site. The estimate does not include process equipment and related items; the number of shipments associated with these resources is expected to be small in comparison with the estimate of 5,000 total shipments.

An order-of-magnitude estimate of the emissions from construction delivery vehicles to the site is provided in Table 3.9, assuming a one-way trip distance of 20 mi (32 km) and delivery by heavy-duty diesel trucks. The actual trip distances would depend on several factors, including the availability of construction materials from local distributors and the distance of the site from the distributors.

TABLE 3.7 Estimated Materials/Resources Consumed during Construction of a Neutralization/ SCWO Facility at PBA^a

Construction Material/Resource	Total Consumption	Peak Demand
Utilities		
Water ^b	8,000,000 gal	NA ^c
Electricity ^c	57,000 MWh	2.85 MW
Solids		
Concrete	32,000 yd ³	NA
Steel (structural and reinforcing)	7,100 tons	NA
Piping (all)	123,000 linear ft	NA
Liquids		
Fuel	2.4E+06 gal ^d	NA
Gases		
Industrial gases (propane)	6,400 gal	NA

^a All values can be considered order-of-magnitude approximations of the actual values; more accurate values would require a detailed consideration of construction activities.

^b The water requirement was estimated on the basis of DOE (1997), in which each full-time equivalent (FTE) required 20 gal/d, and solidification required 26 lb per 100 lb of cement.

^c NA = not applicable.

^d This system of notation is equivalent to $N \times 10^{+x}$; for example, 2.4E + 06 equals 2.4×10^6 .

3.3.2.2.2 Construction Workforce

The construction workforce is expected to steadily increase to a peak of about 1,000 full-time equivalent (FTE) employees near the midpoint of the construction period, and then to decrease steadily until construction is completed. The average number of construction workers is estimated to be approximately 520 FTEs. When a 32-month construction period is assumed, approximately 1,400-FTE-years of effort would be expended during construction. Table 3.10 provides an estimate of the employment buildup by year during construction.

3.3.2.2.3 Construction Emissions and Waste Estimates

During the construction phase, fugitive emissions would consist mainly of dust and vehicle exhaust. Temporary, regional increases in atmospheric concentrations of CO, NO_x,

TABLE 3.8 Order-of-Magnitude Estimate of the Number of Truck Shipments of Construction Materials for a Neutralization/SCWO Facility at PBA^a

Resource	Total Consumption	Truck Capacity	No. of Truck Shipments
Portland cement ^b	3,520 yd ³	10 yd ³	352
Gravel ^b	13,120 yd ³	10 yd ³	1,312
Sand ^b	8,320 yd ³	10 yd ³	832
Steel ^c	7,100 tons	21 tons	340
Asphalt paving ^d	1,400 tons	20 tons	70
Backfill ^e	12,800 yd ³	10 yd ³	1,280
Fuel ^f	2.4E+06 gal	9,000 gal	270
Total			4,456
Total (rounded up)			5,000

- ^a The calculation did not include process equipment and related items.
- ^b Assumes that concrete is composed of 11% portland cement, 41% gravel, and 26% sand and is shipped to the site in a standard 10-yd³ end-dump truck.
- ^c Assumes that the net payload for steel transport to the site is 42,000 lb.
- ^d Assumes that hot mix asphalt (HMA) is loaded into 20-ton-capacity triaxle trucks for transport to the paving site.
- ^e Assumes that shipment is in standard 10-yd³ end-dump trucks and that no fill material is available on-site.
- ^f Assumes that shipment is in a U.S. Department of Transportation (DOT) 406/MC-306 atmospheric pressure tank truck with 9,000-gal capacity.

hydrocarbons, particulate matter, and sulfur oxides (SO_x) would result from the exhaust emissions of commuter vehicles, heavy construction vehicles, diesel generators, and other machinery and tools. Annual emissions of these pollutants would be small in comparison to de minimis levels typically used by regulators to determine whether an air quality permit or impact analysis is necessary. Emissions from construction vehicles are exempt from permit requirements. Nevertheless, vehicles and machinery would be equipped with standard pollution control devices to minimize air quality impacts.

Estimated emissions from construction activities (not including emissions from commuter and delivery vehicles) are listed in Table 3.11. The emissions listed are based on the

TABLE 3.9 Estimated Emissions from Delivery Vehicles during Construction of a Neutralization/SCWO Facility at PBA

Criteria Pollutant ^a	No. of Auto Round Trips ^b	Emission Factor (g/km) ^c	One-Way Trip Distance (mi) ^d	Construction Period (yr)	Emission Rate (ton/yr)
HC	5,000	2.12	20	2.7	0.3
CO	5,000	11.28	20	2.7	1.5
NO _x	5,000	1.25	20	2.7	0.2
SO _x	5,000	0.23	20	2.7	0.03
PM ₁₀	5,000	0.617	20	2.7	0.1

^a Abbreviations: CO = carbon monoxide, HC = hydrocarbons, NO_x = nitrogen oxides, PM₁₀ = particulate matter with a diameter less than or equal to 10 micrometers, SO_x = sulfur oxides.

^b Number of auto round trips to the construction site estimated on the basis of the total number of deliveries.

^c Emission factors were determined by using the U.S. Environmental Protection Agency (EPA) modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^d One-way trip distance based on DOE (1997).

TABLE 3.10 Estimated Number of Employees Needed by Year for Construction of a Neutralization/SCWO Facility at PBA

Employees	Year 1	Year 2	Year 3
Total craft workers	310	630	140
Construction management and support staff	80	160	40
Total	390	790	180

anticipated construction land disturbance and vehicle traffic (for dust particulate pollutants) and fuel and gas consumption. The column marked "Total" indicates the total amount of emissions that is estimated to occur over the entire construction period.

Emissions from construction worker commuter vehicles were estimated on the basis of the assumption that an average of 511 automobiles (1 car per construction worker) would be added to the area. Table 3.12 gives the annual emissions estimates due to the increased traffic.

Additional emissions would result from the use of paints and thinners, aerosols, and other area source emissions. These emissions are expected to be minor contributors to air pollution and were not included in current estimates.

Construction would generate solid wastes primarily in the form of excavation spoils and building material debris. These latter wastes would include concrete forms, equipment and hardware containers and packaging, paint cans, waste metal sheeting, pipe and wire, and landscaping debris. Small amounts of liquid wastes, such as solvents, cleaning solutions, and paint wastes, also would be generated. Wastes would be collected and disposed of in compliance with U.S. Army, federal, state, and local requirements. All construction debris would be removed from the site for disposal. Any batteries, used motor oils, and empty containers would be separated from the waste stream and recycled. Any wastes identified as hazardous would be stored and disposed of in accordance with RCRA requirements. Sanitary wastes would be the only significant liquid effluent generated during construction and would be managed on-site.

Estimated total quantities of solid and liquid wastes generated from activities associated with facility construction are listed in Table 3.13. The waste generation quantities are based on historical data on land area size and the construction labor force.

3.3.2.3 Operations Phase

Information on the facility operations phase is presented in this section. Preoperational testing is discussed first, followed by facility inputs and resource requirements, workforce requirements, and emissions and waste estimates.

3.3.2.3.1 Preoperational Testing

A preoperational testing period assumed to last between 8 and 15 months would begin following facility construction (PMACWA 1999b). Often referred to as systemization, this period would be used to ensure that systems are operating as designed prior to pilot-scale

TABLE 3.11 Estimated Criteria Pollutant Emissions during Construction of a Neutralization/SCWO Facility at PBA

Criteria Pollutant	Total (tons)	Annual (tons/yr)
CO	121	45
HC	51	19
NO _x	179	67
SO _x	12	5
Particulates ^a	522	196

^a Estimated assuming that 50 acres would be disturbed during construction.

TABLE 3.12 Estimated Emissions from Worker Commuter Vehicles during Construction of a Neutralization/SCWO Facility at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Emission Rate (tons/yr)
HC	123,000	1.16	20	10.1
CO	123,000	11.38	20	99.1
NO _x	123,000	0.73	20	6.4
SO _x	123,000	0.12	20	1.0
PM ₁₀	123,000	0.055	20	0.5

^a The number of auto round trips to the construction site estimated on the basis of the average construction personpower and an assumption of 240 work days per year.

^b Emission factors were determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

operations. On the basis of similarity with baseline (incinerator) operations at ANAD (U.S. Army Corps of Engineers [COE] 2000), it is projected that approximately 300 FTEs would be needed at the peak of preoperational testing.

3.3.2.3.2 Operations Inputs and Resource Requirements

At full-scale operation, destruction of the nerve agent inventory at PBA is projected to require 484 days for processing (Mitretek 2001b). Destruction operations at PBA are projected to require approximately 22 months at full-scale operation (see Table 3.14). This duration is based on 12-hours-per-day, 6-days-per-week, 46-weeks-per-year, operations with one 6-week agent/munition changeover period and one 2-week munition changeover period (General Atomics 1999).⁵⁸ For comparison, incineration of the entire chemical agent inventory at PBA is projected to require 40 months (PMCD 1999b). Because baseline incineration at PBA would include destruction of mustard agent in TCs (which are not considered ACW), this option would require a longer period of operation.

Annual utility consumption for facility operation is presented in Table 3.15. Table 3.16 lists the annual use of consumable chemical and process material during nerve agent processing. These estimates are based on an assumed average or normal throughput. Liquid nitrogen would not be required for cryofracture purposes at PBA, because the inventory at the site includes only rockets and mines, which are not disassembled by using cryofracture.

⁵⁸ The full-scale scenario has been selected as the bounding case for this analysis.

TABLE 3.13 Estimated Total Wastes Generated during Construction of a Neutralization/SCWO Facility at PBA

Waste Category	Quantity
Hazardous solids	90 yd ³
Hazardous liquids	38,000 gal
Nonhazardous solids	
Concrete ^a	210 yd ³
Steel ^b	36 tons
Other ^c	1,700 yd ³
Nonhazardous liquids	
Sanitary ^d	5.5E+06 gal
Other	2.5E+06 gal

- ^a Amount of concrete (nonhazardous solid) waste was estimated by assuming that 0.65% of the concrete usage is spoilage.
- ^b Amount of steel waste stream was estimated as 0.5% of the steel requirement on the basis of a report by Lawrence Livermore National Laboratory and others (LLNL et al. 1997).
- ^c Amount of other stream estimated as eight times the concrete stream on the basis of LLNL et al. (1997).
- ^d Amount of sanitary waste was estimated on the basis of the total construction workforce.

TABLE 3.14 Inventory and Estimated Processing Time for Neutralization/SCWO of ACW Stored at PBA

Munition	Quantity	Agent	Processing Rate (no. of munitions/h)	Processing Time		Changeover (weeks)	Total (weeks)
				Hours	Weeks ^a		
M55 rocket	90,231	GB	20	4,512	62.7	0.0	62.7
M55 rocket	19,582	VX	20	979	13.6	6.0	19.6
M23 land mine	9,378	VX	30	313	4.3	2.0	6.3
Total	119,191			5,803	80.6	8.0	88.6

^a Estimated by assuming 6-days-per-week operations, 12 hours per day.

TABLE 3.15 Estimated Utilities Consumed during Destruction of ACW at the Neutralization/SCWO Facility at PBA

Utility	Average Daily Consumption	Peak-Day Consumption	Annual Consumption
Process water ^a	22,000 gal/d	600 gal/min	6,100,000 gal/yr ^b
Potable water ^a	15,000 gal/d	170,000 gal/d	5,480,000 gal/yr ^b
Fire water ^a	NA ^c	3,000 gal/min	NA
Sanitary sewer ^a	20,650 gal/d	395 gal/min	7,540,000 gal/yr ^b
Natural gas	190,000 scf/d	15,000 scf/h	52,000,000 scf/yr ^d
Fuel oil	962 gal/d	406 gal/h	48,000 gal/yr ^e
Electricity	163 MWh	8.0 MW	59.6 GWh ^f

^a Assumed to be similar to incineration because the number of operations and maintenance personnel and land area are unchanged from incineration.

^b Based on 365 days of operation per year.

^c NA = not applicable.

^d Based on 276 days of operations.

^e Based on 600 hours of operations per year.

^f Based on an average power rating of 80%.

Source: PMCD (1997).

TABLE 3.16 Estimated Raw Materials Consumed Annually during Normal Neutralization/SCWO Operation at PBA, Nerve Agent Processing

Material	Average Daily Consumption (lb/d)	Annual (tons/yr) ^a
LN ₂	0	0
Liquid oxygen (LOX)	32,000	4,400
Water in caustic solution	14,800	2,000
NaOH	13,000	1,800
Phosphoric acid (H ₃ PO ₄)	8,800	1,200
Kerosene for SCWO	6,000	829
Air for SCWO and HDC	1,500	2,100

^a Estimated by assuming 276 days of operations per year (nominal campaign length of 484 days).

Source: Mitretek (2001b).

Table 3.17 gives transportation data for annual shipment of input material streams into PBA for nerve agent processing. Hazardous materials shipped to the site include corrosives such as NaOH and H₃PO₄, combustibles (kerosene), and a nonflammable gas-oxidizer (oxygen). The oxygen would be transported to the site as a liquid.

3.3.2.3.3 Operations Workforce

The neutralization/SCWO facility at PBA would be a government-owned, contractor-operated facility. The operating and maintenance labor for neutralization/SCWO is expected to be similar to that for incineration (General Atomics 1999, PMACWA 1999a). This analysis assumed that the estimated operations workforce needs would be approximately 550 contractor employees for plant operations and 170 government employees for munitions handling, security, oversight, and other support activities (PMCD 1997).

TABLE 3.17 Transportation Data for Raw Materials for Neutralization/SCWO of ACW Containing Nerve Agent at PBA

Type of Data	Input Material No. 1	Input Material No. 2	Input Material No. 3	Input Material No. 4	Input Material No. 5
Transported materials					
Type/chemical	NaOH	LN ₂	LOX	H ₃ PO ₄	Kerosene
Physical form	Liquid	Liquid	Liquid	Liquid	Liquid
Chemical composition/ temperature, pressure	NaOH/ambient	N ₂ /-321°F, 1 atm	O ₂ /-297°F, 1 atm	H ₃ PO ₄ / ambient	Kerosene/ ambient
Packaging					
Type	55-gal drum	5,400-gal tanker truck	4,000-gal tanker truck	55-gal drum	5,500-gal tank truck
Container volume (ft ³)	7.35	721.87	534.72	7.35	735.24
Certified by	DOT	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies	Varies
Container weight (lb)	50	NA ^a	NA	50	NA
Material weight (lb) ^b	700	43,720	38,080	774	39,020
Chemical content (wt%)	50% NaOH	100% N ₂	100% O ₂	100% H ₃ PO ₄	NA
Shipments					
Average weight (tons/yr)	1,815	0	4,418	1185.8	829.0
Average volume (ft ³ /yr)	38,568	0	124,089	22,544	31,246
Packages/yr	5,246	0	233	3,067	43
Packages/shipment	48	1	1	48	1
Shipments/yr	110	0	233	64	43
Form of transport/routing					
Form of transportation	Truck	Truck	Truck	Truck	Truck

^a NA = not applicable.

^b Based on Mitretek (2001b).

3.3.2.3.4 Operations Emissions and Waste Estimates

Wastes from the neutralization/SCWO process would include air emissions and solid wastes. The only liquid effluent expected from the destruction facility would be sanitary waste, which would be managed in an on-site treatment unit. All liquids generated by the process and all liquid laboratory wastes would be reused in the process or disposed of internally by neutralization/SCWO. Destruction facility operations, including waste management, would comply with U.S. Army, federal, state, and local requirements. Any wastes that are identified as hazardous would be stored and disposed of in compliance with RCRA requirements. A summary of the types of emissions and solid wastes is provided below.

Atmospheric Emissions. The major process gaseous residuals expected from the neutralization/SCWO operation include the following:⁵⁹

- Ventilation gases from the ERHs, PRHs, and MPF;
- Ventilation gases from agent hydrolysis system; and
- Gases from the agent hydrolysate and energetics/dunnage hydrolysate SCWO systems.

These gases would be vented through scrubbers to the facility ventilation system where they would pass through carbon filters prior to release to the atmosphere. Handling and disposal of process residue in accordance with the provisions of RCRA are expected to result in little potential for significant adverse impacts on air quality. Emissions from vehicles and combustion of natural gas and LPG are regulated by the U.S. Environmental Protection Agency (EPA) and the State of Arkansas, and are expected to result in little potential for significant adverse impacts on air quality. Dust emissions also would be controlled during operations.

The neutralization/SCWO process would be required to meet RCRA requirements and will operate under permit. The process would be required to destroy agent to a DRE of 99.9999% and meet agent emission limits as established by the U.S. Army Surgeon General (ASG). Other emissions, including metals and HCl, would be regulated in accordance with the RCRA and any other required environmental permits. The operation would also be required to meet air pollution control requirements for conventional pollutants, such as CO, sulfur dioxide (SO₂), and opacity.

All ventilation air would be processed through carbon filtration units before being released to the atmosphere. Facility effluent release points would include gaseous releases to the environment. Table 3.18 summarizes the characterization of facility effluent air release points.

⁵⁹ Nitrogen gas from the cryofracture operation would not be applicable to PBA.

TABLE 3.18 Stack Parameters for Neutralization/SCWO at PBA^a

Installation or Emission Point	Physical Stack Height (ft)	Stack Exit Diameter (ft)	Stack Exit Gas Flow (acfm)	Stack Exit		Stack Location ^b
				Gas Velocity (ft/s)	Stack Exit Gas Temp (°F)	
Process steam boiler I ^{b,c}	70	2	13,520	71.73	325	Near southwest corner of PUB
Process steam boiler II ^{b,c}	70	2	13,520	71.73	325	Near southwest corner of PUB
Process steam boiler III ^{b,c}	70	2	13,520	71.73	325	Near southwest corner of PUB
Diesel generator exhaust I ^b	47	0.67	6,765	323.00	925	Near northwest corner of PMB
Diesel generator exhaust II ^b	47	0.67	6,765	323.00	925	Near northwest corner of PMB
Filter farm stack ^d	120	6	96,000	56.59	77	Center of structure
SCWO stack ^d	80	2.5	12,000	40.74	77	NA, center of structure assumed

^a Abbreviations: PMB = Personnel and Maintenance Building, PUB = Process Utilities Building, NA = not available.

^b Information on the stack characteristics for neutralization/SCWO was unavailable; characteristics similar to neutralization/biotreatment were assumed (Parson/Allied Signal 1999).

^c Stack exit gas flow for the process steam boiler was taken from Parsons/Allied Signal (1999) and modified to take into account the annual average natural gas consumption rate of 501,100 scf/d for neutralization/SCWO.

^d Stack characteristics similar to those at Newport, Indiana, were assumed (PMCD 1999a).

Table 3.19 summarizes the emission rates of criteria pollutants during operations, as estimated on the basis of the annual fuel consumption rates listed in Table 3.15 and normal neutralization/SCWO. Daily emissions can be estimated from the hourly rates, assuming 12 operating hours per day.

Small amounts of organic and metallic compounds would be emitted from combustion of natural gas and fuel oil during normal boiler operation and from the combustion of fuel oil during emergency diesel generator operation. Tables 3.20 and 3.21 summarize the emission rates of toxic air pollutants (TAPs) from the process steam boiler and from the emergency diesel generator, respectively.⁶⁰ These rates were estimated on the basis of the annual fuel consumption

⁶⁰ Many of the TAPs that would be emitted from the pilot-test facility would be hazardous air pollutants (HAPs) as defined in Section 112 of the CAA, Title III. The term TAP is broader in that it includes some pollutants that are not HAPs.

TABLE 3.19 Estimated Hourly and Annual Criteria Pollutant Emission Rates during Normal Neutralization/SCWO Operations at PBA

Criteria Pollutant	Process Steam Boiler Stack ^a		Diesel Generator Exhaust Stack ^b		SCWO Stack ^c	
	lb/h	tons/yr	lb/h	tons/yr	lb/h	tons/yr
CO	1.3	2.18	10.4	3.12	0	0
NO _x	2.2	3.64	48.4	14.50	0	0
SO ₂	0.01	0.02	3.2	0.95	0	0
PM ₁₀	0.12	0.20	3.4	1.02	0	0
HC	0.09	0.14	4.0	1.18	0	0
N ₂ O ^d	0.0	0.00	0.0	0.00	201	288
Hydrogen, H ₂ ^d	0.0	0.00	0.0	0.00	56	80

^a Estimated on the basis of the utility requirements listed in Table 3.15.

^b Based on 600 hours of operations per year.

^c Operation similar to neutralization/biotreatment was assumed.

^d Based on Tables 4.5-1 and 4.5-2 in General Atomics (1999).

rates shown in Table 3.15 and with Factor Information Retrieval (FIRE) 6.22 emission factors for large wall-fired boilers with greater than 100 MMBtu/h of heat input and for reciprocating diesel generators (EPA 2000a). Daily emissions can be estimated from the hourly rates, assuming 12 operating hours per day.

The volume percent of hydrogen in the air effluent from the SCWO stack during nerve agent processing is estimated to be approximately 9% (Mitretek 2001b), which is within the flammable range of 4 to 75% for hydrogen. A series of malfunctions could potentially cause an ignition source to be present and rupture the off-gas treatment system (i.e., a process-related upset). Exhaust systems must be designed to minimize this hazard.

The neutralization/SCWO facility at PBA would be equipped with building ventilation systems that would discharge, to the atmosphere, indoor air from the Munitions Demilitarization Building (MDB) process area, the Laboratory Building, and the Personnel and Maintenance Building through the filter farm stack. Of the three ventilation systems, only the indoor air from the MDB process area would be potentially exposed to chemical agents during operations.

To estimate the maximum potential emissions of chemical agents, only the MDB process area was considered to be a significant potential source. The filter systems would be designed to remove chemical agents from the ventilation air streams to levels below the allowable stack

TABLE 3.20 Estimated Hourly and Annual TAP Emission Rates during Normal Boiler Operations for Neutralization/SCWO at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
2-Methylnaphthalene	4.6E-06 ^b	1.2E-03
3-Methylchloranthrene	3.4E-07	9.4E-05
Acenaphthene	3.4E-07	9.4E-05
Acenaphthylene	3.4E-07	9.4E-05
Anthracene	4.6E-07	1.2E-04
Arsenic	3.8E-05	1.0E-02
Barium	8.4E-04	2.3E-01
Benz(a)anthracene	3.4E-07	9.4E-05
Benzene	4.0E-04	1.1E-01
Benzo(a)pyrene	2.3E-07	6.2E-05
Benzo(b)fluoranthene	3.4E-07	9.4E-05
Benzo(g,h,i)perylene	2.3E-07	6.2E-05
Benzo(k)fluoranthene	3.4E-07	9.4E-05
Beryllium	2.3E-06	6.2E-04
Butane	4.0E-01	1.1E+02
Cadmium	2.1E-04	5.7E-02
Chromium	2.7E-04	7.3E-02
Chrysene	3.4E-07	9.4E-05
Cobalt	1.6E-05	4.4E-03
Copper	1.6E-04	4.4E-02
Dibenzo(a,h)anthracene	2.3E-07	6.2E-05
Dichlorobenzene	2.3E-04	6.2E-02
Dimethylbenz(a)anthracene	3.0E-06	8.3E-04
Ethane	5.9E-01	1.6E+02
Fluoranthene	5.7E-07	1.6E-04
Fluorene	5.3E-07	1.5E-04
Formaldehyde	1.4E-02	3.9E+00
Hexane(n)	3.4E-01	9.4E+01
Indeno(1,2,3-cd)pyrene	3.4E-07	9.4E-05
Lead	9.5E-05	2.6E-02
Manganese	7.2E-05	2.0E-02
Mercury	4.9E-05	1.4E-02
Molybdenum	2.1E-04	5.7E-02
Naphthalene	1.2E-04	3.2E-02
Nickel	4.0E-04	1.1E-01
Pentane(n)	4.9E-01	1.4E+02
Phenanthrene	3.2E-06	8.8E-04
Propane	3.0E-01	8.3E+01
Pyrene	9.5E-07	2.6E-04
Selenium	4.6E-06	1.2E-03
Toluene	6.5E-04	1.8E-01
Vanadium	4.4E-04	1.2E-01

^a Emission factors from EPA (2000a).

^b This system of exponential notation is equivalent to $N \times 10^{-x}$. For example, $4.4E-03 = 4.4 \times 10^{-3}$.

TABLE 3.21 Estimated Hourly and Annual TAP Emission Rates during Emergency Diesel Generator Operations for Neutralization/SCWO at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
Acenaphthene	3.1E-07	1.9E-04
Acenaphthylene	1.1E-06	6.7E-04
Acetaldehyde	1.7E-04	1.0E-01
Acrolein	2.0E-05	1.2E-02
Aldehydes	1.5E-02	9.2E+00
Anthracene	4.1E-07	2.5E-04
Benzene	2.0E-04	1.2E-01
Benzo (a) anthracene	3.7E-07	2.2E-04
Benzo (a) pyrene	4.1E-08	2.5E-05
Benzo (b) fluoranthene	2.2E-08	1.3E-05
Benzo (g,h,i) perylene	1.1E-07	6.4E-05
Benzo (k) fluoranthene	3.4E-08	2.0E-05
1,3-Butadiene	8.6E-06	5.1E-03
Chrysene	7.8E-08	4.6E-05
Dibenzo(a,h) anthracene	1.3E-07	7.7E-05
Fluoranthene	1.7E-06	1.0E-03
Fluorene	6.4E-06	3.8E-03
Formaldehyde	2.6E-04	1.6E-01
Indeno(1,2,3-cd)pyrene	8.2E-08	4.9E-05
Isomers of xylene	6.3E-05	3.7E-02
Mercury	6.6E-08	4.0E-05
Naphthalene	1.9E-05	1.1E-02
Phenanthrene	6.5E-06	3.9E-03
Polycyclic aromatic hydrocarbons (PAHs)	3.7E-05	2.2E-02
Propylene	5.7E-04	3.4E-01
Pyrene	1.0E-06	6.3E-04

^a Emission factors from EPA (2000a).

concentrations that have been recommended by the U.S. Department of Health and Human Services, Centers for Disease Control (53 *Federal Register* 8504 – 8507, March 15, 1988). Also, a negative pressure would be maintained at all times in the MDB after initiation of hot operations to inhibit the release of chemical agents. Table 3.22 gives the potential chemical agent emission rates, assuming that the chemical agent concentrations in the air discharged from the filter farm stack would be 20% of the recommended allowable stack concentrations (i.e., the level of quantification of the ventilation exhaust chemical agent monitors). These emission calculations were based on operations time (12 hours per day, 276 days per year), since the only time there is a source of agent is during operations.

TABLE 3.22 Estimated Maximum Hourly and Annual Agent Emission Rates from the Filter Farm Stack for Neutralization/SCWO at PBA

Chemical Agent	Emission Factor (mg/m ³) ^a	Stack Exit Gas Flow (acfm) ^b	Hours of Operation per Year ^c	Stack Emission Rate	
				(lb/h)	(tons/yr) ^d
GB	0.00006	96,000	3,312	2.2E-05	3.6E-05
VX	0.00006	96,000	1,292	2.2E-05	1.4E-05

^a Based on the monitor level of quantification, which is 20% of the allowable stack concentration recommended for each chemical agent in Title 53, Parts 8504 – 8507, *Code of Federal Regulations* (53 CFR 8504 – 8507).

^b Filter farm stack exit flow based on building ventilation for the MDB.

^c Hours of operation based on the assumption that each pilot plant would operate at the design throughputs specified in CBDCOM (1997).

^d Estimate based on the number of hours of operation per year.

Table 3.23 gives the estimated TAP emission rates during operations at the SCWO stack for nerve agent processing. Annual emission rates can be estimated from the daily values, assuming that there are 276 operating days per year.

Emissions from operations worker commuter vehicles were estimated on the basis of the assumption that an average of 720 automobiles (one car per operations worker) would be added to the area of the site and that each worker would drive an average of 20 mi (32 km) to the site. Table 3.24 gives annual emission estimates due to the increased traffic.

Liquid Wastes. As indicated previously, brine liquids from the SCWO units would be sent to the BRA, where they would be dried to form brine salts. Other liquids, such as spent decontamination solutions and laboratory wastes, would be fed to the SCWO units. The only major liquid effluent expected to be generated at the facility is domestic sewage, which would be managed on-site. Small amounts of hazardous liquids could be generated from chemical makeup and reagents for support activities; the quantities are expected to be minor compared with those for domestic sewage (sanitary waste).

Solid Wastes. The major process solid residuals expected from the neutralization/SCWO operation include the following:

- Brine salts from treatment of the SCWO effluent,
- Decontaminated (5X condition) scrap metal from the HDCs and the inductively heated MPF, and

TABLE 3.23 Estimated TAP Emission Rates from the SCWO Stack during Neutralization/SCWO of ACW Containing Nerve Agent at PBA^a

Compound	Emission Rate (lb/d)	Compound	Emission Rate (lb/d)
Acetaldehyde	9.6E-11	Methyl ethyl ketone/butyraldehydes	2.5E-12
Antimony	7.8E-12	Naphthalene	8.0E-14
Arsenic	2.4E-12	Nickel	5.3E-10
Beryllium	4.7E-13	Particulates	9.1E-09
Cadmium	1.2E-11	Phosphorus	2.8E-09
Chromium	1.1E-10	Selenium	1.9E-11
Cobalt	1.5E-11		
Formaldehyde	1.2E-11		
Lead	1.2E-10		
Manganese	1.1E-10		
Mercury	9.6E-12		

^a Annual emissions can be estimated on the basis of the assumption that there are 276 days of operations per year.

TABLE 3.24 Estimated Emissions from Worker Commuter Vehicles for Neutralization/SCWO Operations at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Emission Rate (tons/yr)
HC	199,000	1.16	20	16.4
CO	199,000	11.38	20	160.5
NO _x	199,000	0.73	20	10.3
SO ₂	199,000	0.12	20	1.7
PM ₁₀	199,000	0.055	20	0.78

^a Number of auto round trips to the operation site estimated on the basis of the annual operating personpower and an assumption of 276 days of operation per year.

^b Emission factors determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

- Decontaminated (5X condition) salts removed from the energetics hydrolysates and thermally treated in the inductively heated MPF.

The effluent from the SCWO unit would be sent to an evaporator, which would produce a filter cake with about 70% solids. The water content would be bound as water of hydration; free-standing liquid is not expected (NCD 1998b). The filter cake would be transported to an approved off-site hazardous waste treatment, storage, and disposal facility for additional treatment and/or ultimate disposal. Table 3.25 provides information on the chemical composition of the brine salts (filter cake).

Nonhazardous scrap metal (5X condition) from the munition bodies would be sold to a scrap dealer or smelter for reuse if approved by the regulatory authority (see Table 3.26). However, if it proved necessary, these metals could be disposed of off-site in a nonhazardous waste landfill or in a RCRA-permitted hazardous waste landfill. Table 3.27 gives the amounts of other process wastes.

TABLE 3.25 Estimated Generation Rates of Brine Salts from Neutralization/SCWO at PBA To Be Sent Off-Site for Land Disposal

Generation Rate(lb/d)		Generation Rate (lb/d)	
Compound	Mustard	Compound	Mustard
2-Butanone	3.8E-04	Magnesium	1.6E+00
Acetaldehyde	7.7E-02	Mercury	2.3E-03
Acetone	1.7E-03	Methylene chloride	5.8E-04
Aldol condensate	5.8E-04	Molybdenum	2.7E+00
Aluminum	3.5E+01	Nickel	9.5E+01
Antimony	1.2E-01	Nitrate	5.2E+01
Arsenic	3.0E-01	Nitrite	8.9E+00
Bis(2-ethylhexyl)phthalate	3.1E-03	Phenol	1.9E-04
Bromomethane	7.5E-03	Potassium	4.6E-01
Cadmium	1.8E-02	Silane	2.9E-02
Calcium	1.7E+00	Siloxane	2.1E-02
Calcium silicate	7.4E+00	Silver	7.6E-02
Chloromethane	1.0E-02	Sodium chloride	9.6E-04
Chromium	2.1E+01	Sodium fluoride	5.8E+02
Cobalt	1.4E-01	Sodium phosphate	1.7E+04
Copper	5.6E+00	Sodium sulfate	3.1E+02
Cyclohexanone	2.5E-02	Sulfide, reactive	1.5E+00
Di-n-butylphthalate	7.2E-04	Thallium	2.1E-01
Fluoride	3.4E+02	Vanadium	4.0E-02
Formaldehyde	3.9E-02	Water in salt cake	2.7E+03
Iron	1.8E+01	Zinc	3.4E+00
Lead	2.4E+01	Total	2.1E+04

TABLE 3.26 Estimated Generation Rates of 5X Solids from Neutralization/SCWO at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)
Steel/iron	5.4E+03
Aluminum	8.3E+02
Glass fiber	8.8E+02
Total	7.1E+03

TABLE 3.27 Estimated Generation Rates of Other Solid Wastes from Neutralization/SCWO at PBA To Be Sent Off-Site for Land Disposal or Recycling

Other Wastes	Generation Rate (lb/d)
Metal from dunnage	3.5E+02
Al(OH) ₃	9.1E+03

Nonprocess waste streams would include decon solution, DPE suits, spent carbon, waste oils, trash, debris, and spent hydraulic fluid, which are assumed to be potentially contaminated with nerve agent and that would be processed in the dunnage/waste processing system. After this processing, the only streams with a significant solid residue would be the decon solution (containing NaOH and sodium hypochlorite [NaOCl]) and miscellaneous metal parts from equipment operation. Table 3.28 provides information on the daily and annual generation rates of treated nonprocess wastes for ACW contaminated with nerve agent.

Annual waste generation rates can be estimated from the daily values, assuming 276 days of operations per year for agent processing (since total campaign length of 484 days exceeds 276 days).

The above waste streams may be shipped from the on-site facility to off-site locations. Table 3.29 provides transportation data for annual shipment of these waste streams during nerve agent processing and for nonprocess solid wastes from neutralization/SCWO. It was assumed that all wastes would be packaged in 55-gal (208-L) drums prior to off-site shipment.

Table 3.30 lists the types and quantities of nonhazardous (nonprocess) solid and liquid wastes that could be generated from facility operation. Waste generation rates are based on historical data on building size, utility requirements, and facility workforce.

3.3.2.4 Activities

The PMACWA described activities for installation of the neutralization/SCWO system (PMACWA 1999a). The major phases of the project are shown in Table 3.31.

TABLE 3.28 Calculated Quantities of Solid Residues from Nonprocess Wastes from Neutralization/SCWO of ACW Containing Nerve Agent at PBA

Waste Type	Inlet Waste Composition	Treatment Process	Product	Daily Quantity (lb/d)	Annual Quantity (tons/yr)
Decon solution	18 wt% NaOH, NaOCl ^a	SCWO	Brine, 15% water	320	44
Miscellaneous metal parts	Nonmunition scrap metal	MPF	100% metal	100	14
Total	NA ^a	NA	NA	420	58

^a NA = not applicable.

Source: APG (1997).

3.3.2.5 Uncertainties

As indicated previously, each of the individual technologies that form the neutralization/SCWO system has either been proven to be a successful technology or has been demonstrated by PMACWA to be an acceptable technologies for application at PBA. However, demonstration testing focused on individual technologies and sometimes used less-than-full-scale units. In addition, although EDSs were conducted to evaluate the long-term adequacy of individual technologies, it was not possible to evaluate the long-term viability and performance of the entire, integrated treatment system. Thus, the primary uncertainty associated with neutralization/SCWO is that the entire, integrated treatment system, with all its component units, has not been assembled and tested. The pilot program, if implemented for this technology system, would be designed to evaluate overall operability and long-term performance.

3.3.3 NEUTRALIZATION/BIOTREATMENT

As indicated in Section 3.2.2.3, demonstration testing for neutralization/biotreatment was unsuccessful for nerve agents. Because PBA stores only ACW containing nerve agents, neutralization/biotreatment is not an applicable technology for PBA.

3.3.4 NEUTRALIZATION/GPCR/TW-SCWO

This description of the neutralization/GPCR /TW-SCWO technology system is based on several primary reports. A description of the proposed technology system can be found in the

TABLE 3.29 Transportation Data for Solid Wastes from Neutralization/SCWO of ACW Containing Nerve Agent at PBA

Type of Data	Output Material No. 1	Output Material No. 2	Output Material No. 3	Output Material No. 4
Transported Materials				
Type/chemical	Brine salts – waste	5X solids – waste	Other wastes	Nonprocess wastes
Physical form	Solid	Solid	Solid	Solid
Chemical composition/ temperature, pressure	See Table 3.24	See Table 3.25	See Table 3.26	See Table 3.27
Packaging				
Type	55-gal drum ^a	55-gal drum	55-gal drum	55-gal drum
Container volume (ft ³)	7.35	7.35	7.35	7.35
Certified by	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies
Container weight (lb)	50	50	50	50
Material weight (lb)	1,060	450	450	494
Chemical content (wt%)	See Table 3.24	See Table 3.25	See Table 3.26	See Table 3.27
Shipments				
Average weight (tons/yr) ^b	2,922	985	1,310	57
Average volume (ft ³ /yr)	58,310	32,750	43,560	1,712
Packages/yr	7,931	4,455	5,925	233
Packages/shipment	48	48	48	48
Shipments/yr	166	93	124	5
Form of transport/routing				
Form of transportation	Truck	Truck	Truck	Truck
Destination – facility type	Land disposal ^c	Land disposal ^c	Land disposal ^c	Land disposal ^c

^a Review of the disassembly process indicates that the dimensions of the solids would allow disposal in standard 55-gal drums. Further validation with the technology provider may be required.

^b Estimated on the basis of 276 operating days per year.

^c Depending on test results for hazardous constituents, off-site disposal at a RCRA-permitted facility may be required.

TABLE 3.30 Estimated Annual Nonhazardous (Nonprocess) Waste Generated during Neutralization/SCWO Operations at PBA

Category	Solid (yd ³)	Liquid (gal)
Nonhazardous (sanitary) wastes	NA ^a	4.6E+06
Nonhazardous (other) wastes ^b	1,800	NA
Recyclable wastes ^c	720	NA

^a NA = not applicable.

^b Nonhazardous (other) wastes include domestic trash and office waste.

^c Recyclable wastes include paper, aluminum, etc., generated by the facility.

technology's provider's demonstration report (Foster Wheeler/Eco Logic International/Kvaerner 2000). As indicated in that report, many of the estimates provided for facility design and operation refer comparatively to the U.S. Army baseline incineration process, which indicates, in general, that estimates are comparable to those associated with the baseline incineration process. Thus, another of the primary sources for this section of the TRD is the EIS for disposal of chemical agents and munitions stored at Pine Bluff Arsenal, Arkansas (PMCD 1997). That EIS is the most recent EIS that the U.S. Army has prepared for baseline incineration of chemical munitions (General Atomics 1999).

In addition to the above, mass balance estimates, air emission estimates, and solid waste estimates for application of the neutralization/GPCP/TW-SCWO technology at PBA have been developed (Mitretek 2001c). Air emissions and solid waste estimates for neutralization/ GPCP/TW-SCWO, as discussed below, are based on Mitretek inputs, along with appropriate assumptions on filtration systems, plant operations, and schedule.

Many of the figures and tables referred to in the facility description for this technology system contain estimates (e.g., emissions, resources consumed) associated with processing ACW with a specified agent; these estimates are given on an annual basis (e.g., tons/yr). In some cases, the estimates have been converted from other units (e.g., lb/d) by accounting for the number of days of operation required for processing a specific type of ACW. This time period is referred to as a campaign; a campaign is agent-specific. The values in many of the following figures and

TABLE 3.31 Activities for Neutralization/SCWO at PBA

Key Milestones
EIS start
EDS testing start
Final EIS/ROD
Final design (65% completion)
RCRA Part B issued
MDB construction start
MDB construction finish
Systemization start (pilot train)
Systemization start (all trains)
Operations start
Operations finish

Source: PMACWA (1999a).

tables are based on the number of days in the campaign required to process ACW containing a specific agent. It was assumed that there are 276 operating days in a year. If the campaign is less than or equal to 276 days, annual quantities equal total quantities. If the campaign is greater than 276 days, quantities in the figures and tables are for 276 days of processing. In the latter case, the estimates provided are less than total quantities. Daily (or other) quantities may be obtained by adjusting for the number of days in the campaign.

Figures 3.29 and 3.30 provide input/output material balances for the major streams for neutralization/GPCP/TW-SCWO of ACW containing GB and VX agent, respectively. The amounts of air, potable water, natural gas input, treated off-gas, ventilation air, wastewater, and boiler flue gas shown in each of these figures represent total annual amounts.

3.3.4.1 General Facility Description

The proposed neutralization/GPCR/TW-SCWO facility is designed to fit approximately into the general configuration and site area as the baseline incineration process, except that it requires slightly more space (25%) for the MDB. Munitions access and disassembly, base hydrolysis, GPCR, and SCWO operations have been substituted for incineration operations. The physical plant would consist of a two-story building constructed of noncombustible materials, with a concrete structural frame and a low-slope concrete roof.

The site layout for neutralization/GPCR/TW-SCWO is shown in Figures 3.31 through 3.33. Figure 3.31 shows the general facility layout, Figure 3.32 shows the layout of the first floor of the MDB, and Figure 3.33 shows the layout of the second floor of the MDB. Additional diagrams may be found in Foster Wheeler/Eco Logic/Kvaerner (2000). In addition, Foster Wheeler/Eco Logic/Kvaerner (2000) provides descriptions of the various units and operations that would be included in each section of the building, as shown in Figures 3.31 through 3.33.

3.3.4.2 Construction Phase

The schedule for destruction of the stockpile at PBA, although tentative, calls for construction of the selected alternative to begin following issuance of the EIS ROD and receipt of the RCRA permit and any other environmental permits, as necessary. It is anticipated that the construction schedule for the neutralization/GPCR/TW-SCWO facility would be similar to that for the baseline incineration facility. Construction would take approximately 29 months (PMACWA 2001b). However, the PMACWA is investigating means of shortening the construction period including a 2-month design and procurement verification period.

Construction of the destruction facility on the PBA installation would result in consumption of materials and resources, vehicle exhaust emissions, fugitive dust, noise,

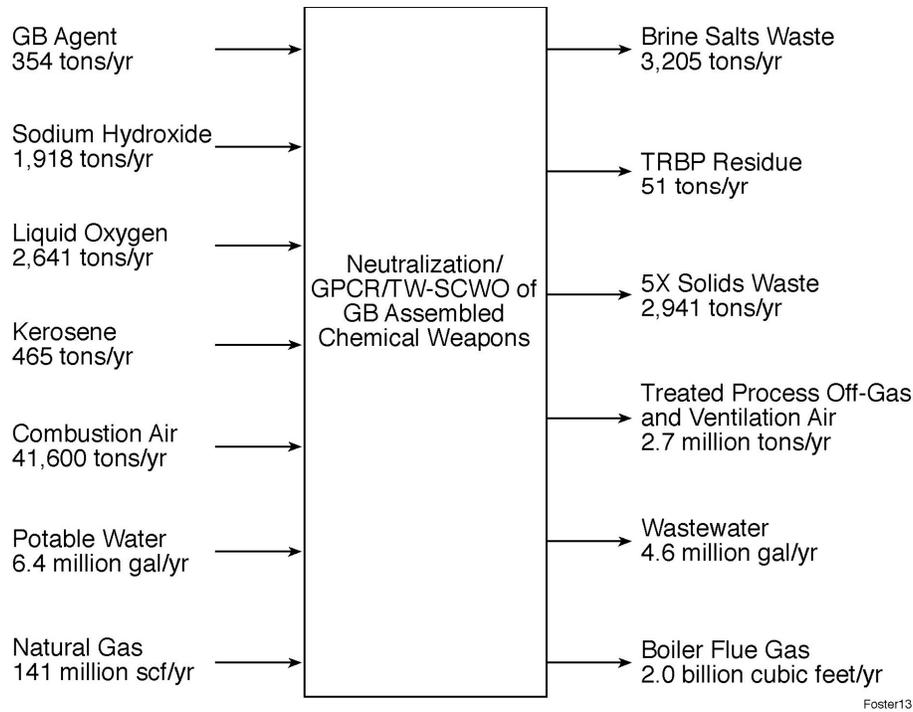


FIGURE 3.29 Input/Output Material Balance for Neutralization/GPCR/TW-SCWO of ACW Containing GB Agent at PBA

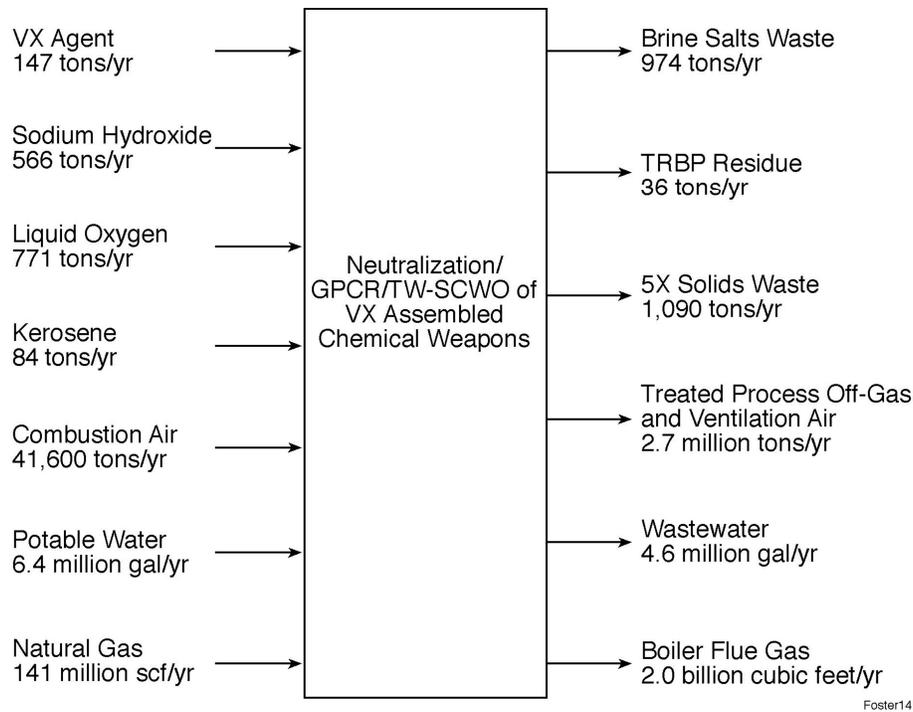
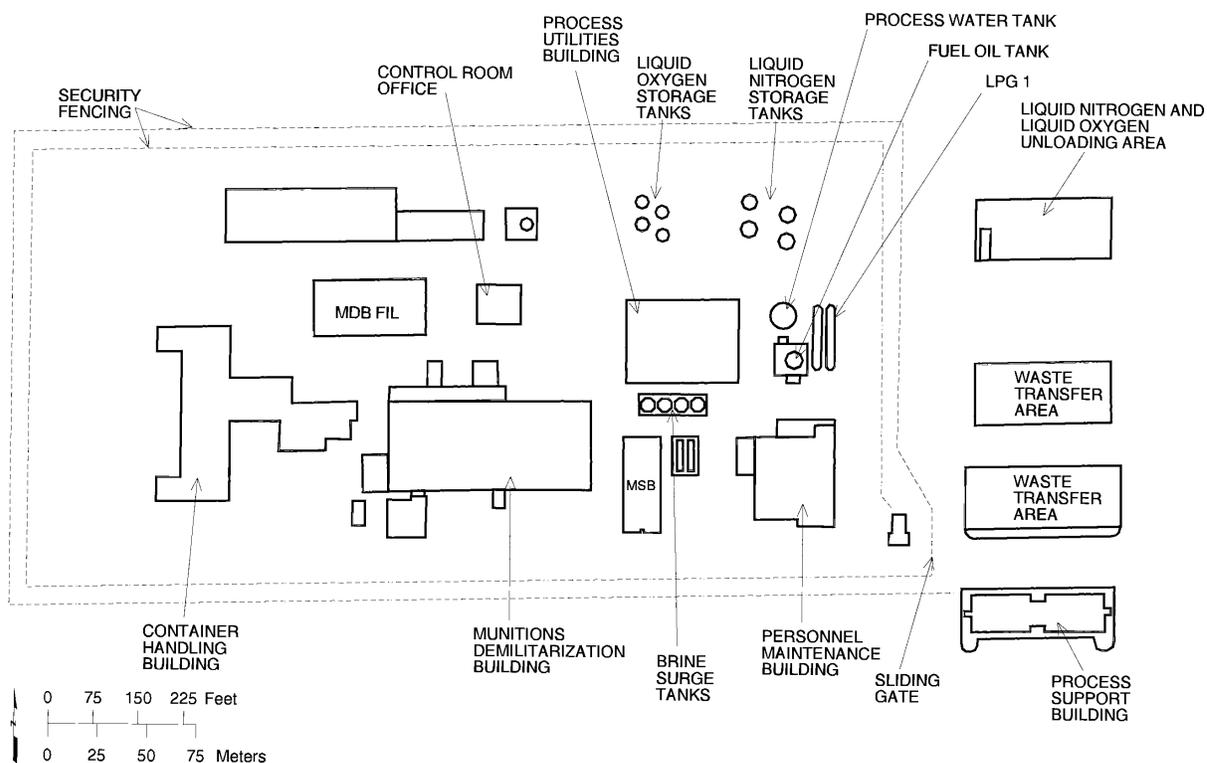


FIGURE 3.30 Input/Output Material Balance for Neutralization/GPCR/TW-SCWO of ACW Containing VX Agent at PBA



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FIGURE 3.31 Neutralization/GPCR/TW-SCWO Facility Layout at PBA (Source: Adapted from Foster Wheeler/Eco Logic/Kvaerner 2000)

destruction of wildlife habitat and native vegetation, increased employment, increased demand for public services, and occupational health hazards.

3.3.4.2.1 Construction Inputs and Resource Requirements

Resources and materials needed for constructing the disposal facility would include water, electricity, structural and piping steel, concrete, vehicle fuel, and industrial gases (propane). Table 3.32 contains order-of-magnitude estimates of the materials and resources that would be consumed during construction. These estimates are based on material and resource estimate methodologies used in engineering analyses and environmental documents concerning DOE waste management activities. For example, the estimates of 20 gal (76 L) of water for each construction FTE and solidification requiring 26 lb (12 kg) of water for each 100 lb (45 kg) of cement are from DOE (1997). More precise estimates would require a detailed consideration of construction activities.

Process equipment would use some materials that also would be used in construction, such as steel. However, the amount of such material used for process equipment is expected to be

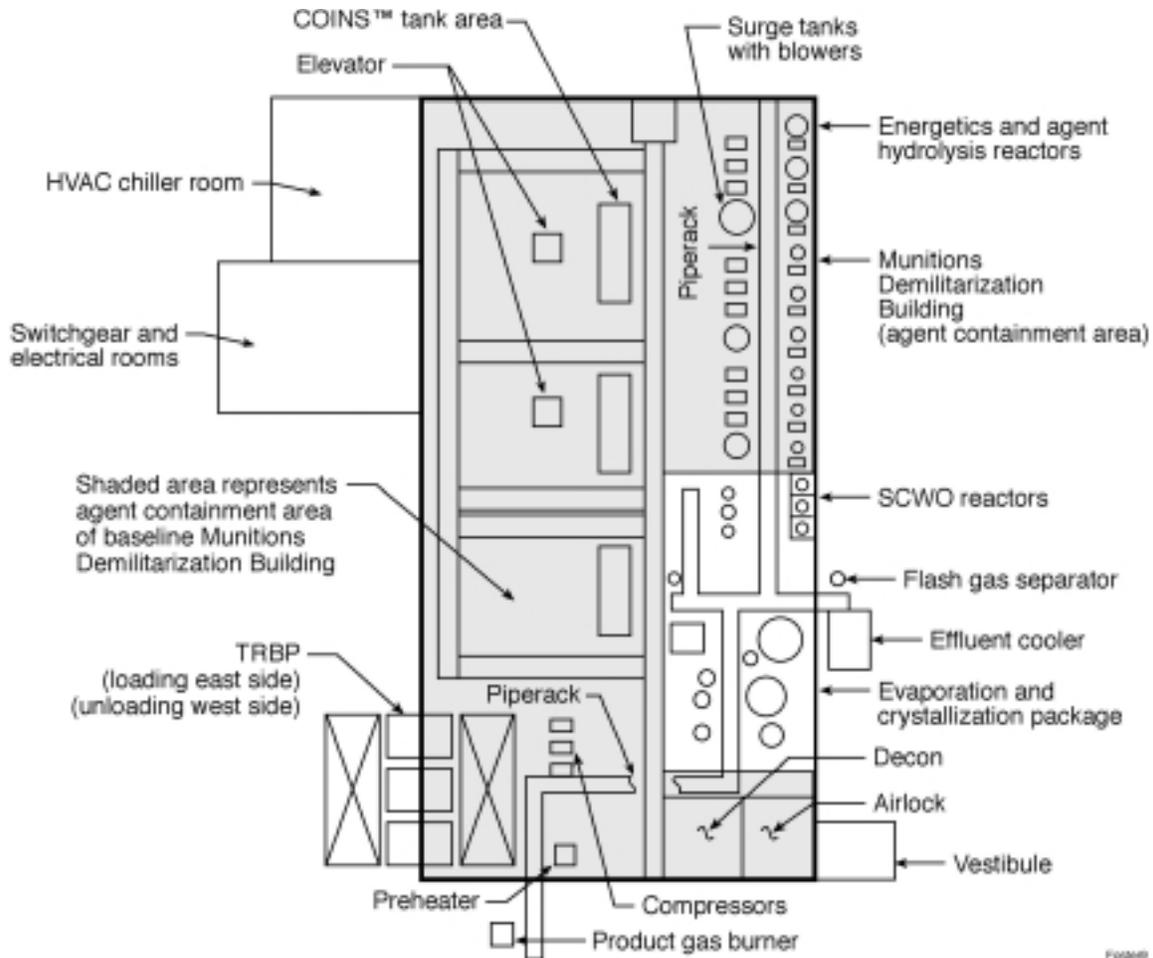


FIGURE 3.32 Layout of First Floor of Neutralization/GPCR/TW-SCWO Facility at PBA
(Source: Adapted from Foster Wheeler/Eco Logic/Kvaerner 2000)

small compared to that used in building construction, and, therefore, was not included in Table 3.32.

Order-of-magnitude estimates of the number of shipments of construction material to the site are given in Table 3.33. These estimates do not include shipments of process and related equipment, the number of which is expected to be small compared to the number of shipments of construction material. It was assumed that constituents of cement and backfill would be shipped in end-dump trucks with a capacity of 10 yd³ (8 m³), that steel would be shipped on trucks with a 21-ton (19-t) net payload, and that liquid fuel would be shipped in tank trucks with a nominal capacity of 9,000 gal (34,000 L).

Table 3.34 provides order-of-magnitude estimates of the emissions of criteria pollutants from construction delivery vehicles. It was assumed that the delivery vehicles would be heavy-duty diesel trucks and that the length of a one-way trip would be 20 mi (32 km). Actual trip

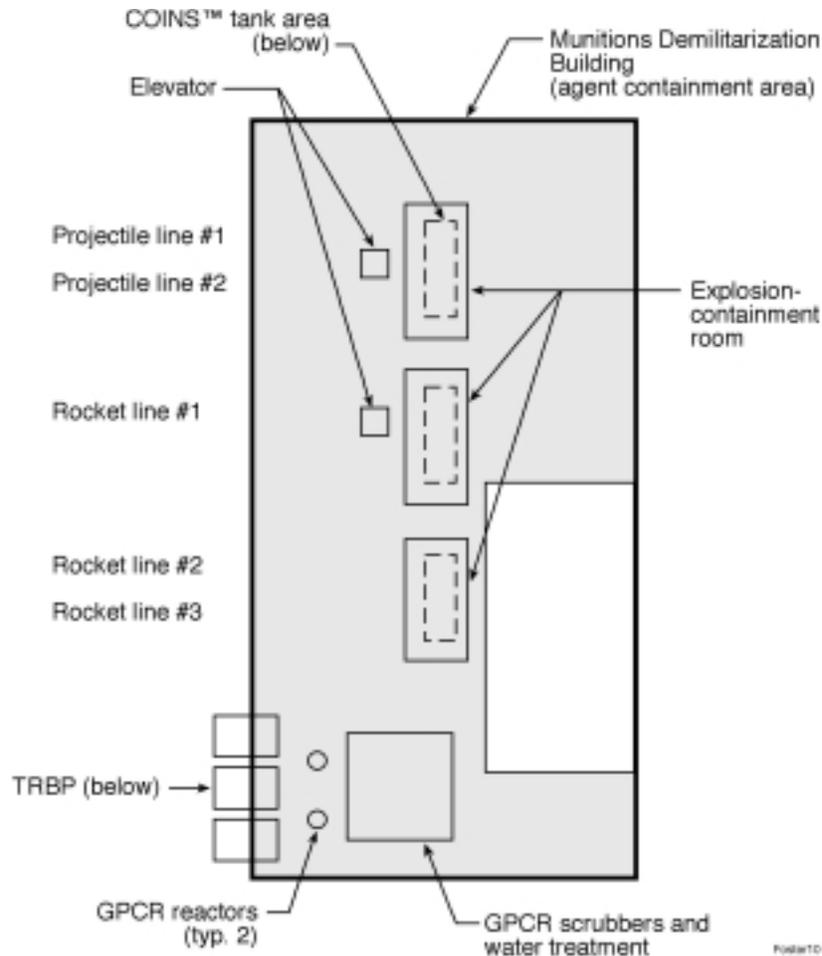


FIGURE 3.33 Layout of Second Floor of Neutralization/GPCR/TW-SCWO Facility at PBA (Source: Adapted from Foster Wheeler/Eco Logic/Kvaerner 2000)

distances would depend on a number of factors, including the availability of construction materials from local distributors and the distance of the site from the distributors.

3.3.4.2.2 Construction Workforce

The construction workforce is expected to increase steadily to a peak of about 1,040 FTEs near the midpoint of the 29-month construction period, and then to decrease steadily until construction is completed. The average number of construction workers per month is estimated to be approximately 518 FTEs. The total effort during construction is estimated to be approximately 1,250 FTE-years. These estimates were developed from an activity-based approach that considered the various types of buildings, required instrumentation, process equipment installation, and other related construction activities. Table 3.35 provides an estimate of the employment buildup by year.

TABLE 3.32 Estimated Materials/Resources Consumed during Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA^a

Construction Material/Resource	Total Consumption	Peak Demand
Utilities		
Water ^b	8,000,000 gal	NA ^c
Electricity	52,000 MWh	2.65 MW
Solids		
Concrete	32,400 yd ³	NA
Steel	5,800 tons	NA
Piping	96,000 linear ft	NA
Liquids		
Fuel ^d	2.4E+06 gal	NA
Gases		
Industrial gases (propane) ^d	6,500 gal	NA

^a All values can be considered order-of-magnitude approximations of the actual values; more accurate values would require a detailed consideration of construction activities.

^b The water requirement was estimated on the basis of DOE (1997), in which each FTE required 20 gal/d, and solidification required 26 lbs per 100 lb of cement.

^c NA = not applicable.

^d Scaling method based on Folga et al. (1999).

3.3.4.2.3 Construction Emissions and Waste Estimates

During the construction phase, fugitive emissions would consist mainly of dust and vehicle exhaust. Temporary, regional increases in atmospheric concentrations of CO, NO_x, hydrocarbons, particulate matter, and SO_x would result from the exhaust emissions of commuter vehicles, heavy construction vehicles, diesel generators, and other machinery and tools. Annual emissions of these pollutants would be small in comparison to de minimis levels used by regulators to determine whether an air quality permit or impact analysis is necessary. Emissions from construction vehicles are exempt from permit requirements. Nevertheless, vehicles and machinery would be equipped with standard pollution control devices to minimize air quality impacts.

Estimated emissions from construction activities (not including emissions from delivery vehicles) are shown in Table 3.36. The emissions shown are based on the anticipated construction land disturbance and vehicle traffic (for dust particulate pollutant) and fuel and gas

TABLE 3.33 Order-of-Magnitude Estimate of the Number of Truck Shipments of Materials for Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA^a

Resource	Total Consumption	Truck Capacity	No. Truck Shipments
Portland Cement ^b	3,564 yd ³	10 yd ³	357
Gravel ^b	13,284 yd ³	10 yd ³	1,329
Sand ^b	8,424 yd ³	10 yd ³	843
Steel ^c	5,800 tons	21 tons	280
Asphalt paving ^d	1,600 tons	20 tons	80
Backfill ^e	12,200 yd ³	10 yd ³	1,220
Fuel ^f	2.4E+06 gal	9,000 gal	270
Total			4,379
Total (rounded up)			5,000

^a The calculation did not include truck deliveries of process equipment and related items.

^b Assumes that concrete is composed of 11% portland cement, 41% gravel, and 26% sand, and is shipped to the site in a standard 10-yd³ end-dump truck.

^c Assumes that the net payload for steel transport to the site is 42,000 lb.

^d Assumes HMA is loaded into 20-ton-capacity triaxle trucks for transport to the paving site.

^e Assumes shipment is in standard 10-yd³ end-dump trucks and no fill is available on-site.

^f Assumes shipment is in DOT 406/MC-306 atmospheric pressure tank truck with a 9,000-gal capacity.

consumption. The column marked “Total” indicates the total amount of emissions that is estimated to occur over the entire construction period.

Emissions from construction worker commuter vehicles were estimated on the basis of the assumption that an average of about 518 automobiles (one car per construction worker) would be added to the area. As with construction delivery vehicles it was assumed that a one-way trip in a commuter vehicle would be 20 mi (32 km) in length. Table 3.37 gives the estimates of annual emissions of criteria pollutants arising from these trips.

Additional emissions would result from the use of paints and thinners, aerosols, and other area source emissions. These emissions are expected to be minor contributors to air pollution and were not included in current estimates.

TABLE 3.34 Estimated Emissions from Delivery Vehicles During Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Construction Period (yr)	Emission Rate (tons/yr)
HC	5,000	2.12	20	2.4	0.3
CO	5,000	11.28	20	2.4	1.7
NO _x	5,000	1.25	20	2.4	0.2
SO _x	5,000	0.23	20	2.4	0.03
PM ₁₀	5,000	0.617	20	2.4	0.1

^a Number of auto round trips to the construction site estimated on the basis of the total number of deliveries.

^b Emission factors determined using EPA computer modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and EPA PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

TABLE 3.35 Estimated Number of Employees Needed by Year for Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA

Employees	Year 1	Year 2	Year 3
Total craft workers	340	590	60
Construction management and support staff	90	150	20
Total	430	740	80

Construction would generate solid waste primarily in the form of excavation spoils and building material debris. These latter wastes would include concrete forms, equipment and hardware containers and packaging, paint cans, waste metal sheeting, pipe and wire, and landscaping debris. Small amounts of liquid wastes, such as solvents, cleaning solutions, and paint wastes also would be generated. Wastes would be collected and disposed of in compliance with U.S. Army, federal, state, and local requirements. All construction debris would be removed from the site for disposal. Any batteries, used motor oils, and empty containers would be separated from the waste streams and recycled. Any wastes that are identified as hazardous would be stored and disposed of in accordance

TABLE 3.36 Estimated Emissions during Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA

Criteria Pollutant	Total (tons)	Annual (tons/yr)
CO	122	50
HC	51	21
NO _x	181	75
SO _x	12	5
Particulates	450	186

TABLE 3.37 Estimated Emissions from Worker Commuter Vehicles During Construction of a Neutralization/ GPCR/TW-SCWO Facility at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Emission Rate (tons/yr)
HC	124,000	1.16	20	10.2
CO	124,000	11.38	20	100.5
NO _x	124,000	0.73	20	6.4
SO _x	124,000	0.12	20	1.1
PM ₁₀	124,000	0.055	20	0.5

^a Number of auto round trips to the construction site estimated on the basis of the total construction workforce and an assumption of 240 workdays per year.

^b Emission factors determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

with RCRA requirements. Sanitary wastes are the only significant liquid effluent that would be generated during construction and would be managed on-site.

The estimated total quantities of solid and liquid wastes generated from activities associated with facility construction are shown in Table 3.38. The waste generation quantities are based on historic data, land area size, and construction labor force.

3.3.4.3 Operations Phase

Information on the facility operations phase is presented in this section. Pre-operational testing is discussed first, followed by facility inputs and resource requirements, workforce requirements, and emissions and waste estimates.

3.3.4.3.1 Preoperational Testing

Following facility construction, a preoperational testing period assumed to last 14 months would begin (PMACWA 2001b). Often referred to as systemization, this period includes preoperational checkout, training, and integrated systems operation under mock conditions with simulated munitions filled with surrogate chemicals (PMCD 1997). Systemization would be used

to ensure that systems are operating as designed prior to pilot-scale operations. Therefore, it would appear that no hazardous emissions or effluents would be generated. The only types of effluents that would be generated would be criteria pollutants (during testing of the steam boilers and the emergency diesel generator) and sanitary waste (from the systemization workforce). The amounts of criteria pollutants released sanitary wastes generated would be negligible compared with the amount released or generated during construction and operations; thus they were not considered in this analysis. It is projected that 300 contractor FTE-years would be needed for systemization.

3.3.4.3.2 Operations Inputs and Resource Requirements

At full-scale operation, destruction of the nerve agent inventory at PBA is projected to require 484 days for processing (376 for GB and 108 for VX). Destruction operations at PBA are projected to require approximately 20.9 months at full-scale operation (see Table 3.39). This duration is based on a 12-hours-per-day, 6-days-per-week operation, 4 weeks per month, with one 3-week munitions changeover period. For comparison, incineration of the entire chemical agent inventory at PBA is projected to require 40 months (PMCD 1999b). Because baseline incineration at PBA would include destruction of mustard agent in TCs (which are not considered ACW), this option would require a longer period of operation.

Estimated annual utility consumption for facility operation, including electricity, fuel, and potable water usage, is presented in Table 3.40. The estimates in Table 3.40 are based on the assumption that the facility would consume potable water and produce sanitary waste 365 days per year. These are conservative assumptions that would identify an upper bound to potable water and sanitary waste treatment requirements. It was also assumed conservatively that fuel oil would be consumed only by an emergency diesel generator that would operate 600-hours per year. This analysis assumed that the amount of natural gas consumed for space heating would be negligible compared with the amount of natural gas consumed in the destruction process.

TABLE 3.38 Estimated Total Wastes Generated during Construction of a Neutralization/GPCR/TW-SCWO Facility at PBA

Waste Category	Quantity
Hazardous solids	90 yd ³
Hazardous liquids	35,000 gal
Nonhazardous solids	
Concrete ^a	210 yd ³
Steel ^b	29 tons
Other ^c	1,700 yd ³
Nonhazardous liquids	
Sanitary ^d	5,100,000 gal
Other	2,300,000 gal

^a Amount of concrete (nonhazardous solid) waste was estimated by assuming that 0.65% of concrete usage is spoilage.

^b Amount of steel waste stream estimated as 0.5% of steel requirement based on LLNL et al. (1997).

^c Amount of other stream estimated as eight times the concrete stream based on LLNL et al. (1997).

^d Amount of sanitary waste was estimated on the basis of the total construction workforce.

TABLE 3.39 Inventory and Estimated Processing Time for Neutralization/GPCR/TW-SCWO of the ACW Stored at PBA

Munition	Quantity	Agent	Processing Rate (no. of munitions/h)	Processing Time		Changeover (weeks)	Total (weeks)
				Hours	Weeks ^a		
M55 rocket	90,231	GB	20	4,512	62.7	0	62.7
M55 rocket	19,582	VX	20	979	13.6	3.0	16.6
M23 land mine	9,378	VX	30	313	4.3	0.0	4.3
Total	119,191			5,803	80.6	3.0	83.6

^a Estimated by assuming 6-days-per-week operations and 12 hours per day.

Destruction processes would consume raw materials. Table 3.41 gives the amounts of LOX, NaOH, and kerosene that would be consumed during the processing of the two agents.

Tables 3.42 and 3.43 present transportation data estimated using the input material streams from Mitretek (20001c) for LOX, NaOH, and kerosene for GB and VX agent processing, respectively. Each of these materials would be transported to the site as a liquid by truck. The NaOH would be transported in 55-gal (208-L) drums. The other two materials would be transported in bulk by tanker truck.

3.3.4.3.3 Operations Workforce

The neutralization/GPCR/TW-SCWO facility would be a government-owned, contractor-operated facility. Contractor employees would handle plant operations while government employees would handle munitions, provide security, and staff other support activities. It is estimated that 720 FTEs (550 FTEs of contractor employee effort and 170 FTEs of government employee effort) would be needed (PMCD 1997).

3.3.4.3.4 Operations Emissions and Waste Estimates

Wastes from the neutralization/GPCR/TW-SCWO process would include air emissions and solid wastes. The only liquid effluent from the facility would be sanitary waste, which would be managed in an on-site treatment unit. All liquids generated by the process and all liquid laboratory wastes would be reused in the process or destroyed internally by the neutralization/GPCR/TW-SCWO process. Destruction facility operations, including waste management, would comply with U.S. Army, federal, state, and local requirements. Any wastes that are identified as hazardous (e.g., SCWO salts and GPCR residues) would be stored and disposed of in compliance with RCRA requirements.

TABLE 3.40 Estimated Utilities Consumed during Destruction of ACW at the Neutralization/GPCR/TW-SCWO Facility at PBA

Utility	Average Daily Consumption	Peak-Day Consumption	Annual Consumption
Process water ^a	63,700 gal/d	3,600 gal/h	18,000,000 gal/yr
Potable water ^b	17,500 gal/d	180 gal/min	6,400,000 gal/yr ^c
Fire water ^b	NA ^d	3,000 gal/min	NA
Sanitary sewer ^b	20,650 gal/d	395 gal/min	7,500,000 gal/yr ^c
Natural gas ^a	510,000 scf/d	591,000 scf/d	141,000,000 scf/yr ^e
Fuel oil	962 gal/d	406 gal/h	48,000 gal/yr ^f
Electricity	72 MWh	3.5 MW	26.3 GWh ^{c,g}

^a Estimated on the basis of the ratio of munitions processing rate at PBA to that at BGAD and PCD.

^b Assumed to be similar to incineration because the number of operations and maintenance personnel and land area are unchanged from incineration.

^c Based on 365 days of operations per year.

^d NA = not applicable.

^e Based on 276 days of operations per year.

^f Based on 600 hours of emergency diesel generator operation per year.

^g Based on an average power rating of 80%.

Source: Carnes (2001).

TABLE 3.41 Estimated Raw Materials Consumed Annually during Normal Neutralization/GPCR/TW-SCWO Operations at PBA

Agent Processed	Material	Material Consumed	
		Average Daily (lb/d)	Annual ^a (tons/yr)
GB agent nominal 376-day campaign	LOX	19,000	2,600
	NaOH	13,900	1,900
VX nominal 108-day campaign	Kerosene for SCWO	3,400	460
	LOX	14,000	770
	NaOH	10,500	570
	Kerosene for SCWO	1,600	85

^a Annual estimates based on 276 days for GB processing and 108 days for VX processing.

Source: Mitretek (2001c).

TABLE 3.42 Transportation Data for Raw Materials for Neutralization/GPCR/TW-SCWO of ACW Containing GB Agent at PBA

Type of Data	Input Material No. 1	Input Material No. 2	Input Material No. 3
Transported materials			
Type/chemical	NaOH	LOX	Kerosene
Physical form	Liquid	Liquid	Liquid
Chemical composition/ temperature, pressure	NaOH/ambient	O ₂ /-297°F, 1 atm	Kerosene/ ambient
Packaging			
Type	55-gal drum	4,000-gal tanker truck	5,500-gal tank truck
Container volume (ft ³)	7.35	535	735
Certified by	DOT	DOT	DOT
Identifier	Varies	Varies	Varies
Container weight (lb)	50	NA ^a	NA
Material weight (lb) ^b	700	38,080	39,020
Chemical content (wt%)	50% NaOH	100% O ₂	NA
Shipments			
Average weight (tons/yr) ^c	1,918	2,641	465
Average volume (ft ³ /yr)	40,759	74,173	17,513
Packages/yr	5,544	139	24
Packages/shipment	48	1	1
Shipments/yr	116	139	24
Form of transport/routing			
Form of transportation	Truck	Truck	Truck
Specific gravity (77°F)	NA	1.14	0.85

^a NA = not applicable.

^b Based on Mitretek (2001c).

^c Estimated on the basis of 276 days of operations per year.

**TABLE 3.43 Transportation Data for Raw Materials for Neutralization/GPCR/
TW-SCWO of ACW Containing VX Agent at PBA**

Type of Data	Input Material No. 1	Input Material No. 2	Input Material No. 3
Transported materials			
Type/chemical	NaOH	LOX	Kerosene
Physical form	Liquid	Liquid	Liquid
Chemical composition/ temperature, pressure	NaOH/ ambient	O ₂ /-297°F, 1 atm	Kerosene/ ambient
Packaging			
Type	55-gal drum	4,000-gal tanker truck	5,500-gal tank truck
Container volume (ft ³)	7.35	535	735
Certified by	DOT	DOT	DOT
Identifier	Varies	Varies	Varies
Container weight (lb)	50	NA ^a	NA
Material weight (lb) ^b	700	38,080	39,020
Chemical content (wt%)	50% NaOH	100% O ₂	NA
Shipments			
Average weight (tons)/yr ^c	566	771	84
Average volume (ft ³)/yr	12,024	21,647	3,171
Packages/yr	1,636	41	5
Packages/shipment	48	1	1
Shipments/yr	35	41	5
Form of transport/routing			
Form of transportation	Truck	Truck	Truck
Specific gravity (77°F)	NA	1.14	0.85

^a NA = not applicable.

^b Based on Mitretek (2001c).

^c Estimated on the basis of a total campaign length of 108 days.

The only solid effluents from the process would include salts from TW-SCWO and solid residues from GPCR. Solid residues from GPCR collected during the PMACWA Demo II Test Program, passed the TCLP requirements, with the exception of DPE runs (Foster Wheeler/Eco Logic/Kvaerner 2000).

Gas Effluents. GPCR gas (including COINS and hydrolysate reactors gas streams) containing hydrogen, CH₄, CO₂, and acid gases would be scrubbed with caustic and then held for agent testing. Once cleared, the gas would be passed through a boiler or energy recovery device and then a catalytic converter. The gas product from GPCR would be a RCRA hazardous waste, but may be burned in a BIF if it meets certain requirements. The final technical evaluation for this technology (PMACWA 2001b) states that it appears likely that the GPCR product would exceed the specific heating value threshold (5,000 Btu/h) that is used as a key test to determine the applicability of the BIF exemption.

Product gases would be scrubbed before release to the plant ventilation system. These product gases would be stored and tested prior to release to the atmosphere. Thus if their concentrations leaving the scrubbers are not acceptable, they would reenter the GPCR process. Consequently, it was assumed that emissions from the product gas burner vent would not be further treated after release from the scrubbers. Facility effluent release points would include gaseous releases to the environment. Table 3.44 summarizes the facility effluent air release points.

Handling and disposal of process residue in accordance with the provisions of RCRA are expected to result in little potential for significant adverse impacts on air quality. Emissions from vehicle and combustion of natural gas and LPG are regulated by the EPA and the State of Arkansas and are expected to result in little potential for significant adverse impacts on air quality. Dust emissions would be controlled during operations as well.

The neutralization/GPCR/TW-SCWO process would be required to meet RCRA and any other applicable environmental requirements and would operate under permit. Permit conditions are expected to require the process to destroy agent and energetics to a DRE of 99.9999% and to meet agent emission limits as established by the ASG. Other emissions, including metals and HCl, would be regulated in accordance with the RCRA permit. The operation would also be required to meet air pollution control requirements for conventional pollutants, such as CO, SO₂, and opacity.

Table 3.45 summarizes the estimated criteria pollutant emission rates during operations; these rates were estimated on the basis of the annual fuel consumption rates shown in Table 3.40. Daily emissions can be estimated from the hourly rates, assuming 12 hours of operation per day.

Small amounts of organic and metallic compounds would be emitted from the combustion of natural gas during normal boiler operation and from the combustion of fuel oil

TABLE 3.44 Stack Parameters for Neutralization/GPCR/TW-SCWO at PBA^a

Installation or Emission Point	Physical Stack Height (ft)	Stack Exit Diameter (ft)	Stack Exit Gas Flow (acfm)	Stack Exit Gas Velocity (ft/s)	Stack Exit Gas Temp (°F)	Stack Location ^b
Process steam boiler I ^{b,c}	70	1.1	3,353	60	325	Near southwest corner of PUB
Process steam boiler II ^{b,c}	70	1.1	3,353	60	325	Near southwest corner of PUB
Process steam boiler III ^{b,c}	70	1.1	3,353	60	325	Near southwest corner of PUB
Diesel generator exhaust I ^b	47	0.67	6,765	323	925	Near northwest corner of PMB
Diesel generator exhaust II ^b	47	0.67	6,765	323	925	Near northwest corner of PMB
Filter farm stack ^{d,e}	120	6.8	131,000	60	77	Center of structure
Product gas burner stack ^{d,e}	80	0.417	520	64.56	77	Southwest corner of the MDB

^a Abbreviations: MDB = Munitions Demilitarization Building, PMB = Personnel and Maintenance Building, and PUB = Process Utilities Building.

^b Information on the stack characteristics for neutralization/GPCR/TW-SCWO was unavailable; characteristics similar to neutralization/biotreatment were assumed (Parsons/Allied Signal 1999).

^c Stack characteristics similar to those at Newport, Indiana, were assumed (PMCD 1999a).

^d Stack exit gas flow for the process steam boiler taken from Parsons/Allied Signal (1999) and modified to take into account the annual average natural gas consumption rate of 510,000 scf/d for neutralization/GPCR/TW-SCWO.

^e Stack exit gas flow and diameter revised to account for a 25% increase in the MDB proposed by the technology provider (Foster Wheeler/Eco Logic/Kvaerner (2000)).

during emergency diesel generator operation. Tables 3.46 and 3.47 summarize the TAP emission rates for the burning of natural gas in the boiler and fuel oil in the emergency generator, respectively. Many of these emissions are also HAPs, as defined in Section 112 of the CAA, Title III. These TAP emission rates were estimated on the basis of the annual fuel consumption rates shown in Table 3.40 and with FIRE 6.22 emission factors for large wall-fired boilers with greater than 1000 MMBtu/h of heat input and for reciprocating diesel engines (EPA 2000a). Daily emissions can be estimated from hourly rates, assuming 12 hours of operation per day.

The neutralization/GPCR/TW-SCWO facility at PBA would be equipped with building ventilation systems that would discharge, to the atmosphere, indoor air from the MDB process area, the Laboratory Building, and the Personnel and Maintenance Building through the filter farm stack. Of these three discharges, only the indoor air from the MDB process area would be potentially exposed to chemical agents during operations.

TABLE 3.45 Estimated Hourly and Annual Emission Rates of Criteria Pollutants during Normal Operations of a Neutralization/GPCR/TW-SCWO Facility at PBA

Criteria Pollutant	Process Steam Boiler Stack ^a		Diesel Generator Exhaust Stack ^b		Product Gas Burner Stack ^c	
	lb/h	tons/yr	lb/h	tons/yr	lb/h	tons/yr
CO	2.5	4.20	10.4	3.12	1.6E-01	2.7E-01
NO _x	4.2	6.99	48.4	14.50	1.0E-01	1.7E-01
SO _x	<0.02	0.03	3.2	0.95	4.0E-03	6.6E-03
PM ₁₀	0.2	0.38	3.4	1.02	2.8E-02	4.6E-02
HC	0.2	0.27	4.0	1.18	4.8E-02	8.0E-02

^a Estimated on the basis of the utility requirements listed in Table 3.39.

^b Based on 600 hours of operations per year.

^c Estimate based on H₂ generation rate from steam reforming of natural gas.

To estimate the maximum potential emissions of chemical agents, only the MDB process area is considered to be a significant potential source. The filter systems would be designed to remove chemical agents from the ventilation air streams to levels below the allowable stack concentrations that have been recommended by the U.S. Department of Health and Human Services, Centers for Disease Control (53 *Federal Register* 8504 – 8507, March 15, 1988). Also, a negative pressure would be maintained at all times in the MDB after initiation of hot operations to inhibit the release of chemical agents. Table 3.48 gives the potential chemical agent emission rates, assuming that the chemical agent concentrations in the air discharged would be at 20% of the recommended allowable stack concentrations (i.e., the level of quantification of the ventilation exhaust chemical agent monitors.) These emission calculations were based on actual operations time (12 hours per day, 276 days per year), since the only time there is a source of agent is during operations.

The estimated TAP emission rates (lb/h) during operation from the filter farm stack are provided in Tables 3.49 and 3.50 for GB and VX agent processing, respectively. Daily emission rates can be obtained by multiplying the hourly rates by 12. Annual emission rates can be estimated from the daily rates for GB and VX processing by assuming 276 and 108 days of operation, respectively. Tables 3.51 and 3.52 give the corresponding estimated TAP emission rates from the process gas burner stack for GB and VX agent, respectively.

TABLE 3.46 Estimated Hourly and Annual TAP Emission Rates during Normal Boiler Operations for Neutralization/GPCR/TW-SCWO at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
2-Methylnaphthalene	7.2E-07	2.4E-03
3-Methylchloranthrene	5.4E-08	1.8E-04
Acenaphthene	5.4E-08	1.8E-04
Acenaphthylene	5.4E-08	1.8E-04
Anthracene	7.2E-08	2.4E-04
Arsenic	6.0E-06	2.0E-02
Barium	1.3E-04	4.4E-01
Benz(a)anthracene	5.4E-08	1.8E-04
Benzene	6.3E-05	2.1E-01
Benzo(a)pyrene	3.6E-08	1.2E-04
Benzo(b)fluoranthene	5.4E-08	1.8E-04
Benzo(g,h,i)perylene	3.6E-08	1.2E-04
Benzo(k)fluoranthene	5.4E-08	1.8E-04
Beryllium	3.6E-07	1.2E-03
Butane	6.3E-02	2.1E+02
Cadmium	3.3E-05	1.1E-01
Chromium	4.2E-05	1.4E-01
Chrysene	5.4E-08	1.8E-04
Cobalt	2.5E-06	8.4E-03
Copper	2.6E-05	8.5E-02
Dibenzo(a,h)anthracene	3.6E-08	1.2E-04
Dichlorobenzene	3.6E-05	1.2E-01
Dimethylbenz(a)anthracene	4.8E-07	1.6E-03
Ethane	9.4E-02	3.1E+02
Fluoranthene	9.1E-08	3.0E-04
Fluorene	8.4E-08	2.8E-04
Formaldehyde	2.3E-03	7.5E+00
Hexane(n)	5.4E-02	1.8E+02
Indeno(1,2,3-cd)pyrene	5.4E-08	1.8E-04
Lead	1.5E-05	5.0E-02
Manganese	1.1E-05	3.8E-02
Mercury	7.8E-06	2.6E-02
Molybdenum	3.3E-05	1.1E-01
Naphthalene	1.8E-05	6.1E-02
Nickel	6.3E-05	2.1E-01
Pentane(n)	7.8E-02	2.6E+02
Phenanthrene	5.1E-07	1.7E-03
Propane	4.8E-02	1.6E+02
Pyrene	1.5E-07	5.0E-04
Selenium	7.2E-07	2.4E-03
Toluene	1.0E-04	3.4E-01
Vanadium	6.9E-05	2.3E-01
Total	5.7E-02	1.9E+02

^a Emission factors from EPA (2000a).

TABLE 3.47 Estimated Hourly and Annual TAP Emission Rates during Emergency Diesel Generator Operations for Neutralization/GPCR/TW-SCWO at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
Acenaphthene	3.1E-07	1.9E-04
Acenaphthylene	1.1E-06	6.7E-04
Acetaldehyde	1.7E-04	1.0E-01
Acrolein	2.0E-05	1.2E-02
Aldehydes	1.5E-02	9.2E+00
Anthracene	4.1E-07	2.5E-04
Benzene	2.0E-04	1.2E-01
Benzo (a) anthracene	3.7E-07	2.2E-04
Benzo (a) pyrene	4.1E-08	2.5E-05
Benzo (b) fluoranthene	2.2E-08	1.3E-05
Benzo (g,h,i) perylene	1.1E-07	6.4E-05
Benzo (k) fluoranthene	3.4E-08	2.0E-05
1,3-Butadiene	8.6E-06	5.1E-03
Chrysene	7.8E-08	4.6E-05
Dibenzo(a,h) anthracene	1.3E-07	7.7E-05
Fluoranthene	1.7E-06	1.0E-03
Fluorene	6.4E-06	3.8E-03
Formaldehyde	2.6E-04	1.6E-01
Indeno(1,2,3-cd)pyrene	8.2E-08	4.9E-05
Isomers of xylene	6.3E-05	3.7E-02
Mercury	6.6E-08	4.0E-05
Naphthalene	1.9E-05	1.1E-02
Phenanthrene	6.5E-06	3.9E-03
Polycyclic aromatic hydrocarbons (PAHs)	3.7E-05	2.2E-02
Propylene	5.7E-04	3.4E-01
Pyrene	1.0E-06	6.3E-04
Toluene	9.0E-05	5.4E-02

^a Emission factors from EPA (2000a).

Emissions from operations worker commuter vehicles were estimated on the basis of the assumption that each of the operations workers (720) would drive a round trip consisting of two 20-mi (32-km) one-way trips per day. Table 3.53 gives the annual emission estimates due to increased traffic.

Liquid Wastes. Through evaporation, crystallization, and filtration, brine salts would be formed from brine liquids from the TW-SCWO units. Remaining liquids would be recycled. The only major liquid effluent that is expected to be generated at the destruction facility is domestic sewage. Small amounts of hazardous liquids could be generated from chemical makeup and reagents for support activities; the quantities are expected to be minor compared with those for domestic sewage (sanitary waste). Sanitary waste would be managed on-site.

TABLE 3.48 Estimated Maximum Hourly and Annual Agent Emission Rates from the Filter Farm Stack for Neutralization/GPCR/TW-SCWO at PBA

Chemical Agent	Emission Factor (mg/m ³) ^a	Stack Exit Gas Flow (acfm) ^b	Hours of Operation per Year ^c	Stack Emission Rate	
				(lb/h)	(tons/yr) ^d
GB	0.00006	131,000	3,312	2.9E-05	4.9E-05
VX	0.00006	131,000	1,292	2.9E-05	1.9E-05

^a Based on the monitor level of quantification, which is 20% of the allowable stack concentration recommended for each chemical agent in 53 CFR 8504 – 8507.

^b Filter farm stack exit flow based on the estimated building ventilation for the MDB.

^c Hours of operations based on the assumption that each pilot plant operates at the design throughputs specified in CBDCOM (1997).

^d Estimate based on the number of hours of operation per year.

Solid Wastes. The major process solid residuals expected from the neutralization/GPCR/TW-SCWO operation include the following:

- Scrap metal and other solid residues decontaminated to a 5X condition in the GPCR, a thermal system that uses hydrogen in a steam atmosphere to reduce organics into CH₄, CO₂, CO, and acid gases;
- Brine salts from treatment of the SCWO effluent; and
- TRBP residues

The brine salts (filter cake) would be transported to an approved off-site hazardous waste treatment, storage, and disposal facility for additional treatment and/or ultimate disposal. Table 3.54 shows the composition of the filter cake and the rate of generation per processing day for processing of ACW containing GB and VX agent. Tables 3.55 and 3.56 show the corresponding information for the processing of TRBP residues and 5X scrap metal.

These waste streams would be shipped from the on-site facility to off-site locations. Tables 3.57 and 3.58 provide transportation data for annual shipment of these waste streams for GB and VX agent processing on the basis of 276 days of operations for ACW containing GB agent and a campaign length of 108 days for ACW containing VX agent.

TABLE 3.49 Estimated TAP Emission Rates from the Filter Farm Stack during Neutralization/GPCR/TW-SCWO of ACW Containing GB Agent at PBA^a

Compound	Emission Rate (lb/h) ^b
1,1,1-Trichloroethane	5.6E-13
1,2,4-Trimethylbenzene	6.1E-14
1H-Indene, 2,3-dihydro-	3.7E-13
2-Methylnaphthalene	1.4E-13
2-Nitrophenol	4.0E-14
9H-Fluoren-9-one	2.2E-11
Acenaphthene	7.2E-15
Anthracene	8.0E-14
Antimony	1.3E-14
Arsenic	5.3E-14
Benzaldehyde	2.2E-13
Benzene	9.8E-12
Benzo(a)anthracene	1.5E-14
Beryllium	5.7E-15
Bis(2-ethylhexyl)phthalate	5.3E-14
Butanal	6.2E-14
C3-Alkyl benzenes	3.8E-12
Cadmium	2.4E-14
Calcium	6.8E-11
Chrysene	3.1E-14
Cobalt	7.5E-14
Cyclohexane, butyl-	4.5E-14
Cyclohexanone	3.0E-13
Decane	4.9E-13
Decane, 2,6,7-trimethyl-	4.1E-14
Decane, 4-methyl-	5.4E-14
Decane, 5-methyl-	1.9E-13
Dibenzofuran	4.7E-13
Diphenylmethane	4.0E-14
Dodecane	9.1E-13
Dodecane, 2,6,10-trimethyl-	5.7E-14
Dodecane, 4-methyl-	1.7E-13
Dodecane, 6-methyl-	1.0E-13
Ethanol, 2-(2-butoxyethoxy)-, acetate	1.9E-13
Ethanone, 1-(3-methylphenyl)-	6.1E-14
Ethanone, 1-phenyl-	4.4E-13
Ethylene Glycol	1.7E-12
Fluoranthene	9.5E-14
Fluorene	1.7E-13
HCl	3.6E-11
Heptadecane	1.3E-13
Heptanal	2.3E-12

TABLE 3.49 (Cont.)

Compound	Emission Rate (lb/h) ^b
Heptane, 3-ethyl-2-methyl-	1.3E-13
Hexadecane, 2,6,10,14-tetramethyl-	2.5E-13
Hexanal	8.1E-13
Hf	3.7E-04
Iron	6.7E-12
Isobutyl alcohol	7.1E-13
Lead	2.9E-13
Magnesium	2.1E-11
Malonic acid	1.6E-10
Manganese	9.4E-13
Mercury	1.3E-13
Methylene chloride	9.9E-10
Molybdenum	3.5E-13
M-Tolualdehyde	5.6E-13
Naphthalene	9.3E-13
Naphthalene, 1-methyl	1.5E-13
Nickel	2.0E-13
Nitrobenzene	5.0E-13
Nonane, 2,6-dimethyl-	1.5E-13
Pentanal	1.0E-12
Phenanthrene	4.2E-13
Phenol	1.2E-13
Phosphorus	1.0E-10
Propanal	7.5E-13
P-xylene	1.8E-13
Pyrene	5.2E-14
Silver	6.8E-14
Tetradecane	5.6E-13
Toluene	3.2E-12
Tridecane	8.8E-13
Undecane	8.2E-13
Undecane, 2,10-dimethyl-	2.5E-13
Undecane, 2,6-dimethyl-	3.1E-13
Undecane, 2-methyl-	2.0E-13
Vanadium	1.2E-14
Total HAPs	3.7E-04
CO	9.2E-02
NO _x	3.8E-10
Particulates	3.8E-09
SO ₂	5.3E-03
Total VOCs	2.0E-10

^a Total campaign length of 376 operating days.

^b Daily emission rates can be estimated on the basis of the assumption that there are 12 operating hours per day.

TABLE 3.50 Estimated TAP Emission Rates from the Filter Farm Stack during Neutralization/GPCR/TW-SCWO of ACW Containing VX Agent at PBA^a

Compound	Emission Rate ^b (lb/h)
1,2,4-Trimethylbenzene	1.6E-11
1,4-Dichlorobenzene	3.6E-14
1-Ethyl-2,2,6-trimethylcyclohexane	1.2E-11
2-(2-Butoxyethoxy) ethanol	1.4E-11
2-Methylnaphthalene	5.9E-12
Acetic acid	4.4E-12
Anthracene	3.3E-14
Antimony	8.4E-12
Benzene	1.0E-11
Benzene, 1,2,3-trimethyl-	3.1E-12
Benzene, 1,2,4,5-tetramethyl-	1.5E-11
Benzene, 1-methyl-2-propyl-	1.4E-11
Benzene, 1-methyl-3-propyl-	3.5E-12
Benzyl Alcohol	1.4E-11
Bis(2-ethylhexyl)phthalate	5.0E-14
Butanal	2.3E-13
Cadmium	2.4E-12
Calcium	5.4E-10
Cobalt	1.4E-12
Cyclohexane, 2-butyl-1,1,3-trimethyl-	2.7E-12
Cyclohexane, butyl-	2.2E-11
Cyclohexane, hexyl-	3.1E-12
Cyclohexanol	7.0E-12
Cyclohexanone	6.0E-14
Decane	8.9E-11
Decane, 2-methyl-	2.0E-11
Decane, 3-methyl-	1.5E-11
Decane, 4-methyl-	1.1E-11
Dibenzofuran	5.4E-13
Diethylene glycol	4.1E-11
Dodecane	3.4E-11
Dodecane, 6-methyl-	1.1E-11
Ethylene glycol	1.4E-11
Fluoranthene	6.6E-14
Fluorene	1.9E-13
HCl	2.2E-04
Heptane, 3-ethyl-2-methyl-	6.7E-12
Hexanal	8.3E-13
Isobutyl alcohol	1.4E-11
Lead	8.6E-11
Magnesium	1.5E-10
Manganese	4.8E-10
Methylene chloride	5.5E-12

TABLE 3.50 (Cont.)

Compound	Emission Rate ^b (lb/h)
Molybdenum	1.7E-11
m-Tolualdehyde	3.9E-13
Naphthalene	4.6E-12
Naphthalene, 1,2,3,4-tetrahydro-	7.7E-12
Naphthalene, 1,2,3,4-tetrahydro-6-methyl-	4.0E-12
Naphthalene, 1,7-dimethyl-	4.4E-12
Nonane, 2,6-dimethyl-	3.7E-11
Nonane, 3,7-dimethyl-	5.5E-12
Nonane, 3-methyl-	2.8E-12
Octane, 3,6-dimethyl-	1.3E-11
Pentadecane	9.1E-12
Phenanthrene	4.4E-13
Phosphorus	1.6E-09
Potassium	7.2E-10
Propanal	7.3E-13
Pyrene	3.0E-14
Silver	5.1E-13
Sodium	5.3E-10
Tetradecane	4.2E-11
Toluene	1.9E-12
Tridecane	1.9E-11
Tridecane, 2-methyl-	1.2E-11
Tridecane, 4-methyl-	5.5E-12
Tridecane, 6-propyl-	4.2E-12
Undecane	5.6E-11
Undecane, 2,10-dimethyl-	2.5E-12
Undecane, 3,6-dimethyl-	8.7E-12
Undecane, 4-methyl-	5.8E-12
Vanadium	8.5E-13
Total HAPs	2.2E-04
CO	1.5E-03
NO _x	1.3E-02
Particulates	1.0E-07
SO ₂	4.0E-03
Total VOCs	4.5E-10

^a Total campaign length of 108 operating days.

^b Daily emission rates can be estimated on the basis of the assumption that there are 12 operating hours per day.

TABLE 3.51 Estimated TAP Emission Rates from the Product Gas Burner Stack during Neutralization/GPCR/TW-SCWO of ACW Containing GB Agent at PBA^a

Compound ^b	Emission Rate ^c (lb/h)
1,1,1-Trichloroethane	6.9E-07
1,2,3,4,6,7,8-HpCDF	1.1E-13
1,2,3,4,7,8-HxCDF	8.2E-13
1,2,3,6,7,8-HxCDF	3.1E-13
1-Hexanol, 2-ethyl-	2.1E-04
1H-Indene	5.3E-05
2,3,7,8-TCDF	4.9E-13
2,4-Dimethylphenol	2.1E-05
2-Butanone	7.3E-06
Acetone	1.9E-03
Aluminum	7.0E-05
Antimony	2.3E-07
Arsenic	3.3E-06
Barium	3.1E-06
Benzaldehyde	7.3E-05
Benzaldehyde, 4-ethyl-	1.7E-05
Benzaldehyde, ethyl-	1.0E-05
Benzaldehyde, ethyl-Benzenemethanol, 4-(1-methylethyl)-	9.5E-06
Benzene	5.1E-05
Benzo(a)anthracene	5.6E-07
Benzyl alcohol	1.3E-05
Beryllium	6.0E-08
Bis(2-ethylhexyl)phthalate	1.5E-05
Cadmium	9.5E-07
Calcium	1.6E-04
Carbon disulfide	2.0E-06
Chloroform	3.1E-05
Chromium	8.5E-06
Cobalt	2.8E-07
Copper	1.6E-05
Cyclododecane	2.3E-05
Cyclotetrasiloxane, octamethyl-	2.3E-05
Dibenzofuran	8.1E-06
Diethylphthalate	1.4E-05
Di-n-butylphthalate	2.9E-05
Dodecane	8.9E-06
Ether	1.5E-03
Ethylbenzene	4.7E-05
Fluorene	3.7E-07
HCl	6.0E-04
Hexane	9.6E-04
HF	1.1E-05
Hydrogen cyanide	4.2E-05
Hydrogen sulfide	6.1E-02
Iron	1.0E-04
Lead	1.3E-06
Magnesium	2.4E-05
Manganese	2.3E-04
Methylene chloride	8.3E-05

TABLE 3.51 (Cont.)

Compound ^b	Emission Rate ^c (lb/h)
Molybdenum	6.8E-04
Naphthalene	1.2E-06
Nickel	9.9E-06
Nitrobenzene	3.5E-06
Phenol	3.0E-05
Phosphorus	4.5E-05
Selenium	1.3E-06
Silver	8.4E-07
Sodium	2.0E-03
Styrene	4.3E-06
Tetrachloroethene	6.2E-07
Thallium	3.0E-07
Tin	1.2E-05
Toluene	6.9E-06
Total HpCDF	1.2E-14
Total HxCDD	6.1E-12
Total HxCDF	1.3E-11
Total PeCDD	3.5E-12
Total PeCDF	4.4E-12
Total TCDD	2.9E-12
Total TCDF	6.2E-12
Trichloroethene	6.2E-07
Vanadium	9.1E-07
Xylenes	3.2E-06
Zinc	1.3E-05
Total dioxins/furans	1.7E-12
CO	3.4E-03
NO _x	2.0E-01
Particulates	7.7E-02
SO ₂	9.4E-03
Total VOCs	3.1E-03
Total HAPs	6.3E-02

^a Total campaign length of 376 operating days.

^b Abbreviations: HpCDF = heptachlorodibenzo-p-furan; HxCDD = hexachlorodibenzo-p-dioxin; HxCDF = hexachlorodibenzo-p-furan; PeCDD = pentachlorodibenzo-p-dioxin; PeCDF = pentachlorodibenzo-p-furan; TCDD = tetrachlorodibenzo-p-dioxin; and TCDF = tetrachlorodibenzo-p-furan.

^c Daily emission rates can be estimated assuming 12 operating hours per day.

TABLE 3.52 Estimated TAP Emission Rates from the Product Gas Burner Stack during Neutralization/GPCR/TW-SCWO of ACW Containing VX Agent at PBA^a

Compound ^b	Emission Rate ^c (lb/h)
1,1,1-Trichloroethane	5.3E-07
1-Hexanol, 2-ethyl-	8.2E-11
1H-Indene	6.3E-10
2,4-Dimethylphenol	2.4E-10
2-Butanone	1.6E-04
Acetone	4.0E-05
Aluminum	3.7E-10
Antimony	1.6E-05
Arsenic	5.6E-06
Barium	1.4E-03
Benzaldehyde	5.4E-05
Benzaldehyde, 4-ethyl-	1.8E-07
Benzaldehyde, ethyl-	2.5E-06
Benzaldehyde, ethyl-Benzenemethanol, 4-(1-methylethyl)-	2.4E-06
Benzene	5.6E-05
Benzo(a)anthracene	1.3E-05
Benzyl alcohol	7.8E-06
Beryllium	7.3E-06
Bis(2-ethylhexyl)phthalate	3.9E-05
Cadmium	4.3E-07
Calcium	1.0E-05
Carbon disulfide	4.6E-08
Chloroform	1.2E-05
Chromium	7.3E-07
Cobalt	1.2E-04
Copper	1.5E-06
Cyclododecane	2.4E-05
Cyclotetrasiloxane, octamethyl-	6.6E-06
Diethylphthalate	2.2E-07
Di-n-butylphthalate	1.2E-05
Dodecane	1.7E-05
Ether	1.7E-05
Ethylbenzene	6.2E-06
Fluorene	1.1E-05
HCl	2.2E-05
Hexane	6.8E-06
HF	1.2E-03
Hydrogen cyanide	3.6E-05
Hydrogen sulfide	2.8E-07
Iron	4.6E-04
Lead	7.3E-04
Magnesium	8.1E-06
Manganese	3.2E-05
Methylene chloride	4.7E-02
Naphthalene	9.6E-07
Nickel	1.8E-05
Nitrobenzene	1.8E-04
Phenol	6.3E-05
Phosphorus	5.2E-04

TABLE 3.52 (Cont.)

Compound ^b	Emission Rate ^c (lb/h)
Selenium	9.0E-07
Silver	7.6E-06
Sodium	2.7E-06
Styrene	2.3E-05
Tetrachloroethene	3.5E-05
Thallium	1.0E-06
Tin	6.4E-07
Toluene	1.6E-03
Trichloroethene	3.3E-06
Vanadium	4.7E-07
Xylenes	2.3E-07
Zinc	9.4E-06
1,2,3,4,6,7,8-HpCDF	5.3E-09
1,2,3,4,7,8-HxCDF	9.1E-15
1,2,3,6,7,8-HxCDF	4.7E-15
2,3,7,8-TCDF	9.7E-15
Dibenzofuran	2.7E-12
Total HpCDF	3.3E-12
Total HxCDD	2.2E-12
Total HxCDF	4.8E-12
Total PeCDD	4.7E-07
Total PeCDF	7.0E-07
Total TCDD	2.4E-06
Total TCDF	9.6E-06
Total dioxins/furans	4.9E-05
CO	1.3E-09
NO _x	5.9E-02
Particulates	1.4E-01
SO ₂	2.5E-03
Total VOCs	3.9E-03
Total HAPs	2.4E-03

^a Total campaign length of 108 operating days.

^b Abbreviations: HpCDF = heptachlorodibenzo-p-furan; HxCDD = hexachlorodibenzo-p-dioxin; HxCDF = hexachlorodibenzo-p-furan; PeCDD = pentachlorodibenzo-p-dioxin; PeCDF = pentachlorodibenzo-p-furan; TCDD = tetrachlorodibenzo-p-dioxin; and TCDF = tetrachlorodibenzo-p-furan.

^c Daily emission rates can be estimated assuming 12 operating hours per day.

TABLE 3.53 Estimated Emissions from Worker Commuter Vehicles during Neutralization/GPCR/TW-SCWO Operations at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Emission Rate (tons/yr)
HC	198,000	1.16	20	16.4
CO	198,000	11.38	20	160.5
NO _x	198,000	0.73	20	10.3
SO _x	198,000	0.12	20	1.7
PM ₁₀	198,000	0.055	20	0.78

^a Number of auto round trips to the operation site estimated on the basis of the total operating personpower and an assumption of 276 days of operations per year.

^b Emission factors determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

3.3.4.3.5 Activities

The PMACWA described activities for installation of the neutralization/GPCR/TW-SCWO system at PBA (PMACWA 2001b). The major phases of the project are shown in Table 3.59.

3.3.4.3.6 Uncertainties

As indicated earlier, each of the individual technologies that form the neutralization/GPCR/TW-SCWO system has either been previously proven to be a successful technology or has been demonstrated by the PMACWA to be an acceptable technology for application at PBA. However, demonstration testing focused on individual technologies and sometimes used less than full-scale units. In addition, although EDSs were conducted to evaluate the long-term adequacy of individual technologies, it was not possible to evaluate the long-term viability and performance of the entire, integrated treatment system. Thus, the primary uncertainty associated with neutralization/GPCR/TW-SCWO is that the entire, integrated treatment system with all its component units has not been assembled and tested. The pilot program, if implemented for this technology system, would be designed to evaluate overall operability and long-term performance.

TABLE 3.54 Estimated Generation Rates of SCWO Brine Salts from Neutralization/GPCR/TW-SCWO at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB	VX
Aluminum	6.2E+01	5.9E+01
Antimony	1.1E-03	2.9E-03
Arsenic	4.2E-02	3.3E-03
Barium	1.1E-03	8.3E-04
Beryllium	5.2E-04	4.0E-04
Cadmium	1.2E-04	0.0E+00
Calcium silicate	3.8E+00	3.3E+00
Chloride	0.0E+00	5.7E+00
Chromium	6.2E-03	6.0E-03
Cobalt	7.2E-04	1.3E-03
Copper	4.1E-03	3.3E-03
Cyanide	2.3E-03	6.5E-03
Fluoride	0.0E+00	2.9E+00
Iron	1.4E-01	6.9E-02
Lead	2.5E+01	1.9E+01
Magnesium	2.3E-02	7.6E-03
Manganese	1.7E-03	1.1E-03
Mercury	1.8E-04	0.0E+00
Molybdenum	3.9E-03	2.6E-03
Nickel	4.8E-02	3.1E-02
Nitrate-N	3.7E+00	6.1E+00
Nitrite-N	5.1E+00	1.1E+01
Phosphorus	7.5E+01	1.3E+01
Potassium	8.3E-01	2.9E-03
Silver	1.2E-03	0.0E+00
Sodium fluoride	7.3E+02	0.0E+00
Sodium phosphate	1.9E+04	1.4E+04
Sodium sulfate	2.0E-03	1.4E+03
Sulfide	0.0E+00	3.6E-01
Sulfur	0.0E+00	0.0E+00
Thallium	1.2E-03	1.7E-03
Water in salt cake	3.0E+03	2.3E+03
Zinc	4.0E-02	8.7E-03
Total	2.3E+04	1.8E+04
Operating days	376	108
Specific density	1.6E+00	1.7E+00

TABLE 3.55 Estimated Generation Rates of TRBP Residues from Neutralization/GPCR/TW-SCWO at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB	VX
2-Pentanone, 4-hydroxy-4-methyl-	1.1E-01	2.9E-01
Aluminum	2.1E+02	5.8E+02
Antimony	1.1E-05	2.9E-05
Arsenic	3.1E-02	8.5E-02
Barium	1.1E-05	8.4E-06
Beryllium	1.8E-03	4.9E-03
Calcium silicate	2.9E-04	2.5E-04
Chloride	1.1E+01	0.0E+00
Chromium	8.6E-02	2.4E-01
Cobalt	9.0E-03	2.5E-02
Copper	2.9E-02	8.0E-02
Cyanide	1.5E-02	4.2E-02
Cyanide, reactive	6.2E-01	1.7E+00
Disodium phosphate	2.5E+01	1.5E+01
Fluoride	0.0E+00	1.3E+00
Iron	4.2E+00	1.1E+01
Lead	2.5E-01	1.9E-01
Magnesium	1.1E+01	2.9E+01
Manganese	7.2E-01	2.0E+00
Mercury	4.2E-03	1.1E-02
Naphthalene	1.5E-03	4.2E-03
Nickel	5.1E-02	1.4E-01
Nitrate-N	4.0E-02	1.1E-01
Nitrite-N	2.3E-02	6.3E-02
Octadecanoic acid, butyl ester	2.5E-02	6.8E-02
Phosphorus	1.0E+00	2.8E+00
Potassium	9.0E+01	2.9E-05
Sodium chloride	7.4E+00	4.3E-05
Sodium fluoride	1.1E-05	0.0E+00
Sodium sulfide	0.0E+00	7.7E+00
Sulfate	2.2E-01	6.1E-01
Unknown alcohol	4.6E-02	1.3E-01
Unknown alkane	3.2E-02	8.9E-02
Unknown amide	1.9E-02	5.1E-02
Unknown amine	3.7E-02	1.0E-01
Vanadium	6.5E-02	1.8E-01
Zinc	3.4E+00	9.4E+00
Total	3.7E+02	6.7E+02
Operating days	376	108

TABLE 3.56 Estimated Generation Rates of 5X Solids from Neutralization/GPCR/TW-SCWO at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB Agent	VX Agent
Aluminum	8.8E+02	6.7E+02
Aluminum oxide	5.5E+03	4.2E+03
Carbon (from wood and resin)	9.5E+02	7.2E+02
Glass fiber	9.3E+03	7.0E+02
Steel/iron	5.6E+03	6.3E+03
Total	2.2E+04	1.3E+04
Operating days	376	108

3.3.5 ELECTROCHEMICAL OXIDATION

This description of the electrochemical oxidation technology system is based on several primary reports. A description of the proposed technology system can be found in the technology provider's demonstration report (AEA/CH2MHILL 2000) and is referred to by its developers as "SILVER II." As indicated in that report, many of the estimates provided for facility design and operation refer comparatively to the U.S. Army baseline incineration process, which indicates, in general, that estimates are comparable to those associated with the baseline incineration process. Thus, another of the primary sources for this section of the TRD is the EIS for disposal of chemical agents and munitions stored at Pine Bluff Arsenal, Arkansas (PMCD 1997). That is the most recent EIS that the U.S. Army has prepared for baseline incineration of chemical munitions.

In addition to the above, mass balance estimates, air emission estimates, and solid waste estimates for application of the electrochemical oxidation technology at PBA have been developed (Mitretek 2001d). Air emissions and solid waste estimates for electrochemical oxidation, as discussed below, are based on Mitretek inputs, along with appropriate assumptions on filtration systems, plant operations, and schedule.

Many of the figures and tables referred to in the facility description for this technology system contain estimates (e.g., emissions, resources consumed) associated with processing ACWs with a specified agent. These estimates are given on an annual basis (e.g., tons/yr). In some cases, these estimates have been converted from other units (e.g., lb/d) by accounting for the number of days of operation required for processing a specific type of ACW. This time period is referred to as a campaign; a campaign is agent-specific. The values in many of the

TABLE 3.57 Transportation Data for Solid Wastes from Neutralization/ GPCR/TW-SCWO during Processing of ACW Containing GB Agent at PBA

Type of Data	Output Material No. 1	Output Material No. 2	Output Material No. 3
Transported materials			
Type/chemical	Brine salts – waste	TRBP residue – waste	5X solids – waste
Physical form	Solid	Solid	Solid
Chemical composition/ temperature, pressure	See Table 3.54	See Table 3.55	See Table 3.56
Packaging			
Type ^a	55-gal drum	55-gal drum	55-gal drum
Container volume (ft ³)	7.35	7.35	7.35
Certified by	DOT	DOT	DOT
Identifier	Varies	Varies	Varies
Container weight (lb)	50	50	50
Material weight (lb)	760	970	450
Chemical content (wt%)	See Table 3.54	See Table 3.55	See Table 3.56
Shipments			
Average weight (tons/yr) ^b	3,205	51	2,941
Average volume (ft ³ /yr)	62,630	770	97,820
Packages/yr	8,519	105	13,305
Packages/shipment	48	36	48
Shipments/yr	178	3	278
Form of transport/routing			
Form of transportation	Truck	Truck	Truck
Destination – facility type	Land disposal ^c	Land disposal ^c	Land disposal ^c

^a Review of the disassembly process indicates that the dimensions of the solids would allow disposal in standard 55-gal drums. Further validation with the vendor may be required.

^b Annual estimates based on 276 days of operations per year.

^c Depending on test results for hazardous constituents, off-site disposal at a RCRA-permitted facility may be required.

following figures and tables are based on the number of days in the campaign required to process ACW containing a specific agent. It was assumed that there are 276 days of operation in a year. If the campaign is less than or equal to 276 days, annual quantities equal total quantities. If the campaign is greater than 276 days, quantities in the figures and tables are for 276 days of processing. In the latter case, the estimates provided are less than total quantities. Daily (or other) quantities may be obtained by adjusting for the number of days in the campaign.

Figures 3.34 and 3.35 provide input/output material balances for the major streams for electrochemical oxidation of ACW containing GB and VX agent, respectively. The amounts of air, potable water, natural gas input, treated off-gas, ventilation air, wastewater, and boiler flue gas shown in each of these figures represent total annual amounts.

**TABLE 3.58 Transportation Data for Solid Wastes from Neutralization/GPCR/
TW-SCWO during Processing of ACW Containing VX Agent at PBA**

Type of Data	Output Material No. 1	Output Material No. 2	Output Material No. 3
Transported materials			
Type/chemical	Brine salts – waste	TRBP residue – waste	5X solids – waste
Physical form	Solid	Solid	Solid
Chemical composition/ temperature, pressure	See Table 3.54	See Table 3.55	See Table 3.56
Packaging			
Type ^a	55-gal drum	55-gal drum	55-gal drum
Container volume (ft ³)	7.35	7.35	7.35
Certified by	DOT	DOT	DOT
Identifier	Varies	Varies	Varies
Container weight (lb)	50	50	50
Material weight (lb)	770	1,220	450
Chemical content (wt%)	See Table 3.54	See Table 3.55	See Table 3.56
Shipments			
Average weight (tons/yr) ^b	885	32	1,939
Average volume (ft ³ /yr)	16,910	390	64,490
Packages/yr	2,300	54	8,772
Packages/shipment	48	32	48
Shipments/yr	48	2	183
Form of transport/routing			
Form of transportation	Truck	Truck	Truck
Destination – facility type	Land disposal ^c	Land disposal ^c	Land disposal ^c

^a Review of the disassembly process indicates that the dimensions of the 5X solids would allow disposal in standard 55-gal drums. Further validation with the vendor may be required.

^b Annual estimates based on a campaign length of 108 days.

^c Depending on the test results for hazardous constituents, off-site disposal at a RCRA-permitted facility may be required.

3.3.5.1 General Facility Description

The proposed electrochemical oxidation facility is designed to fit approximately into the same space and general configuration as the baseline incineration process. The physical plant is expected to consist of a two-story building constructed of noncombustible materials, with a concrete structural frame and a low-slope concrete roof.

The site layout for the electrochemical oxidation facility is shown in Figures 3.36 through 3.38. Figure 3.36 shows the general facility layout, Figure 3.37 shows the layout of the first floor of the MDB, and Figure 3.38 shows the layout of the second floor of the MDB. Additional diagrams may be found in AEA/CH2MHILL (2000). In addition, AEA/CH2MHILL (2000) provides descriptions of the various units and operations that are to be included in each section of the building, as shown in Figures 3.36 through 3.38.

3.3.5.2 Construction Phase

The schedule for destruction of the stockpile at PBA, although tentative, calls for construction of the selected alternative to begin following issuance of the EIS ROD and receipt of the RCRA permit and any other environmental permits, as necessary. It is anticipated that the construction schedule of the electrochemical oxidation facility would be similar to that of the baseline incineration facility. Construction would take approximately 30 months (PMACWA 2001b), including a 2-month design and procurement verification period. However, the PMACWA is investigating means of shortening the construction phase.

Construction of the destruction facility at PBA would result in consumption of materials and resources, vehicle exhaust emissions, fugitive dust, noise, destruction of wildlife habitat and native vegetation, increased employment, increased demand for public services, and occupational health hazards.

TABLE 3.59 Activities for Neutralization/GPCR/TW-SCWO at PBA

Key Milestones
EIS start
Start of EDS-II testing
PMACWA programmatic EIS submittal
PMACWA programmatic ROD submittal
DOD technology decision
RCRA Part B and CAA permits approval
MDB construction start
MDB construction completion
Systemization/pilot test start
Systemization/pilot test completion
Operations start
Operations completion

Source: PMACWA (2001b).

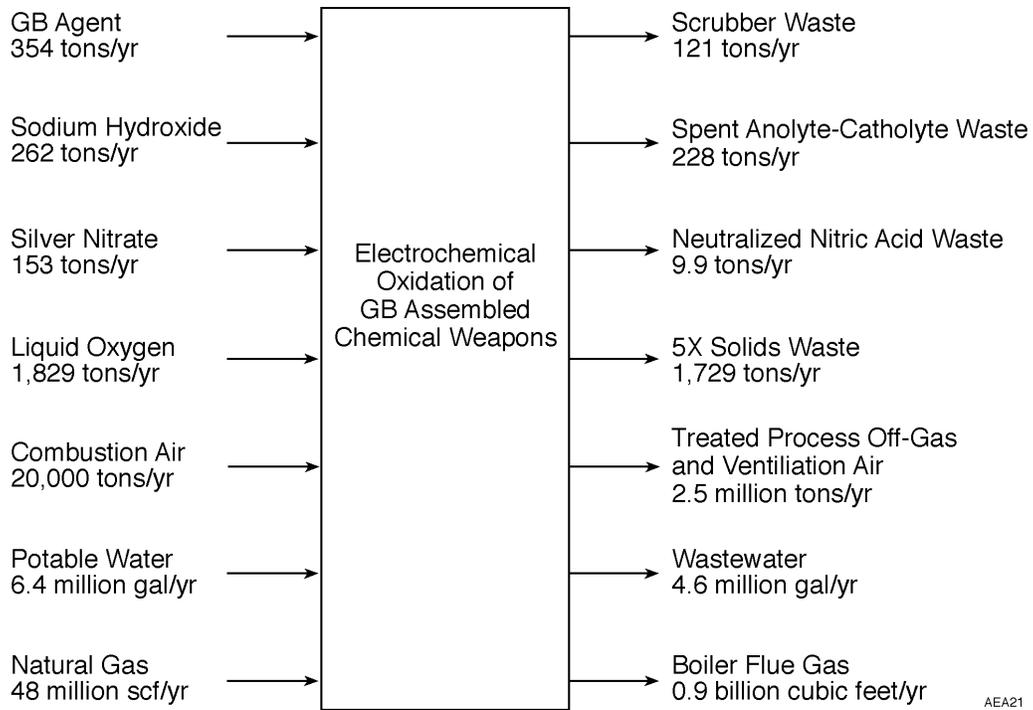


FIGURE 3.34 Input/Output Material Balance for Electrochemical Oxidation of ACW Containing GB Agent at PBA

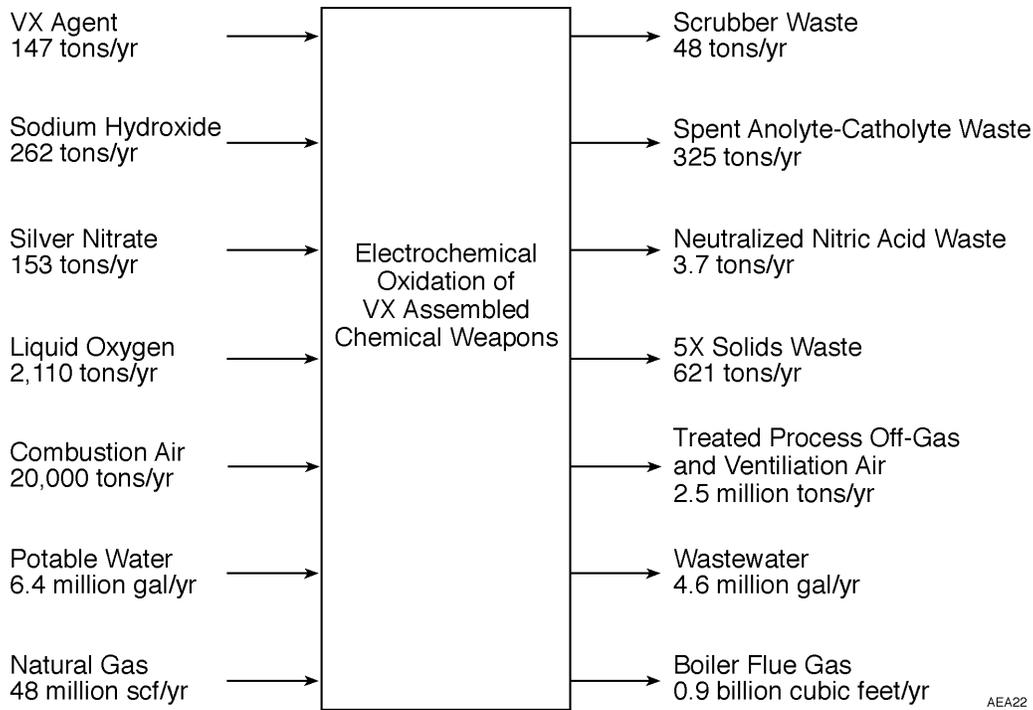


FIGURE 3.35 Input/Output Material Balance for Electrochemical Oxidation of ACW Containing VX Agent at PBA

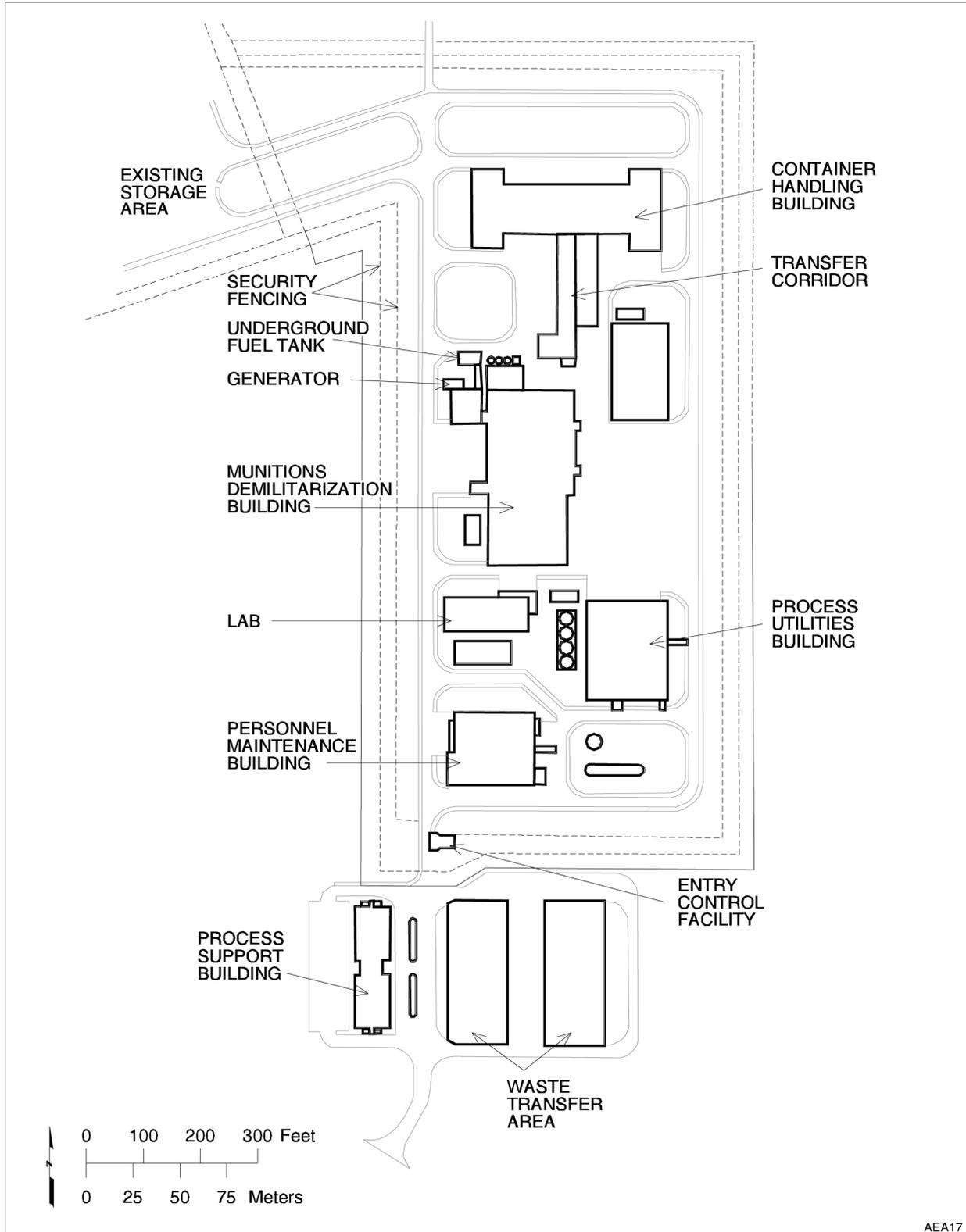


FIGURE 3.36 Facility Layout for Electrochemical Oxidation at PBA (Source: Adapted from AEA/CH2MHILL 2000)

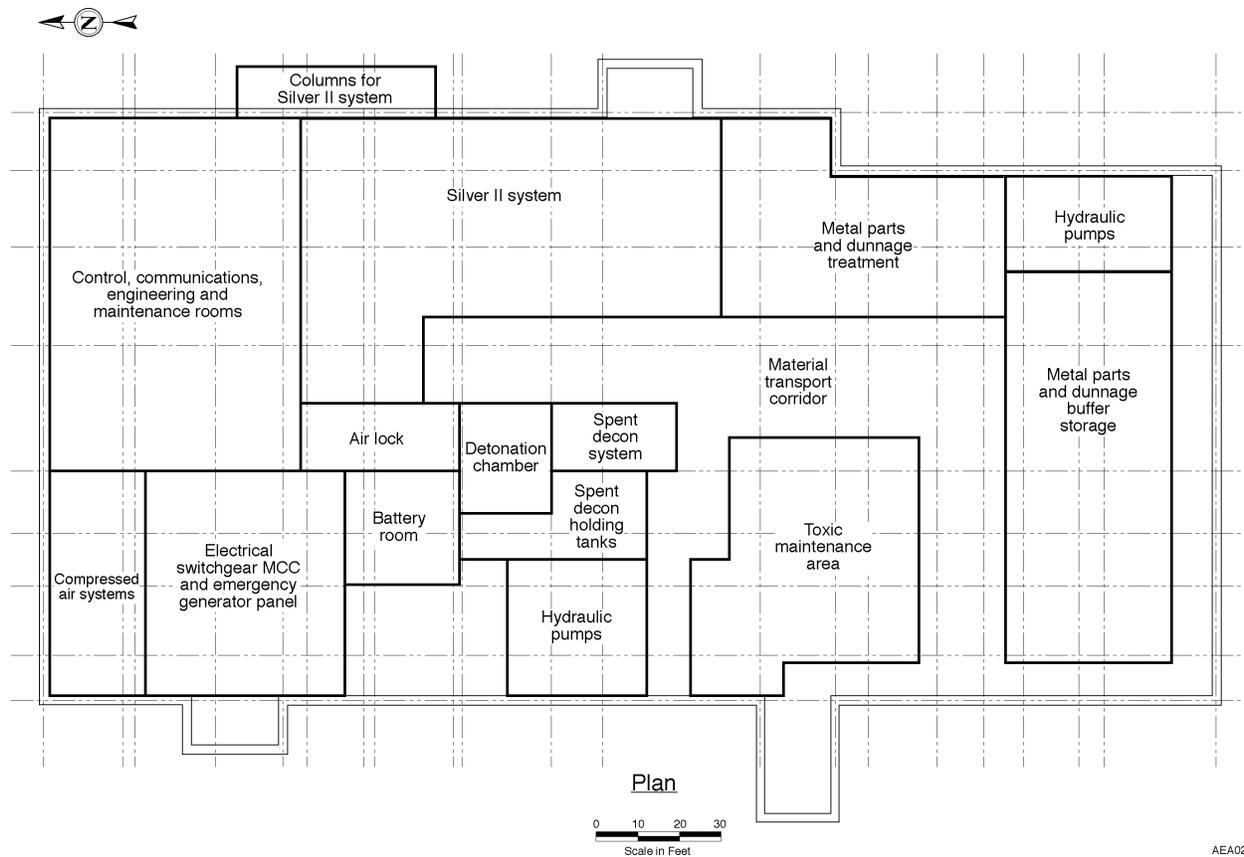


FIGURE 3.37 Layout of First Floor of the Munitions Demilitarization Building for the Electrochemical Oxidation Facility at PBA (Source: Adapted from AEA/CH2MHILL 2000)

3.3.5.2.1 Construction Inputs and Resource Requirements

Resources and materials needed for construction of the disposal facility would include water, electricity, structural and piping steel, concrete, vehicle fuel, and industrial gases (propane). Table 3.60 contains order-of-magnitude estimates of the materials and resources that would be consumed during construction. These estimates are based on material and resource estimate methodologies used in engineering analyses and environmental documents concerning DOE waste management activities. For example, estimates of 20 gal (76 L) of water for each construction FTE and solidification requiring 26 lb (12 kg) of water for each 100 lb (45 kg) of cement are from DOE (1997). More precise estimates would require a detailed consideration of construction activities.

Process equipment would use some materials that are also used in construction, such as steel. However, the amount of such material used for process equipment is expected to be small compared to that used in building construction and is not considered in Table 3.60.

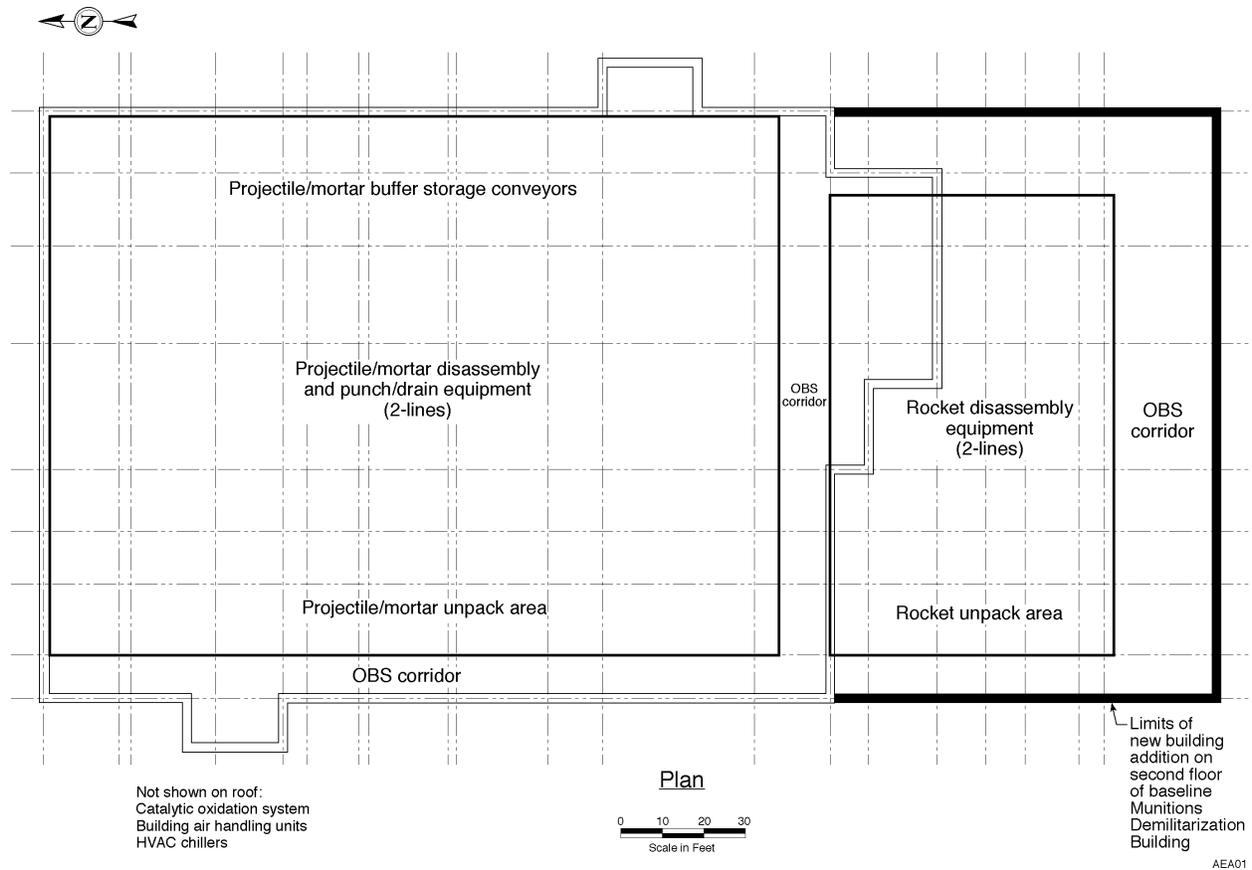


FIGURE 3.38 Layout of Second Floor of the Munitions Demilitarization Building for the Electrochemical Oxidation Facility at PBA (Source: Adapted from AEA/CH2MHILL 2000)

Table 3.61 gives order-of-magnitude estimates of the number of shipments of construction material to the site. These estimates do not include shipments of process and related equipment, the number of which is expected to be small compared to the number of shipments of construction material. It was assumed that constituents of cement and backfill would be shipped in end-dump trucks with a capacity of 10 yd³ (8 m³), that steel would be shipped on trucks with a 21-ton (19 t) net payload, and that liquid fuel would be shipped in tank trucks with a nominal capacity of 9,000 gal (34,000 L).

Order-of-magnitude estimates of the emission of criteria pollutants from construction delivery vehicles are provided in Table 3.62. It was assumed that the delivery vehicles would be heavy-duty diesel trucks and that the length of a one-way trip would be 20 mi (32 km). Actual trip distances would depend on a number of factors, including the availability of construction materials from local distributors and the distance of the site from the distributors.

TABLE 3.60 Estimated Materials/Resources Consumed during Construction of an Electrochemical Oxidation Facility at PBA^a

Construction Material/Resource	Total Consumption	Peak Demand
Utilities		
Water ^b	9,000,000 gal	NA ^c
Electricity ^d	57,000 MWh	2.85 MW
Solids		
Concrete	29,700 yd ³	NA
Steel	6,600 tons	NA
Piping	120,000 linear feet	NA
Liquids		
Fuel ^d	2,300,000 gal	NA
Gases		
Industrial gases (propane) ^d	6,100 gal	NA

^a All values can be considered order-of-magnitude approximations of the actual values; more accurate values would require a detailed consideration of construction activities.

^b Water requirement estimated is based on DOE (1997), in which each FTE required 20 gal/d, and solidification required 26 lbs per 100 lb of cement.

^c NA = not applicable.

^d Scaling method based on Folga et al. (1999).

3.3.5.2.2 Construction Workforce

The construction workforce is expected to increase steadily to a peak of about 1,100 FTEs near the midpoint of the 30-month construction period, and then to decrease steadily until construction is completed. The average number of construction workers per month would be approximately 550 FTEs. The total effort during construction is estimated to be nearly 1,400 FTE-years. These estimates were developed from an activity-based approach that considered the various types of buildings, required instrumentation, process equipment installation, and other related construction activities. Table 3.63 provides an estimate of the employment buildup by year.

TABLE 3.61 Order-of-Magnitude Estimate of the Number of Truck Shipments of Construction Materials during Construction of an Electrochemical Oxidation Facility at PBA^a

Resource	Total Consumption	Truck Capacity	No. Truck Shipments
Portland cement	3,267 yd ³	10 yd ³	327
Gravel ^b	12,177 yd ³	10 yd ³	1,218
Sand ^b	7,722 yd ³	10 yd ³	773
Steel ^c	6,600 tons	21 tons	320
Asphalt paving ^d	1,600 tons	20 tons	80
Backfill ^e	12,000 yd ³	10 yd ³	1,200
Fuel ^f	2,300,000 gal	9,000 gal	260
Total			4,178
Total (rounded up)			5,000

^a The calculation did not include truck deliveries of process equipment and related items.

^b Assumes that concrete is composed of 11% portland cement, 41% gravel, and 26% sand and is shipped to the site in a standard 10-yd³ end-dump truck.

^c Assumes that the net payload for steel transport to the site is 42,000 lb.

^d Assumes that HMA is loaded into 20-ton-capacity triaxle trucks for transport to the paving site.

^e Assumes that shipment is in standard 10-yd³ end-dump trucks and no fill material is available on-site.

^f Assumes shipment is in a DOT 406/MC-306 atmospheric pressure tank truck with a 9,000-gal capacity.

3.3.5.2.3 Construction Emissions and Waste Estimates

During the construction phase, fugitive emissions would consist mainly of dust and vehicle emissions. Temporary, regional increases in atmospheric concentrations of CO, NO_x, hydrocarbons, particulate matter, and SO_x would result from the exhaust emissions of commuter vehicles, heavy construction vehicles, diesel generators, and other machinery and tools. Annual emissions of these pollutants would be small in comparison to de minimis levels used by regulators to determine whether an air quality permit or impact analysis is necessary. Emissions from construction vehicles are exempt from permit requirements. Nevertheless, vehicles would be equipped with standard pollution control devices to minimize air quality impacts.

TABLE 3.62 Estimated Emissions from Delivery Vehicles during Construction of an Electrochemical Oxidation Facility at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance(mi) ^c	Construction Period (yr)	Emission Rate (tons/yr)
HC	5,000	2.12	20	2.5	0.3
CO	5,000	11.28	20	2.5	1.6
NO _x	5,000	1.25	20	2.5	0.2
SO _x	5,000	0.23	20	2.5	0.03
PM ₁₀	5,000	0.617	20	2.5	0.1

^a Number of auto round trips to the construction site estimated on the basis of the total number of deliveries.

^b Emission factors determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x, and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

TABLE 3.63 Estimated Number of Employees Needed by Year for Construction of an Electrochemical Oxidation Facility at PBA

Employees	Year 1	Year 2	Year 3
Total craft workers	360	640	100
Construction management and support staff	90	160	30
Total	450	800	130

Estimated emissions from construction activities (not including emissions from delivery vehicles) are shown in Table 3.64. The emissions shown are based on the anticipated construction land disturbance and vehicle traffic (for dust particulate pollutants) and fuel and gas consumption. The column marked "Total" indicates the total amount of emissions that is estimated to occur over the entire construction period.

Emissions from construction worker commuter vehicles were estimated on the basis of the assumption that an average of about 550 automobiles (one car per construction worker) would be added to the area. As with construction delivery vehicles, it was assumed that a one-way trip in a commuter vehicle would be 20 mi (32 km). Table 3.65 gives the estimated annual emissions of criteria pollutants arising from these trips.

TABLE 3.64 Estimated Emissions during Construction of an Electrochemical Oxidation Facility at PBA

Criteria Pollutant	Total (tons)	Annual (tons/yr)
CO	114	46
HC	48	19
NO _x	170	68
SO _x	11	5
Particulates	449	180

TABLE 3.65 Estimated Emissions from Worker Commuter Vehicles during Construction of an Electrochemical Oxidation Facility at PBA

Criteria Pollutant	No. of Round Trips ^a	Emission Factor (g/km) ^b	One-Way Trip Distance (mi) ^c	Emission Rate (tons/yr)
HC	132,000	1.16	20	10.9
CO	132,000	11.38	20	106.6
NO _x	132,000	0.73	20	6.4
SO _x	132,000	0.12	20	1.1
PM ₁₀	132,000	0.055	20	0.5

^a Number of auto round trips to the construction site estimated on the basis of the average construction workforce and an assumption of 240 workdays per year.

^b Emission factors determined by using EPA modeling software MOBILE5b (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

Additional emissions would result from the use of paints and thinners, aerosols, and other area source emissions. These emissions are expected to be minor contributors to air pollution and were not included in current estimates.

Construction would generate solid waste primarily in the form of excavation spoils and building material debris. These latter wastes would include concrete forms, equipment and hardware containers and packaging, paint cans, waste metal sheeting, pipe and wire, and landscaping debris. Small amounts of liquid wastes, such as solvents, cleaning solutions, and paint wastes, also would be generated. Wastes would be collected and disposed of in compliance with U.S. Army, federal, state, and local requirements. All construction debris would be removed

from the site for disposal. Any batteries, used motor oils, and empty containers would be separated from the waste streams and recycled. Any wastes that are identified as hazardous would be stored and disposed of per RCRA requirements. Sanitary wastes are the only significant liquid effluents that would be generated during construction and would be managed on-site.

Table 3.66 gives the estimated total quantities of solid and liquid wastes generated from activities associated with facility construction. The waste generation quantities are based on historic data on land area size and the construction labor force.

3.3.5.3 Operations Phase

Information on the facility operations phase is presented in this section. Pre-operational testing is discussed first, followed by facility inputs and resource requirements, workforce requirements, and emissions and waste estimates.

TABLE 3.66 Estimated Total Wastes Generated during Construction of an Electrochemical Oxidation Facility at PBA

Waste Category	Quantity
Hazardous solids	90 yd ³
Hazardous liquids	39,000 gal
Nonhazardous solids	
Concrete ^a	190 yd ³
Steel ^b	33 tons
Other ^c	1,500 yd ³
Nonhazardous liquids	
Sanitary ^d	5,600,000 gal
Other	2,500,000 gal

^a Amount of concrete (nonhazardous solid) waste estimated by assuming that 0.65% of concrete usage is spoilage.

^b Amount of steel waste stream estimated as 0.5% of steel requirement on the basis of LLNL et al. (1997).

^c Amount of other stream estimated as eight times the concrete stream on the basis of LLNL et al. (1997).

^d Amount of sanitary waste estimated on the basis of the total construction workforce.

3.3.5.3.1 Preoperational Testing

A preoperational testing period assumed to last 14 months would begin following facility construction (PMACWA 2001b). Often referred to as systemization, this period would include preoperational checkout, training, and integrated systems operation under mock conditions with simulated munitions filled with surrogate chemicals (PMCD 1997). Systemization would be used to ensure that systems are operating as designed prior to pilot-scale operations. Therefore, it would appear that no hazardous emissions or effluents would be generated. The only types of effluents that would be generated are criteria pollutants (during testing of the steam boilers and the emergency diesel generator) and sanitary waste (from the systemization workforce). The amounts of criteria pollutants released and sanitary wastes generated would be negligible compared with those during construction and operations; thus, they were not considered in this analysis. It is projected that 300 contractor FTE-years would be needed for systemization.

3.3.5.3.2 Operations Inputs and Resource Requirements

At full-scale operation, destruction of the ACW containing nerve agent at PBA is projected to require 484 days for processing (376 for GB and 108 for VX). No ACW containing mustard agent are stored at PBA. Destruction operations at PBA are projected to require approximately 20.9 months at full-scale operation (see Table 3.67). This duration is based on a 12-hours-per-day, 6-days-per-week operation, 4 weeks per month, with a 3-week munitions changeover period. For comparison, incineration of the entire chemical agent inventory at PBA is projected to require 40 months (PMCD 1999b). Because baseline incineration at PBA would include destruction of mustard agent in TCs (which are not considered ACW), this option would require a longer period of operation.

Estimated annual utility consumption for facility operation, including electricity, fuel, and potable water usage, is presented in Table 3.68. The estimates in Table 3.69 are based on the assumption that the facility would consume potable water and produce sanitary waste 365 days

TABLE 3.67 Inventory and Estimated Processing Time for Electrochemical Oxidation of ACW Stored at PBA

Munition	Quantity	Agent	Processing Rate (No. of munitions/h)	Processing Time		Changeover (weeks)	Total (weeks)
				Hours	Weeks		
M55 rocket	90,231	GB	20	4,512	62.7	0.0	65.7
M55 rocket	19,582	VX	20	979	13.6	3.0	13.6
M23 land mine	9,378	VX	30	313	4.3	0.0	4.3
Total	119,191			5,803	80.6	3.0	83.6

^a Estimated by assuming 6-days-per-week operations and 12 hours per day.

TABLE 3.68 Estimated Utilities Consumed during Destruction of ACW at the Electrochemical Oxidation Unit at PBA

Utility	Average Daily Consumption	Peak-Day Consumption	Annual Consumption
Process water ^a	3,400 gal/d	191 gal/h	900,000 gal/yr
Potable water ^b	17,500 gal/d	180 gal/min	6,400,000 gal/yr ^c
Fire water ^b	NA ^d	3,000 gal/min	NA
Sanitary sewer ^b	20,650 gal/d	395 gal/min	7,500,000 gal/yr ^c
Natural gas ^a	174,000 scf/d	202,000 scf/d	48,000,000 ^c scf/yr ^e
Fuel oil	962 gal/d	406 gal/d	48,000 gal/yr ^f
Electricity	440 MWh	21.6 MW	121.3 GWh ^{c,g}

^a Estimated on the basis of the ratio of the munitions processing rate at PBA to that at BGAD and PCD.

^b Assumed to be similar to incineration because the number of operations and maintenance personnel and land area are unchanged from incineration.

^c Based on 365 days of operation per year.

^d NA = not applicable.

^e Based on 276 days of operations per year.

^f Estimated on the basis of 600 hours of emergency diesel generator operation per year.

^g Based on an average power rating of 80%.

Source: PMCD (1997).

per year. These are conservative assumptions that would identify an upper bound to natural gas, potable water, and sanitary waste treatment requirements. It was also assumed conservatively that fuel oil would be consumed only by an emergency diesel generator that would operate 600 hours per year. This analysis assumed that the amount of natural gas consumed for space heating would be negligible compared with that for natural gas consumed during the destruction process.

The destruction processes would consume raw materials. Table 3.69 gives the amounts of AgNO₃, HNO₃ (VX processing only), calcium nitrate (CaN₂O₆) (GB processing only), LOX, and NaOH that would be consumed during the processing of the two agents.

Tables 3.70 and 3.71 present transportation data estimated using the input material streams from Mitretek (2001d) for these raw materials for GB and VX agent processing, respectively. Liquid NaOH and solid AgNO₃ and Ca₂N₂O₆ would be transported in 55-gal (208-L) drums. LOX would be transported in bulk by tanker truck, and liquid HNO₃ would be transported in railcars.

TABLE 3.69 Estimated Raw Materials Consumed Annually during Normal Electrochemical Oxidation Operations at PBA

Agent Processed	Material	Material Consumed	
		Average Daily (lb/d)	Annual ^a (tons/yr)
GB, nominal 376-day campaign	AgNO ₃	1,100	150
	HNO ₃	0	0
	CaN ₂ O ₆	1,509	200
	Oxygen	13,000	1,800
	NaOH	1,900	262
VX, nominal 108-day campaign	AgNO ₃	660	35
	HNO ₃	136	7.3
	CaN ₂ O ₆	0	0
	Oxygen	14,000	750
	NaOH	2,000	100

^a Based on 276 days of operation per year for GB agent processing and a nominal campaign length of 108 days of operation for VX agent processing.

Source: Mitretek (2001d).

3.3.5.3.3 Operations Workforce

The electrochemical oxidation facility would be a government-owned, contractor-operated facility. Contractor employees would handle plant operations, while government employees would handle munitions, provide security, and staff other support activities. It is estimated that the average annual effort would be 720 FTEs (550 FTEs of contractor employee effort and 170 FTEs of government employee effort).

3.3.5.3.4 Operations Emissions and Waste Estimates

Wastes from the electrochemical oxidation process would include air emissions, solid wastes, and liquid wastes. The liquid effluents from the facility would be dilute, neutralized HNO₃, which would be accepted by a publicly owned treatment works (POTW) (PMACWA 2001b), and sanitary waste, which would be managed in an on-site treatment unit. All other liquids generated by the process and all liquid laboratory wastes would be reused in the process or destroyed internally by the electrochemical oxidation process. Destruction facility operations, including waste management, would comply with U.S. Army, federal, state, and local requirements. Any wastes identified as hazardous (such as possibly evaporator bottoms) would be stored and disposed of in compliance with RCRA requirements. Silver salts would be processed off-site for silver recovery after being treated to a 5X condition.

TABLE 3.70 Transportation Data for Raw Materials for Electrochemical Oxidation of ACW Containing GB Agent at PBA

Type of Data	Input Material No. 1	Input Material No. 2	Input Material No. 3	Input Material No. 4	Input Material No. 5
Transported materials					
Type/chemical	NaOH	AgNO ₃	CaN ₂ O ₆	LOX	HNO ₃
Physical form	Liquid	Solid	Solid	Liquid	Liquid
Chemical composition/ temperature, pressure	NaOH/ ambient	AgNO ₃ / ambient	CaN ₂ O ₆ / ambient	O ₂ / -297°F, 1 atm	HNO ₃ / ambient
Packaging					
Type	55-gal drum	55-gal drum	55-gal drum	4,000-gal tanker truck	11,000-gal railcar
Container volume (ft ³)	7.35	7.35	7.35	535	1,470
Certified by	DOT	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies	Varies
Container weight (lb)	50	50	50	NA ^a	NA
Material weight (lb) ^b	700	2,000	1,090	38,080	107,000
Chemical content (wt%)	50% NaOH	100% AgNO ₃	100% CaN ₂ O ₆	100% O ₂	50% HNO ₃
Shipments					
Average weight (tons/yr) ^c	262	153	209	1,829	0
Average volume (ft ³ /yr)	5,564	1,127	2,838	51,371	0
Packages/yr	757	154	387	97	0
Packages/shipment	48	20	36	1	1
Shipments/yr	16	8	11	97	0
Form of transport/routing					
Form of transportation	Truck	Truck	Truck	Truck	Railcar
Specific gravity (77°F)	NA	4.35	2.36	1.14	1.30

^a NA = not applicable.

^b Based on Mitretek (2001a).

^c Annual estimates based on a campaign length of 276 days.

TABLE 3.71 Transportation Data for Raw Materials for Electrochemical Oxidation of ACW Containing VX Agent at PBA

Type of Data	Input Material No. 1	Input Material No. 2	Input Material No. 3	Input Material No. 4	Input Material No. 5
Transported materials					
Type/chemical	NaOH	AgNO ₃	CaN ₂ O ₆	LOX	HNO ₃
Physical form	Liquid	Solid	Solid	Liquid	Liquid
Chemical composition/ temperature, pressure	NaOH/ ambient	AgNO ₃ / ambient	CaN ₂ O ₆ / ambient	O ₂ /-297°F, 1 atm	HNO ₃ / ambient
Packaging					
Type	55-gal drum	55-gal drum	55-gal drum	4,000-gal tanker truck	11,000-gal railcar
Container volume (ft ³)	7.35	7.35	7.35	535	1,470
Certified by	DOT	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies	Varies
Container weight (lb)	50	50	50	NA ^a	NA
Material weight (lb) ^b	700	2,000	1,090	38,080	107,000
Chemical content (wt%)	50% NaOH	100% AgNO ₃	100% CaN ₂ O ₆	100% O ₂	50% HNO ₃
Shipments					
Average weight (tons/yr) ^c	108	35	0	745	7.3
Average volume (ft ³ /yr)	2,293	261	0	20,913	180
Packages/yr	312	36	0	40	1
Packages/shipment	48	20	36	1	1
Shipments/yr	7	2	0	40	1
Form of transport/routing					
Form of transportation	Truck	Truck	Truck	Truck	Railcar
Specific gravity (77°F)	NA	4.35	2.36	1.14	1.30

^a NA = not applicable.

^b Based on Mitretek (2001d).

^c Annual estimates based on a campaign length of 108 days.

Solid effluents from the process would include caustic scrubber waste, spent anolyte-catholyte waste from agent treatment, spent anolyte-catholyte waste from energetics treatment, and primarily metals that have been treated to a 5X condition.

Gas Effluents. Off-gas from the MPT and BRT (mostly steam and HNO₃) would be condensed in the SILVER II process for recovery or disposal. All process off-gas would be mixed with air and treated with a catalytic oxidation system.

In the facility ventilation system, these gases would pass through carbon filters prior to release to the atmosphere. This analysis assumes an off-gas treatment system consisting of six activated carbon beds and two HEPA filtration units in series. Handling and disposal of process residue in accordance with the provisions of RCRA are expected to result in little potential for significant adverse impacts on air quality. Emissions from vehicles and combustion of natural gas and LPG are regulated by the EPA and the State of Arkansas and are expected to result in little potential for significant adverse impacts on air quality. Dust emissions would be controlled during operations as well.

The electrochemical oxidation process would be required to meet RCRA and any other applicable environmental requirements and would operate under permit. The process would be required to destroy agent and energetics to a DRE of 99.9999% and to meet agent emission limits as established by the ASG. Other emissions, including metals, would be regulated in accordance with the RCRA permit. The operation would also be required to meet air pollution control requirements for conventional pollutants, such as CO, SO₃, and opacity.

All ventilation air would be processed through carbon filtration before being released to the atmosphere. Facility effluent release points would include gaseous releases to the environment. Table 3.72 summarizes the facility effluent air release points.

Table 3.73 summarizes the estimated criteria pollutants emission rates during operations; these were estimated on the basis of the annual fuel consumption rates shown in Table 3.68. Daily emissions can be estimated from the hourly rates, assuming 12 operating hours per day.

Small amounts of organic and metallic compounds would be emitted from the combustion of natural gas during normal boiler operation and from the combustion of fuel oil during emergency diesel generator operation. Tables 3.74 and 3.75 summarize the TAP emission rates for the burning of natural gas in the boiler and fuel oil in the emergency generator, respectively. Many of these emissions are also HAPs, as defined in Section 112 of the CAA, Title III. The emission rates of these TAPs were estimated on the basis of the annual consumption rates shown in Table 3.68 and with FIRE 6.22 emission factors for large wall-fired boilers with greater than 1000 MMBtu/h of heat input and for reciprocating diesel engines (EPA 2000a). Daily emissions can be estimated from hourly rates, assuming 12 operating hours per day.

TABLE 3.72 Stack Parameters for Electrochemical Oxidation at PBA^a

Installation or Emission Point	Physical		Stack Exit Gas Flow (acfm)	Stack Exit		Stack Location ^b
	Stack Height (ft)	Stack Exit Diameter (ft)		Gas Velocity (ft/sec)	Stack Exit Gas Temp (°F)	
Process steam boiler I ^{b,c}	70	1,555	60	60	325	Near southwest corner of PUB
Process steam boiler II ^{b,c}	70	1,555	60	60	325	Near southwest corner of PUB
Process steam boiler III ^{b,c}	70	1,555	60	60	325	Near southwest corner of PUB
Diesel generator exhaust I ^b	47	6,765	323	323	925	Near northwest corner of PMB
Diesel generator exhaust II ^b	47	6,765	323	323	925	Near northwest corner of PMB
Filter farm stack ^{d,e}	120	118,000	60	60	77	Center of structure

^a Abbreviations: PUB = Process Utilities Building, PMB = Personnel and Maintenance Building, MDB = Munitions Demilitarization Building.

^b Information on the stack characteristics for electrochemical oxidation was unavailable; characteristics similar to neutralization/biotreatment were assumed (Parsons/Allied Signal 1999).

^c Stack exit gas flow for the process steam boiler taken from Parsons/Allied Signal 1999 and modified to take into account the annual average natural gas consumption rate of 174,000 scfd for electrochemical oxidation.

^d Stack characteristics similar to those at Newport, Indiana were assumed (PMCD 1999a).

^e Stack exit gas flow and diameter revised to account for 15% increase in the MDB proposed by the technology provider (AEA/CH2MHILL 2000).

The electrochemical oxidation facility at PBA would be equipped with building ventilation systems that would discharge, to the atmosphere, indoor air from the MDB process area, the Laboratory Building, and the Personnel and Maintenance Building through the filter farm stack. Of the three ventilation systems, only the indoor air from the MDB process area would be potentially exposed to chemical agents during operations.

To estimate the maximum potential emissions of chemical agents, only the MDB process area was considered to be a significant potential source. The filter systems would be designed to remove chemical agents from the ventilation air streams to levels below the allowable stack concentrations that have been recommended by the U.S. Department of Health and Human Services, Centers for Disease Control (53 *Federal Register* 8504 – 8507, March 15, 1988). Also, a negative pressure would be maintained at all times in the MDB after the initiation of hot operations to inhibit the release of chemical agents. Table 3.76 gives the potential chemical agent

TABLE 3.73 Estimated Hourly and Annual Emission Rates of Criteria Pollutants during Normal Operations of an Electrochemical Oxidation Facility at PBA

Criteria Pollutant	Process Steam Boiler ^a		Diesel Generator Exhaust ^b	
	lb/h	tons/yr	lb/h	tons/yr
CO	1.2	2.02	10.4	3.12
NO _x	2.0	3.36	48.4	14.50
SO _x	<0.01	0.01	3.2	0.95
PM ₁₀	0.1	0.18	3.4	1.02
HC	0.2	0.13	4.0	1.18

^a Estimated on the basis of the utility requirements listed in Table 3.67.

^b Based on 600 hours of operations per year.

emission rates, assuming that the chemical agent concentrations in the air discharged would be at 20% of the recommended allowable stack concentrations (i.e., the level of quantification of the ventilation exhaust chemical agent monitors.). These emission calculations were based on actual operations time (12 hours per day, 276 days per year), since the only time there is a source of agent is during operations.

Tables 3.77 and 3.78 give the estimated TAP emission rates (lb/h) during operation from the filter farm stack for GB and VX agent processing, respectively. Daily emission rates can be obtained by multiplying the hourly rates by 12. Annual emission rates can be estimated from the daily rates, assuming 276 operating days for GB agent processing and 108 operating days for VX agent processing.

Emissions from operations workers commuter vehicles were estimated on the basis of the assumption that each of the operations workers (720) would drive a round trip consisting of two 20-mi (32-km) one-way trips per day. Table 3.79 gives the annual emission estimates due to the increased traffic.

Liquid Wastes. Liquid wastes would include dilute HNO₃ and sanitary wastes. The final PMACWA technology evaluation for electrochemical oxidation (PMACWA 2001b) noted that the technology provider proposes to route certain effluents to either a POTW or an on-site wastewater treatment plan, although the availability and acceptability of these disposal methods was not identified. These effluents would include a treated effluent from a packaged batch fluoride treatment system, cooling tower blowdown, water softener, boiler blowdown, and sanitary wastewater.

TABLE 3.74 Estimated Hourly and Annual TAP Emission Rates during Normal Boiler Operations for Electrochemical Oxidation at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
2-Methylnaphthalene	3.5E-07	1.2E-03
3-Methylchloranthrene	2.6E-08	8.6E-05
Acenaphthene	2.6E-08	8.6E-05
Acenaphthylene	2.6E-08	8.6E-05
Anthracene	3.5E-08	1.2E-04
Arsenic	2.9E-06	9.6E-03
Barium	6.4E-05	2.1E-01
Benz(a)anthracene	2.6E-08	8.6E-05
Benzene	3.0E-05	1.0E-01
Benzo(a)pyrene	1.7E-08	5.8E-05
Benzo(b)fluoranthene	2.6E-08	8.6E-05
Benzo(g,h,i)perylene	1.7E-08	5.8E-05
Benzo(k)fluoranthene	2.6E-08	8.6E-05
Beryllium	1.7E-07	5.8E-04
Butane	3.0E-02	1.0E+02
Cadmium	1.6E-05	5.3E-02
Chromium	2.0E-05	6.7E-02
Chrysene	2.6E-08	8.6E-05
Cobalt	1.2E-06	4.0E-03
Copper	1.2E-05	4.1E-02
Dibenzo(a,h)anthracene	1.7E-08	5.8E-05
Dichlorobenzene	1.7E-05	5.8E-02
Dimethylbenz(a)anthracene	2.3E-07	7.7E-04
Ethane	4.5E-02	1.5E+02
Fluoranthene	4.4E-08	1.4E-04
Fluorene	4.1E-08	1.3E-04
Formaldehyde	1.1E-03	3.6E+00
Hexane(n)	2.6E-02	8.6E+01
Indeno(1,2,3-cd)pyrene	2.6E-08	8.6E-05
Lead	7.3E-06	2.4E-02
Manganese	5.5E-06	1.8E-02
Mercury	3.8E-06	1.2E-02
Molybdenum	1.6E-05	5.3E-02
Naphthalene	8.8E-06	2.9E-02
Nickel	3.0E-05	1.0E-01
Pentane(n)	3.8E-02	1.2E+02
Phenanthrene	2.5E-07	8.2E-04
Propane	2.3E-02	7.7E+01
Pyrene	7.3E-08	2.4E-04
Selenium	3.5E-07	1.2E-03
Toluene	4.9E-05	1.6E-01
Vanadium	3.3E-05	1.1E-01

^a Emission factors from EPA (2000a).

TABLE 3.75 Estimated Hourly and Annual TAP Emission Rates during Emergency Diesel Generator Operations for Electrochemical Oxidation at PBA^a

Compound	Hourly Emission (lb/h)	Annual Emission (lb/yr)
Acenaphthene	3.1E-07	1.9E-04
Acenaphthylene	1.1E-06	6.7E-04
Acetaldehyde	1.7E-04	1.0E-01
Acrolein	2.0E-05	1.2E-02
Aldehydes	1.5E-02	9.2E+00
Anthracene	4.1E-07	2.5E-04
Benzene	2.0E-04	1.2E-01
Benzo(a)anthracene	3.7E-07	2.2E-04
Benzo(a)pyrene	4.1E-08	2.5E-05
Benzo(b)fluoranthene	2.2E-08	1.3E-05
Benzo(g,h,i)perylene	1.1E-07	6.4E-05
Benzo(k)fluoranthene	3.4E-08	2.0E-05
1,3-Butadiene	8.6E-06	5.1E-03
Chrysene	7.8E-08	4.6E-05
Dibenzo(a,h) anthracene	1.3E-07	7.7E-05
Fluoranthene	1.7E-06	1.0E-03
Fluorene	6.4E-06	3.8E-03
Formaldehyde	2.6E-04	1.6E-01
Indeno(1,2,3-cd)pyrene	8.2E-08	4.9E-05
Isomers of xylene	6.3E-05	3.7E-02
Mercury	6.6E-08	4.0E-05
Naphthalene	1.9E-05	1.1E-02
Phenanthrene	6.5E-06	3.9E-03
Polycyclic aromatic hydrocarbons (PAHs)	3.7E-05	2.2E-02
Propylene	5.7E-04	3.4E-01
Pyrene	1.0E-06	6.3E-04

^a Emission factors from EPA (2000a).

TABLE 3.76 Estimated Maximum Hourly and Annual Agent Emission Rates from the Filter Farm Stack for Electrochemical Oxidation at PBA

Chemical Agent	Emission Factor (mg/m ³) ^a	Stack Exit Gas Flow (acfm) ^b	Hours of Operation per Year ^c	Stack Emission Rate	
				(lb/h)	(tons/yr) ^d
GB	0.00006	118,000	3,312	2.7E-05	4.4E-05
VX	0.00006	118,000	1,292	2.7E-05	1.7E-05

^a Based on the monitor level of quantification, which is 20% of the allowable stack concentration recommended for each chemical agent in 53 CFR 8504 – 8507.

^b Filter farm stack exit flow based on estimated building ventilation for the MDB.

^c Hours of operations based on the assumption that each pilot plant operates at the design throughputs specified in CBDCOM (1997).

^d Estimate based on number of hours of operation per year.

Solid Wastes. The major process solid residuals expected from the electrochemical oxidation operation include the following:

- Scrap metal, dunnage, spent carbon garnet, and firing tubes would be decontaminated to a 5X condition primarily in the MPT or BRT;
- Decontaminated solid residues from the anolyte and catholyte circuits of the agent SILVER II process;
- Decontaminated solid residues from the anolyte and catholyte circuits of the energetics SILVER II process; and
- Wastes from the caustic scrubber circuits used in post-treatment.

These solid wastes would be transported to an approved off-site hazardous waste treatment, storage, and disposal facility for additional treatment and/or ultimate disposal. Table 3.80 shows the composition of the solid caustic scrubber waste and the rate of generation per processing day for processing of ACWs containing GB and VX agent. Tables 3.81 through 3.84 show the corresponding information for the processing of agent treatment spent anolyte-catholyte waste, energetics treatment spent anolyte-catholyte waste, 5X solids, and neutralized HNO₃, respectively.

TABLE 3.77 Estimated TAP Emission Rates from the Filter Farm Stack during Electrochemical Oxidation of ACW Containing GB Agent at PBA

Compound	Emission Rate (lb/h)	Compound	Emission Rate (lb/h)
1,5-Pentanediol, dinitrate	4.6E-11	Hexadecane	1.0E-11
1-Butanol, 3-methyl-, nitrate	2.1E-10	Hexanenitrile	5.5E-12
1-Hexanol, 2-ethyl-	2.6E-12	Isopropyl nitrate	1.3E-09
2-heptanone	4.7E-12	Naphthalene	2.4E-10
2-hexanone	4.3E-11	Nitric acid esters	4.9E-11
2-octanone	7.7E-12	Nitric acid, butyl ester	2.3E-10
2-Pentanol, nitrate	2.9E-10	Nitric acid, decyl ester	1.9E-11
4-Methyl-2-pentanone	1.6E-12	Nitric acid, ethyl ester	1.3E-10
4-octene, (e)-	7.1E-13	Nitric acid, hexyl ester	1.3E-10
Acetamide, N,N-dimethyl-	1.6E-11	Nitric acid, nonyl ester	4.2E-11
Acetic acid	2.1E-11	Nitric acid, pentyl ester	1.3E-10
Acetone	1.2E-13	Nitric acid, propyl ester	1.4E-10
Benzene	1.6E-11	Nonanal	6.7E-12
Bis(2-ethylhexyl)phthalate	7.2E-12	Nonanenitrile	1.2E-11
Carbon disulfide	6.1E-10	Octanal	1.2E-11
Cyclohexane, 1,2,3-trimethyl-	2.5E-12	Octanenitrile	1.4E-11
Decane	4.1E-11	Pentadecane	2.0E-11
Decanenitrile	7.0E-12	Tetradecane	6.6E-11
Dodecane	5.6E-11	Toluene	4.3E-12
Ethylbenzene	1.1E-12	Tridecane	5.9E-11
Heptanal	1.0E-11	Undecane	5.0E-11
Heptanenitrile	6.1E-12	Xylenes	5.7E-12

These waste streams would be shipped from the on-site facility to off-site locations. Tables 3.85 and 3.86 provide transportation data for annual shipment of these waste streams for GB and VX agent processing on the basis of 276 days of operations for ACWs containing GB agent, the assumed number of days of processing per year, and a campaign length of 108 days for ACWs containing VX agent.

3.3.5.4 Activities

The PMACWA described activities for installation of the electrochemical oxidation system (PMACWA 2001b). The major phases of the project are shown in Table 3.87.

TABLE 3.78 Estimated TAP Emission Rates from the Filter Farm Stack during Electrochemical Oxidation of ACW Containing VX Agent at PBA

Compound	Emission Rate (lb/h)	Compound	Emission Rate (lb/h)
1,5-Pentanediol, dinitrate	3.5E-11	Hexanenitrile	4.2E-12
1-Butanol, 3-methyl-, nitrate	1.6E-10	Isopropyl nitrate	9.8E-10
1-Hexanol, 2-ethyl-	2.0E-12	Naphthalene	2.1E-10
2-heptanone	3.6E-12	Nitric acid esters	3.7E-11
2-hexanone	3.3E-11	Nitric acid, butyl ester	1.7E-10
2-octanone	5.9E-12	Nitric acid, decyl ester	1.5E-11
2-Pentanol, nitrate	2.2E-10	Nitric acid, ethyl ester	9.7E-11
4-Methyl-2-pentanone	1.4E-12	Nitric acid, hexyl ester	9.6E-11
4-octene, (e)-	6.2E-13	Nitric acid, nonyl ester	3.2E-11
Acetamide, N,N-dimethyl-	1.2E-11	Nitric acid, pentyl ester	1.0E-10
Acetic acid	1.8E-11	Nitric acid, propyl ester	1.0E-10
Acetone	1.0E-13	Nonanal	5.8E-12
Benzene	1.3E-11	Nonanenitrile	9.1E-12
Bis(2-ethylhexyl)phthalate	5.5E-12	Octanal	9.7E-12
Carbon disulfide	4.6E-10	Octanenitrile	1.0E-11
Cyclohexane, 1,2,3-trimethyl-	2.2E-12	Pentadecane	1.5E-11
Decane	3.1E-11	Tetradecane	5.0E-11
Decanenitrile	5.3E-12	Toluene	3.3E-12
Dodecane	4.3E-11	Tridecane	5.2E-11
Ethylbenzene	8.5E-13	Undecane	3.8E-11
Heptanal	7.8E-12	Xylenes	4.5E-12
Heptanenitrile	4.6E-12	MPA ^a	6.2E-17
Hexadecane	2.0E-11		

^a MPA = methylphosphonic acid.

3.3.5.5 Uncertainties

As indicated earlier, each of the individual technologies that forms the electrochemical oxidation system has either been previously proven to be a successful technology or has been demonstrated by the PMACWA to be an acceptable technology for application at PBA. However, demonstration testing focused on individual technologies and sometimes used less than full-scale units. In addition, although EDSs were conducted to evaluate the long-term adequacy of individual technologies, it was not possible to evaluate the long-term viability and performance of the entire, integrated treatment system. Thus, the primary uncertainty associated with electrochemical oxidation is that the entire, integrated treatment system, with all its component units, has not been assembled and tested. The pilot program, if implemented for this technology system, would be designed to evaluate overall operability and long-term performance.

TABLE 3.79 Estimated Emissions from Worker Commuter Vehicles for Electrochemical Oxidation at PBA

Criteria Pollutant	No. of Auto Round Trips ^a	Emission Factor (g/km) ^b	One-Way Distance (mi) ^c	Emission Rate (tons/yr)
HC	199,000	1.16	20	16.4
CO	199,000	11.38	20	160.5
NO _x	199,000	0.73	20	10.3
SO _x	199,000	0.12	20	1.7
PM ₁₀	199,000	0.055	20	0.78

^a Number of auto round trips to the operation site estimated on the basis of the total operating workforce and an assumption of 276 days of operations per year.

^b Emission factors determined by using EPA modeling software MOBILE5B (EPA 2000c) for HC, CO, and NO_x and PART5 (EPA 2000b) for PM₁₀.

^c One-way trip distance based on DOE (1997).

3.3.6 DISMANTLING AND CLOSURE

The legislation that established the ACWA (Public Law 104-208) instructed DOD to demonstrate alternatives to the baseline incineration process for the demilitarization of ACW. Subsequent legislation specified the continued management of the development and testing of technologies for the destruction of lethal chemical munitions. The status and disposition of ACWA pilot test facilities were not addressed in the legislation. An ACWA pilot facility could be (1) closed and decommissioned (i.e., operations terminated and the site secured) after the conclusion of testing; (2) converted to an operational chemical weapon destruction facility (this option assumes that there would be chemical weapons remaining at the site); or (3) assigned functions other than the demilitarization of weapons in the chemical weapons stockpile (within the constraints imposed by the National Defense Authorization Act for Fiscal Year 2000). The latter two options, however, are beyond the scope of the ACWA EIS and this TRD. The future use of the current chemical weapons storage and related facilities is also beyond the scope of the ACWA EIS and this TRD. Only closure and decommissioning of an ACWA pilot facility can be addressed in the ACWA EIS and this TRD.

The closure and decommissioning of an ACWA pilot facility would require compliance with the provisions of any permits issued by regulatory agencies for the construction and operation of the facility. This would include compliance with RCRA requirements for the closure of a hazardous waste treatment, storage, or disposal facility. The PMACWA and other parties

TABLE 3.80 Estimated Generation Rates of Solid Caustic Scrubber Waste from Electrochemical Oxidation at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound ^a	Generation Rate (lb/d)	
	GB	VX
(Carbethoxyethylidene) triphenylphos	9.0E-06	7.8E-06
1-Butanamine, N-butyl-N-nitroso-	3.4E-04	0.0E+00
2,4-Dinitrotoluene	4.1E-06	3.6E-06
2-Butenoic acid, 4-nitrophenyl ester	0.0E+00	2.4E-02
2-Nitrophenol	3.4E-04	6.8E-05
2-Propanamine, N-(1-methylethyl)-N-nitro	1.8E-03	0.0E+00
2-Pyrrolidinone, 1-methyl-	7.1E-05	5.4E-05
3-Buten-2-one, 3-methyl-	0.0E+00	3.4E-04
Acetaldehyde	3.4E-04	0.0E+00
Acetone	0.0E+00	9.5E-03
Aluminum	2.3E-03	1.7E-03
Calcium	5.7E-01	4.3E-01
Chloride	TBD ^b	TBD
Chromium	7.2E-04	5.6E-04
Copper	6.2E-05	5.4E-05
Cyclohexanone	3.2E-04	2.4E-04
DIPA	2.7E-04	0.0E+00
EMPA	0.0E+00	1.5E-03
Fluoride	0.0E+00	6.3E-01
Formamide, n,n-dibutyl-	4.0E-04	0.0E+00
IMPA	1.5E+01	0.0E+00
Iron	7.9E-04	6.9E-04
Magnesium	6.8E-01	5.1E-01
Mercury	6.6E-05	3.3E-05
Methyl nitrate	1.5E-04	1.1E-04
Molybdenum	4.8E-05	4.2E-05
MPA	0.0E+00	1.3E-03
Nickel	9.1E-04	7.9E-04
Nitrate-N	1.4E+02	1.4E+02
Nitric acid, 1-methylethyl ester	2.2E-01	1.9E-02
Nitric acid, butyl ester	1.5E-03	0.0E+00
Nitric acid, propyl ester	9.7E-04	0.0E+00
Nitrite-N	1.1E+02	1.3E+02
Nitrobenzene	0.0E+00	0.0E+00
Nitropropane isomer	3.7E-03	0.0E+00
N-Nitrosodimethylamine	6.7E-04	0.0E+00
Phenol	3.0E-05	0.0E+00
Phenol, 2-fluoro-4-nitro- + unknown coelution	4.0E-04	0.0E+00
Phosphorus	4.3E-03	6.1E-02

TABLE 3.80 (Cont.)

Compound ^a	Generation Rate (lb/d)	
	GB	VX
Propane, 2-nitro-	1.0E-03	0.0E+00
Silver	1.7E-03	2.7E-05
Sodium	6.0E+02	6.0E+02
Sulfate	6.8E-02	9.0E-01
Tributylamine	4.4E-02	0.0E+00
Undecanoic acid	1.4E-06	1.2E-06
Unknown alcohol	4.7E-02	1.0E-01
Unknown alkane	2.8E-03	5.9E-03
Unknown alkene	2.8E-02	4.6E-02
Unknown amine	4.4E-03	0.0E+00
Unknown chlorinated hydrocarbon	0.0E+00	1.8E-06
Unknown ketone	6.0E-03	1.8E-02
Unknown organic acid	3.7E-02	1.7E-03
Unknown PAH	1.1E-05	9.6E-06
Unknown substituted alkane	2.4E-06	3.2E-03
Unknown substituted alkene	1.6E-04	4.8E-03
Urea, tetrabutyl-	2.0E-04	0.0E+00
Water	5.1E+00	1.0E+01
Total (lb/d)	8.7E+02	8.8E+02
Operating days	376	108

^a Abbreviations: DIPA = diisopropanolamine, EMPA = ethyl methyl phosphonic acid, IMPA = isopropyl methyl phosphonic acid.

^b TBD = to be determined.

TABLE 3.81 Estimated Generation Rates of Solid Spent Anolyte-Catholyte Waste from Agent Treatment during Electrochemical Oxidation at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB	VX
1-Butanamine, N-butyl-N-nitroso-	8.8E-03	0.0E+00
2-Butenal, 3-methyl-	1.5E-03	0.0E+00
2-Propanamine, N-(1-methylethyl)-N-nitro	0.0E+00	1.6E-01
2-Propanamine, n-ethyl-n-nitroso-	0.0E+00	5.8E-03
2-Propanamine, N-methyl-N-nitroso-	0.0E+00	3.8E-03
3-Hydroxy-3-methyl-2-butanone	4.8E-03	0.0E+00
3-Methyl-3-chloro-1-butene	1.5E-03	0.0E+00
Aluminum	2.8E+00	0.0E+00
Arsenic	2.0E-03	0.0E+00
Barium	7.2E-03	0.0E+00
Chromium	0.0E+00	1.9E+01
Cobalt	4.3E-01	9.2E-01
Copper	1.5E-01	1.2E-01
Diethylamine, 1,1'-dimethyl-n-nitro-	0.0E+00	2.4E-02
Diethylphthalate	5.6E-04	0.0E+00
Diisopropylamine	0.0E+00	4.8E+00
DIPA	0.0E+00	9.7E-02
Fluoride	4.6E+01	0.0E+00
Formamide, n,n-dibutyl-	1.5E-03	0.0E+00
Glycerol tricaprylate	0.0E+00	6.8E-03
Hexavalent chromium	3.6E+00	1.2E+01
Iron	1.5E+01	8.3E+00
Magnesium	3.9E-02	0.0E+00
Manganese	3.0E-01	2.8E-01
Mercury	1.6E-04	8.3E-05
MPA	0.0E+00	3.8E+02
Nickel	1.0E+01	4.0E+01
Pentachlorophenol	0.0E+00	1.8E-03
Phosphorus	8.1E+01	2.8E+02
Selenium	5.8E-03	1.3E-02
Silver	5.5E+02	4.3E+03
Sodium	7.6E+00	0.0E+00
Sulfate	8.7E+02	8.9E+02
Unknown hydrocarbon	1.9E-03	0.0E+00
Urea, tetrabutyl-	3.3E-03	0.0E+00
Vanadium	4.2E-02	1.2E-01
Vinyl chloride	5.4E-03	0.0E+00
Water	7.5E+00	1.6E+01

TABLE 3.81 (Cont.)

Compound	Generation Rate (lb/d)	
	GB	VX
Zinc	1.0E-01	3.9E-02
Total (lb/d)	1.6E+03	6.0E+03
Operating days	376	108

involved in the closure and decommissioning of an ACWA pilot facility also would have to meet U.S. Army and DOD requirements for managing and disposing of facilities involved in the handling of chemical warfare materials.

The closure and decommissioning of an ACWA facility would likely be similar to the closure of baseline incineration facilities (such as JACADS and TOCDF) and destruction facilities using alternative technologies (located at APG in Maryland and NCD in Indiana). The JACADS site closure plan (Washington 2000) and the APG and NCD RCRA permit applications (APG 1997, NCD 1998a) contain general concepts for facility closure and decommissioning.

On the basis of the general requirements for a treatment, storage, or disposal facility under RCRA, U.S. Army, and DOD policies and regulations, and concepts for the decommissioning of chemical destruction facilities, the following steps would likely be involved in the closure and decommissioning of an ACWA pilot facility:

- Removal of all hazardous wastes from the site;
- Decontamination of the structures and equipment (to include piping and tankage) to allow safe handling;
- Removal of all or part of the remaining equipment;
- Demolition of all or part of the facility;
- Removal or abandonment of all or part of the supporting infrastructure; and
- Grading and revegetation, as needed, of the areas after removal of structures and infrastructure.

TABLE 3.82 Estimated Generation Rates of Solid Spent Anolyte-Catholyte Waste from Energetics Treatment during Electrochemical Oxidation at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB	VX
1,3,5-Trinitrobenzene	4.1E+00	3.6E+00
1,4-Dimethyl-4,5,7,8-tetrahydroimidazo-[7.3E-01	6.4E-01
1-Propanone, 1-phenyl-, phenylhydrazone	3.4E-05	2.9E-05
2,4,6-Trinitrotoluene	2.8E+00	2.4E+00
2,4-Dinitrophenol	2.5E-05	2.1E-05
2,4-Dinitrotoluene	2.7E-02	2.0E-02
Aluminum	3.0E-02	2.2E-02
Barium	4.8E-02	3.6E-02
Benzenamine, 2,4,6-trinitro-	3.4E-03	3.0E-03
Benzoic acid, 3,4,5-trimethoxy-2-nitro-,	9.0E-05	7.8E-05
Bicyclo[4.3.0]nona-3,7-diene, trans-	1.6E-03	1.4E-03
Bis(2-ethylhexyl)phthalate	8.7E-04	7.0E-04
Calcium	8.0E-01	6.0E-01
Chromium	3.3E-02	2.6E-02
Copper	8.0E-01	6.1E-01
Cyclohexane, 1-methyl-2-propyl-	2.7E-03	2.1E-03
Hexavalent chromium	7.8E-04	6.7E-04
Iron	2.5E+00	1.9E+00
Lead	2.4E+00	1.8E+00
Manganese	9.0E-03	6.9E-03
Nickel	2.3E-02	1.8E-02
Pyridine, 1-acetyl-1,2,3,4-tetrahydro-5-	1.6E-03	1.4E-03
Salicylaldehyde, azine	2.3E-05	2.0E-05
Silver	5.0E+01	4.3E+01
Tetryl	3.9E+00	3.3E+00
Unknown cyclic alkane	2.0E-03	1.5E-03
Unknown hydrocarbon	9.8E-04	7.4E-04
Water	2.3E+00	1.7E+00
Zinc	1.3E-02	1.1E-02
Total (lb/d)	7.0E+01	6.0E+01
Operating days	376	108

TABLE 3.83 Estimated Generation Rates of 5X Solids from Electrochemical Oxidation at PBA To Be Sent Off-Site for Land Disposal or Recycling

Compound	Generation Rate (lb/d)	
	GB	VX
Steel body and other iron	5.6E+03	6.3E+03
Aluminum	6.0E+03	4.5E+03
Glass fiber	9.3E+02	7.0E+02
Total	1.3E+04	1.2E+04
Operating days	376	108

These actions would generate wastes similar to those created during the operation of the facility. Wastes would include decontamination solutions consisting of water or caustic solutions containing agent and energetic by-products (similar to agent and energetic hydrolysates), contaminated and noncontaminated debris (such as metals, wood, and concrete that are similar to dunnage and maintenance wastes), protective clothing, wastes from administrative and maintenance areas, petroleum products, and industrial chemicals. To the degree feasible, these materials would be processed through the ACWA facility in the same manner as like materials during pilot testing. Once the facility is rendered nonoperational, these materials would be collected, containerized, and treated or disposed of in accordance with environmental regulations.

Equipment removed from the facility would be decontaminated and reused or recycled when possible. Structures would be decontaminated to the degree required by U.S. Army and DOD regulations to allow their reuse or demolition. Demolition debris would be disposed of in accordance with environmental, U.S. Army, and DOD regulations.

Removal, demolition, grading, and revegetation operations would be similar to the activities during construction. Disassembly of the facility would involve equipment and actions very much like those used to prepare the site and to erect the facility. Materials used in the construction of the facility would be conveyed out of the area in a manner similar to that used to bring them into the area; for example, concrete and steel would be trucked away from the site. The area required to support removal and demolition operations would not exceed that needed for material staging and facility construction.

TABLE 3.84 Estimated Generation Rates of Liquid Neutralized HNO₃ from Electrochemical Oxidation at PBA To Be Sent Off-Site for Disposal or Treatment

Compound	Generation Rate (lb/d)	
	GB	VX
2,3,3-Trimethyl-1-hexene	5.2E-04	4.5E-04
2,6-Dinitrotoluene	0.0E+00	1.5E-03
Benzene, 1,4-dinitro-	6.0E-04	5.2E-04
Benzene, 2-methyl-1,3,5-trinitro-	0.0E+00	3.6E-03
Benzofurazan, 4-nitro-	1.6E-03	1.4E-03
Bis(2-ethylhexyl)phthalate	9.5E-04	7.2E-04
Chromium	2.3E-04	2.0E-04
Copper	6.5E-04	4.9E-04
Decanoic acid	1.5E-03	1.2E-03
Heptanoic acid	3.3E-03	2.5E-03
Iron	7.6E-03	6.5E-03
Lead	3.5E-03	3.0E-03
Ng	3.3E-03	2.5E-03
Nitrate-N	5.9E-01	4.8E+00
Nitrobenzene	3.3E-03	0.0E+00
Nitrocellulose	2.8E-03	2.1E-03
Nonanoic acid	2.4E-03	1.8E-03
Octanenitrile	8.3E-04	6.3E-04
Octanoic acid	3.6E-03	2.7E-03
Pentanal, 2-methyl-	1.7E-03	1.4E-03
Silver	6.8E-02	5.9E-02
Sodium	2.2E-01	1.8E+00
Tetryl	1.1E+01	9.6E+00
Unknown hydrocarbon	2.9E-03	2.3E-03
Water	6.0E+01	5.2E+01
Zinc	9.2E-04	8.0E-04
Total (lb/d)	7.2E+01	6.9E+01
Operating days	376	108

TABLE 3.85 Transportation Data for Solid and Liquid Wastes from Electrochemical Oxidation during Processing of ACW Containing GB Agent at PBA

Type of Data	Output Material No. 1	Output Material No. 2	Output Material No. 3	Output Material No. 4	Output Material No. 5
Transported Materials					
Type/chemical	Scrubber waste	Spent anolyte-catholyte waste from agent treatment	Spent anolyte-catholyte waste from energetics treatment	5X solids – waste ^a	Neutralized HNO ₃ waste
Physical form	Solid	Solid	Solid	Solid	Liquid
Chemical composition/temperature, pressure	See Table 3.80	See Table 3.81	See Table 3.82	See Table 3.83	See Table 3.84
Packaging					
Type	55-gal drum	55-gal drum	55-gal drum	55-gal drum	55-gal drum
Container volume (ft ³)	7.35	7.35	7.35	7.35	7.35
Certified by	DOT	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies	Varies
Container weight (lb)	50	50	50	50	50
Material weight (lb)	480	1,110	1,530	450	500
Chemical content (wt%)	See Table 3.80	See Table 3.81	See Table 3.82	See Table 3.83	See Table 3.84
Shipments					
Average weight (tons/yr) ^b	120.5	219.4	9.7	1,729	9.9
Average volume (ft ³ /yr)	3,710	2,930	93.6	57,502	292
Packages/yr	505	399	13	7,821	40
Packages/shipment	48	36	24	48	48
Shipments/yr	11	12	1	163	1
Form of transport/routing					
Form of transportation	Truck	Truck	Truck	Truck	Truck
Destination – facility type	Land disposal ^c	Land disposal ^c	Land disposal ^c	Land disposal ^c	Treatment at POTW ^d

^a Review of the disassembly process indicates that the dimensions of the solids would allow disposal in standard 55-gal drums. Further validation with the vendor may be required.

^b Estimated on the basis of 276 days of operations per year.

^c Depending on test results for hazardous constituents, off-site disposal at a RCRA-permitted facility may be required.

^d Depending on test results for hazardous constituents, off-site treatment at a POTW may be required.

TABLE 3.86 Transportation Data for Solid and Liquid Wastes from Electrochemical Oxidation during Processing of ACW Containing VX Agent at PBA

Type of Data	Output Material No. 1	Output Material No. 2	Output Material No. 3	Output Material No. 4	Output Material No. 5
Transported Materials					
Type/chemical	Scrubber waste	Spent anolyte-catholyte waste from agent treatment	Spent anolyte-catholyte waste from energetics treatment	5X solids – waste ^a	Neutralized HNO ₃ Waste
Physical form	Solid	Solid	Solid	Solid	Liquid
Chemical composition/temperature, pressure	See Table 3.80	See Table 3.81	See Table 3.82	See Table 3.83	See Table 3.84
Packaging					
Type	55-gal drum	55-gal drum	55-gal drum	55-gal drum	55-gal drum
Container volume (ft ³)	7.35	7.35	7.35	7.35	7.35
Certified by	DOT	DOT	DOT	DOT	DOT
Identifier	Varies	Varies	Varies	Varies	Varies
Container weight (lb)	50	50	50	50	50
Material Weight (lb)	490	1,330	1,510	450	510
Chemical content (wt%)	See Table 3.80	See Table 3.81	See Table 3.82	See Table 3.83	See Table 3.84
Shipments					
Average weight (tons/yr) ^b	47.5	322.1	3.2	621	3.7
Average volume (ft ³ /yr)	1,450	3,560	31.5	20,664	108
Packages/yr	198	485	5	2,811	15
Packages/shipment	48	28	24	48	48
Shipments/yr	5	18	1	59	1
Form of transport/routing					
Form of transportation	Truck	Truck	Truck	Truck	Truck
Destination – facility type	Land disposal ^c	Land disposal ^c	Land disposal ^c	Land disposal ^c	Treatment at POTW ^d

^a Review of the disassembly process indicates that the dimensions of the 5X solids would allow disposal in standard 55-gal drums. Further validation with the vendor may be required.

^b Estimated on the basis of a campaign length of 108 days.

^c Depending on test results for hazardous constituents, off-site disposal at a RCRA-permitted facility may be required.

^d Depending on test results for hazardous constituents, off-site treatment at a POTW may be required.

The operation of an ACWA facility would cease with the termination of pilot testing or the elimination of the chemical weapons stockpile. Unless the ACWA pilot facility was converted to some other use, closure and decommissioning would be unavoidable. Thus, both the potential positive and negative impacts of closure and decommissioning would be unavoidable.

3.3.7 COMBINATION TREATMENT TECHNOLOGIES

As indicated previously, the elements of the various unit operations could be combined into different, but viable, ACW treatment alternatives. A number of different combination technologies may be considered. Supplemental information is not provided here for combination technologies. However, based on the information provided in Sections 3.3.2 and 3.3.3, it appears that system inputs and resource requirements, routine emissions and wastes, activities and schedules, and uncertainties would not differ appreciably from the basic systems described in this document.

TABLE 3.87 Activities for Electrochemical Oxidation at PBA

Key Milestones
EIS start
Start of EDS-II testing
PMACWA programmatic EIS submittal
PMACWA programmatic ROD submittal
DOD technology decision
RCRA Part B and CAA permits approval
MDB construction start
MDB construction completion
Systemization/pilot test start
Systemization/pilot test completion
Operations start
Operations completion

Source: PMACWA (2001b).

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